

FS x DYNAMICS

Your Simulation Expert

Jose Fonseca
Group Manager - Germany

FS Dynamics (Fluid Structural Dynamics)

- Consulting-firm concentrated on technical calculations with **over +150 CAE engineers** and **+20 years of experience** in several different industry segments.
- This narrow focus, together with the company's high competence and long-term customer relationships are success factors
- Today, FS Dynamics is the leading consulting-firm focused on calculation services within fluid dynamics (CFD) and structural dynamics (FEM) in the Nordic region.



The Company CFD FEM

CAE Services

All sites, 150+ FEA and CFD, Plasma and Molecular Dynamics consultants.

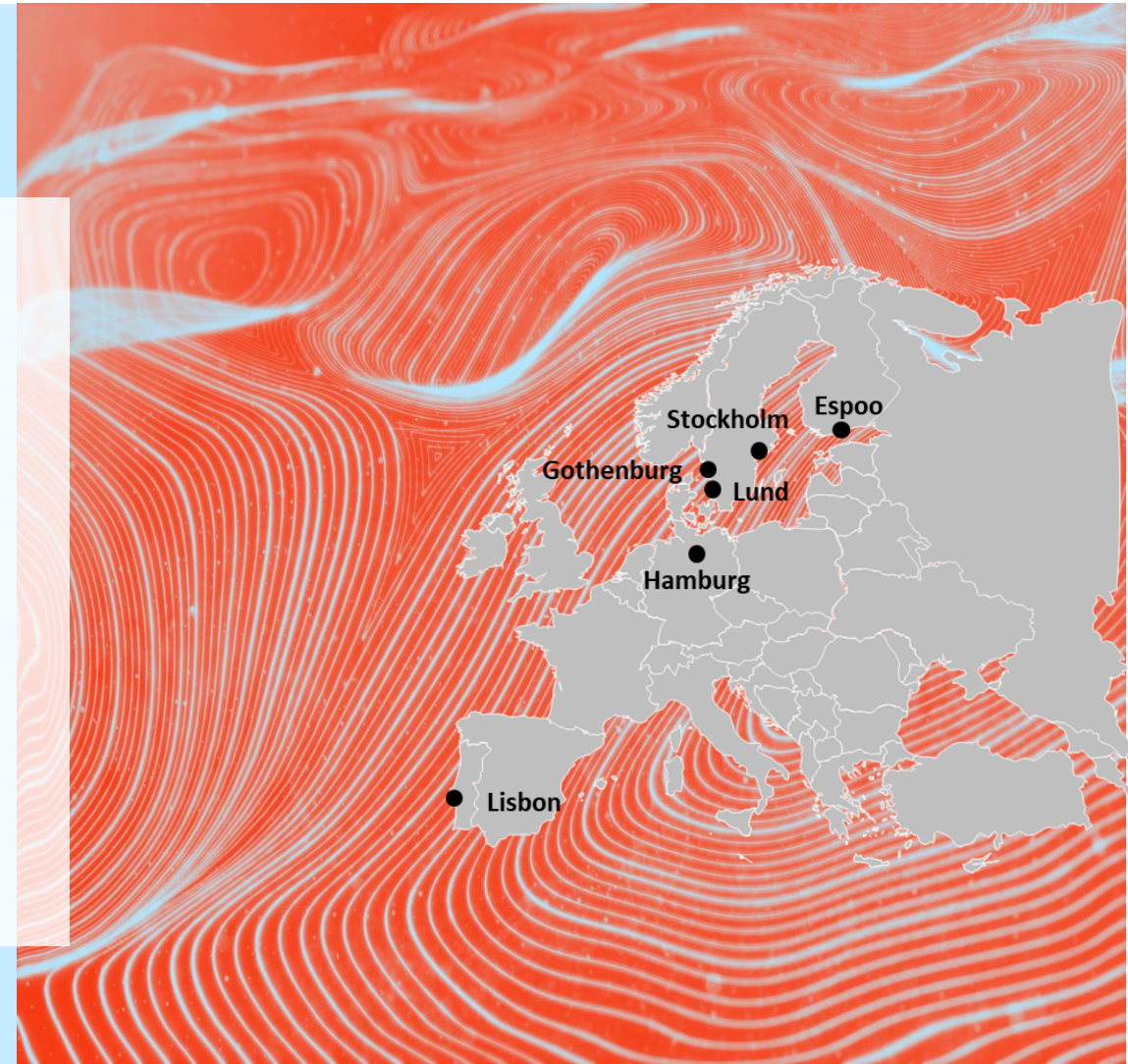
Top Talent recruitment
(~25% PhD, minimum MSc.)

500+ projects with 200+ customers every year

ISO9001: 2015
ISO14001:2015

~50% CFD / ~50% FEM split

Average of 8,5 years of experience per consultant



The Company CFD FEM

Great variation of industries

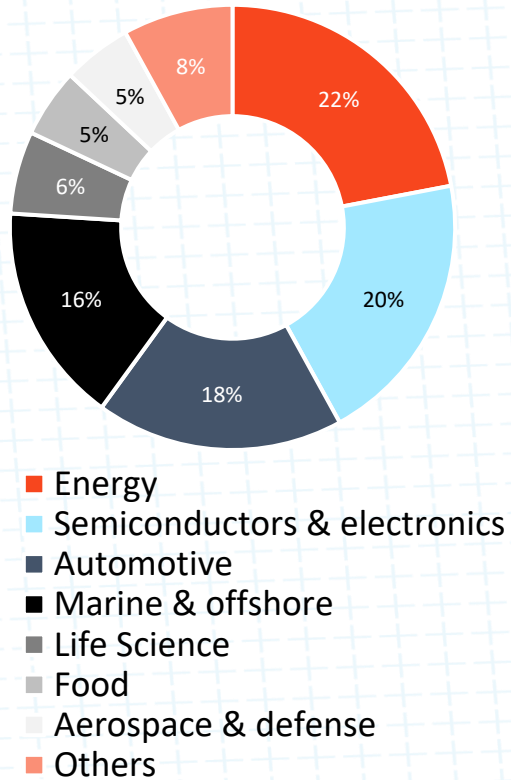
Work within all major markets and all size of companies

- Energy
- Food & Packaging
- Offshore
- Semiconductor
- Process Industry
- Nuclear Energy
- Automotive / Electrification
- Defense
- Medical / Life Science



The Company CFD FEM

Market

**Diversity**

- Mix of SMB and Enterprise customers
- Mix of markets
- Mix of consultant experience level
- Mix of Software

Suitable Ambition Level

- Consultation
- Hand calculation
- Simple Simulations
- Advance Simulations
- Method Development
- Research

The Company CFD FEM



Branch-leading technical resources

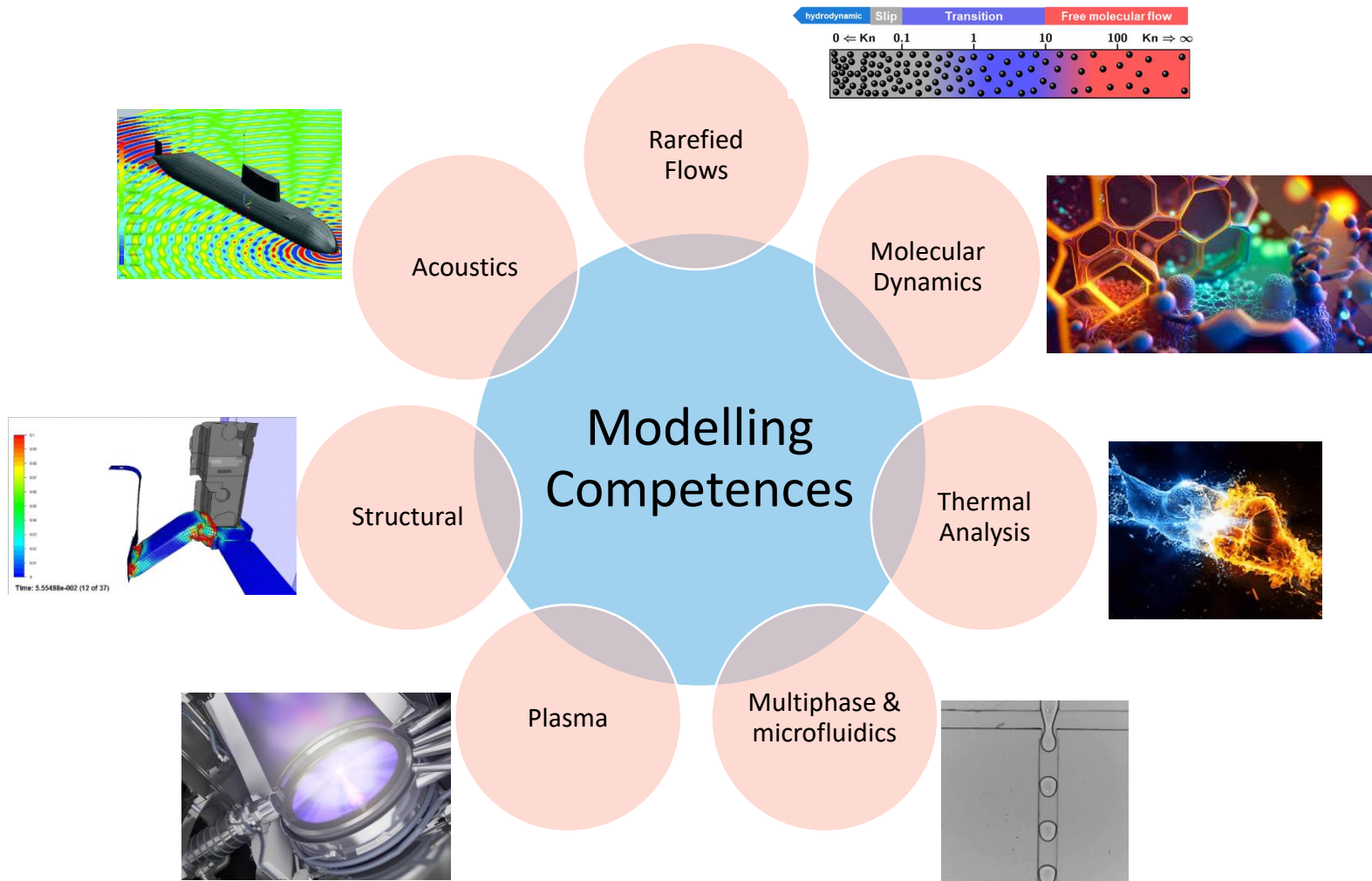
HPC

- Self-hosted server room in Gothenburg
- 2500 CPUs up to 4 TB RAM
- Available for CFD, FEM, Molecular Dynamics and Plasma computation.

The tool is chosen based on the physics, application and customer preference.



Additionally, to standard fluid flow, thermal, acoustics and electrical analyses, FS Dynamics has strong competences in: .

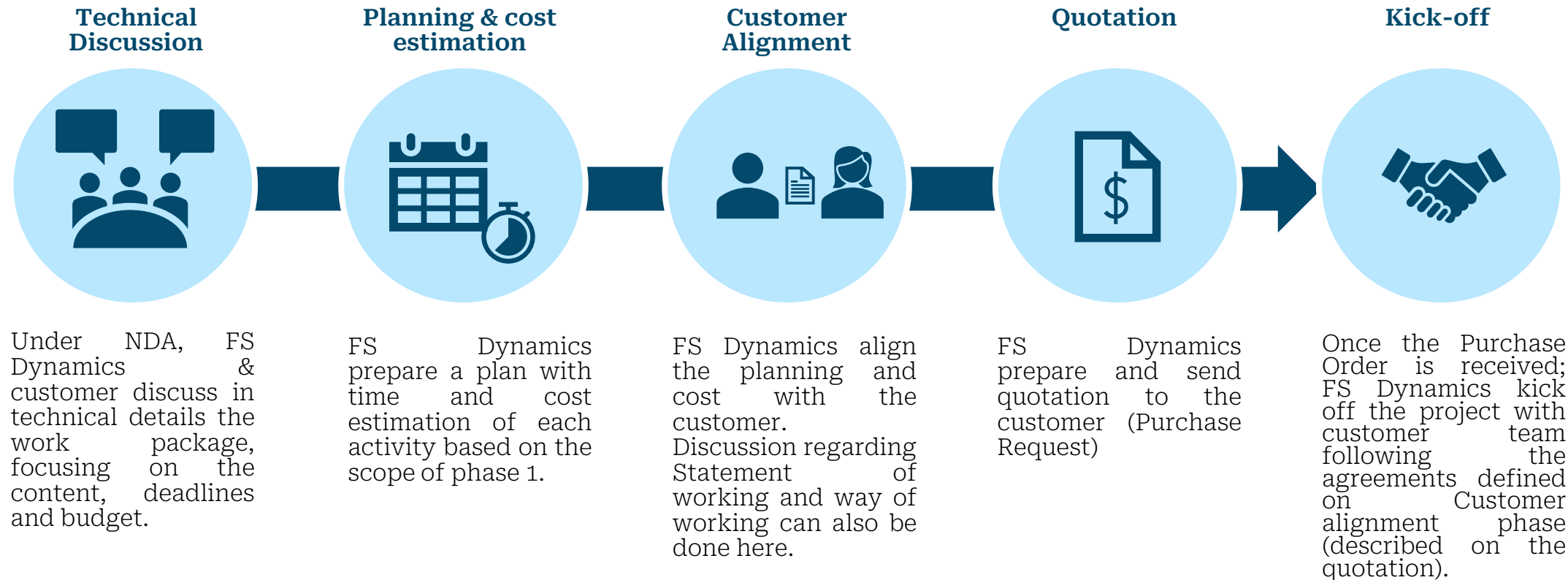




1. Deploying OpenFOAM® anywhere the client needs it
 - Porting to Microsoft Windows - blueCFD-Core: <http://bluecfd.com/Core>
2. Developing GUIs and middleware for client's requirements in their use of OpenFOAM
3. Developing solvers to meet client's simulation needs
4. Developing meshing workflows beyond those available in OpenFOAM
 - Using ANSA from Beta CAE with Python
 - Modifying *snappyHexMesh* to include missing features
5. Setting up and running single phase, multiphase and multi-region simulations
6. Tackling existing modelling limitations in
7. Validating existing models in

Open▽FOAM

FS Dynamics works with work packages



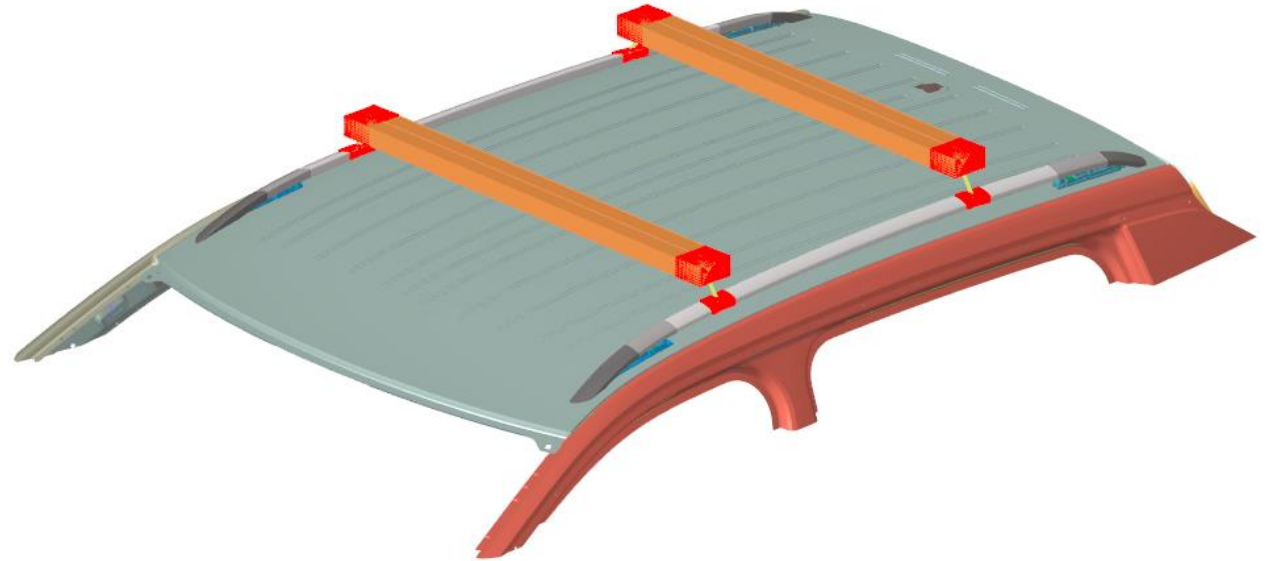
Portfolio

Transport
Energy
Electronics
Aviation
Space

Roof rail systems - FEM

Objective

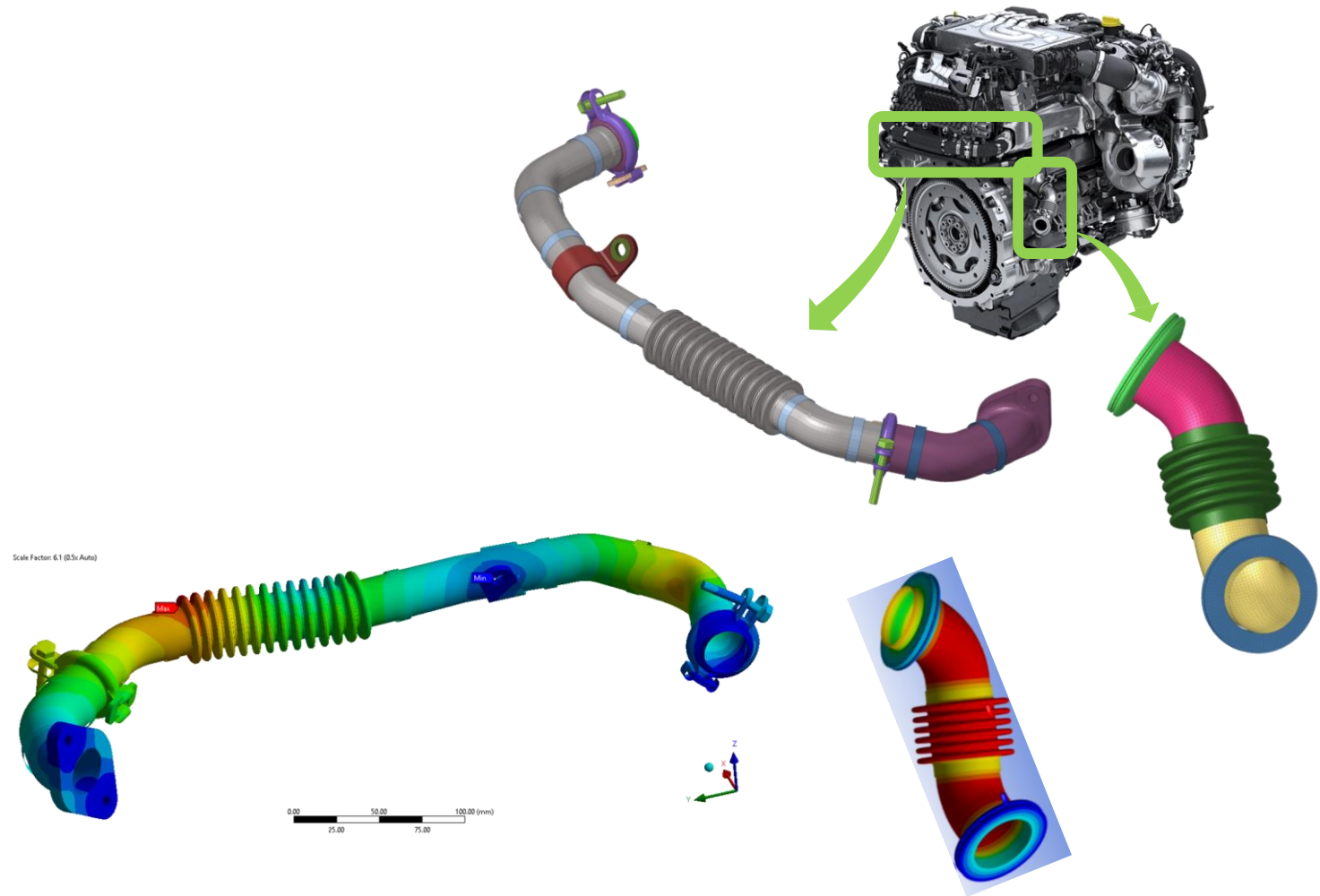
Validate different designs of the roof rail systems for the automotive industry simulating the standard tests scenarios.



ICE tubes - FEM

Objective

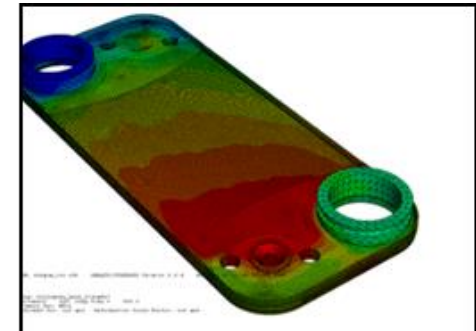
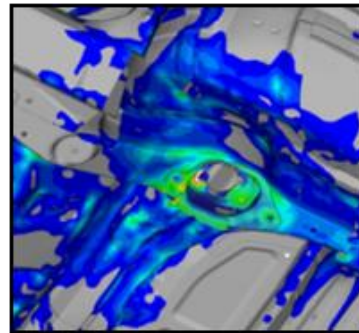
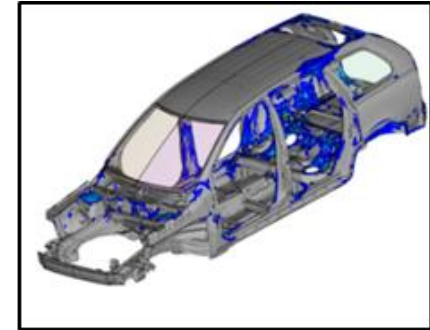
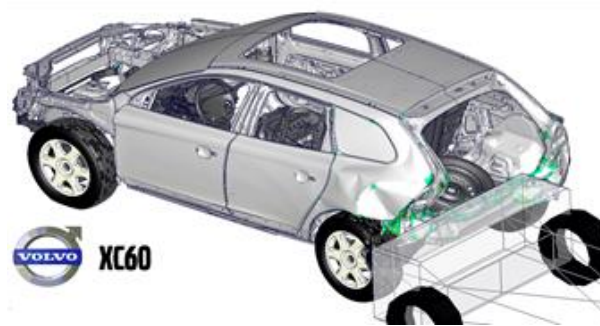
Thermo-mechanical static and dynamics response of different manifolds installed on internal combustion engines.



Crash test - FEM

Objective

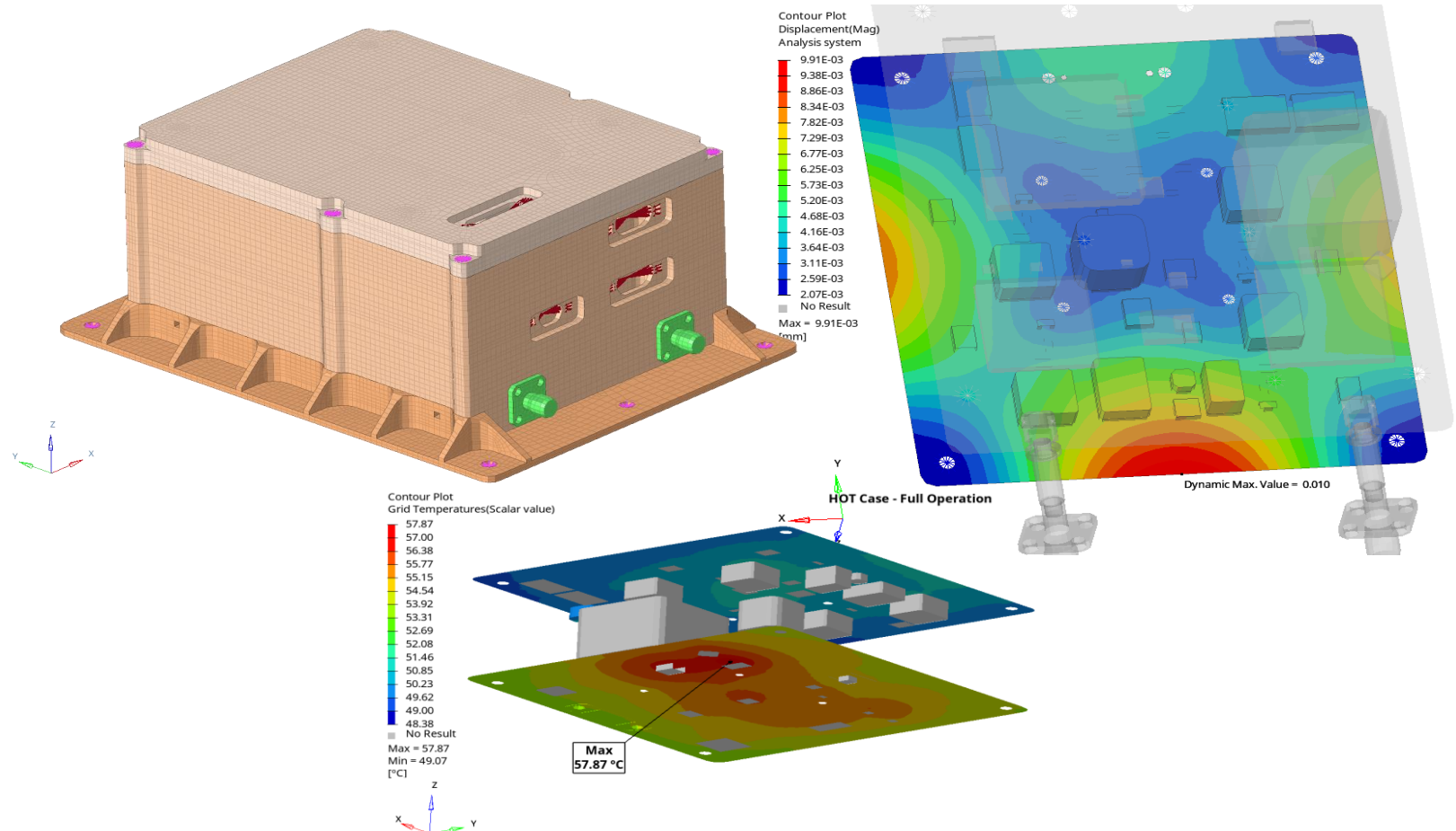
Crash test simulation of vehicle with structural verification down to the single component level.



Payload and system hardware structural verification - FEM

Objective

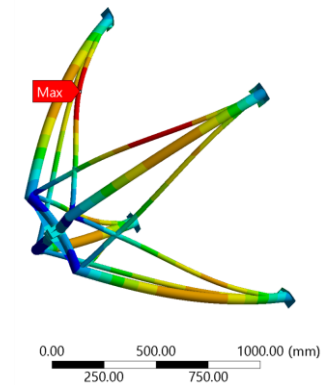
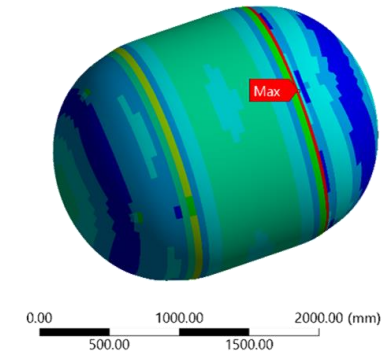
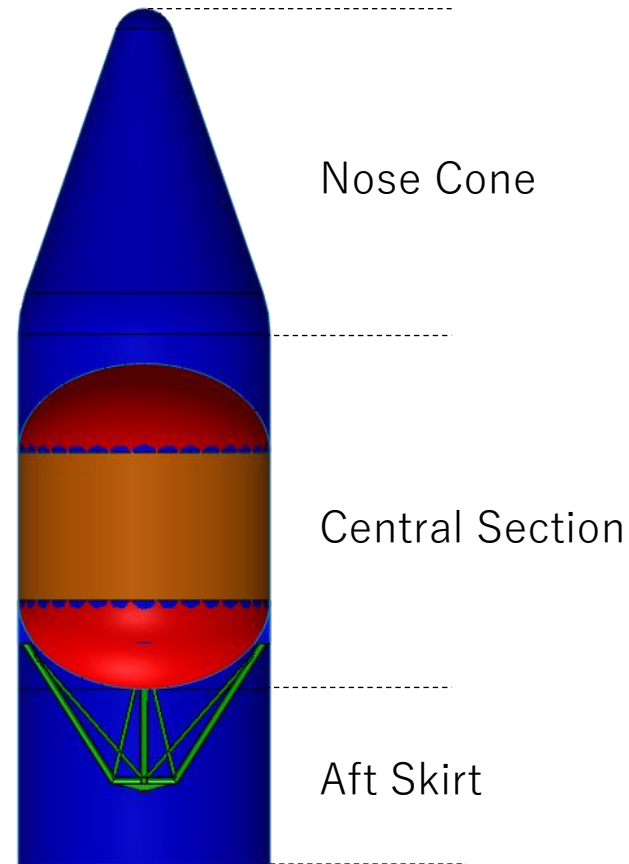
Thermal, static and dynamic response of electronics components for satellites according to ESA requirements.



Rocket launcher - FEM

Objective

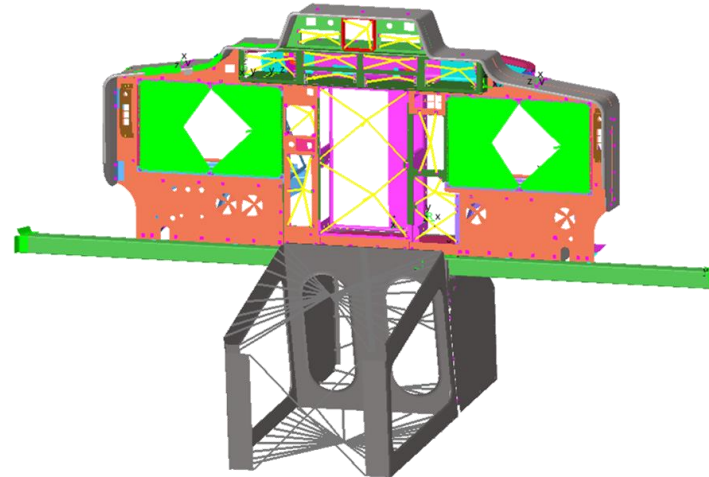
Predesign of a rocket with a tank built with composites materials.



Cockpit avionics panel - FEM

Objective

Static and dynamic response of the new upgrade kit for the C-130 cockpit.

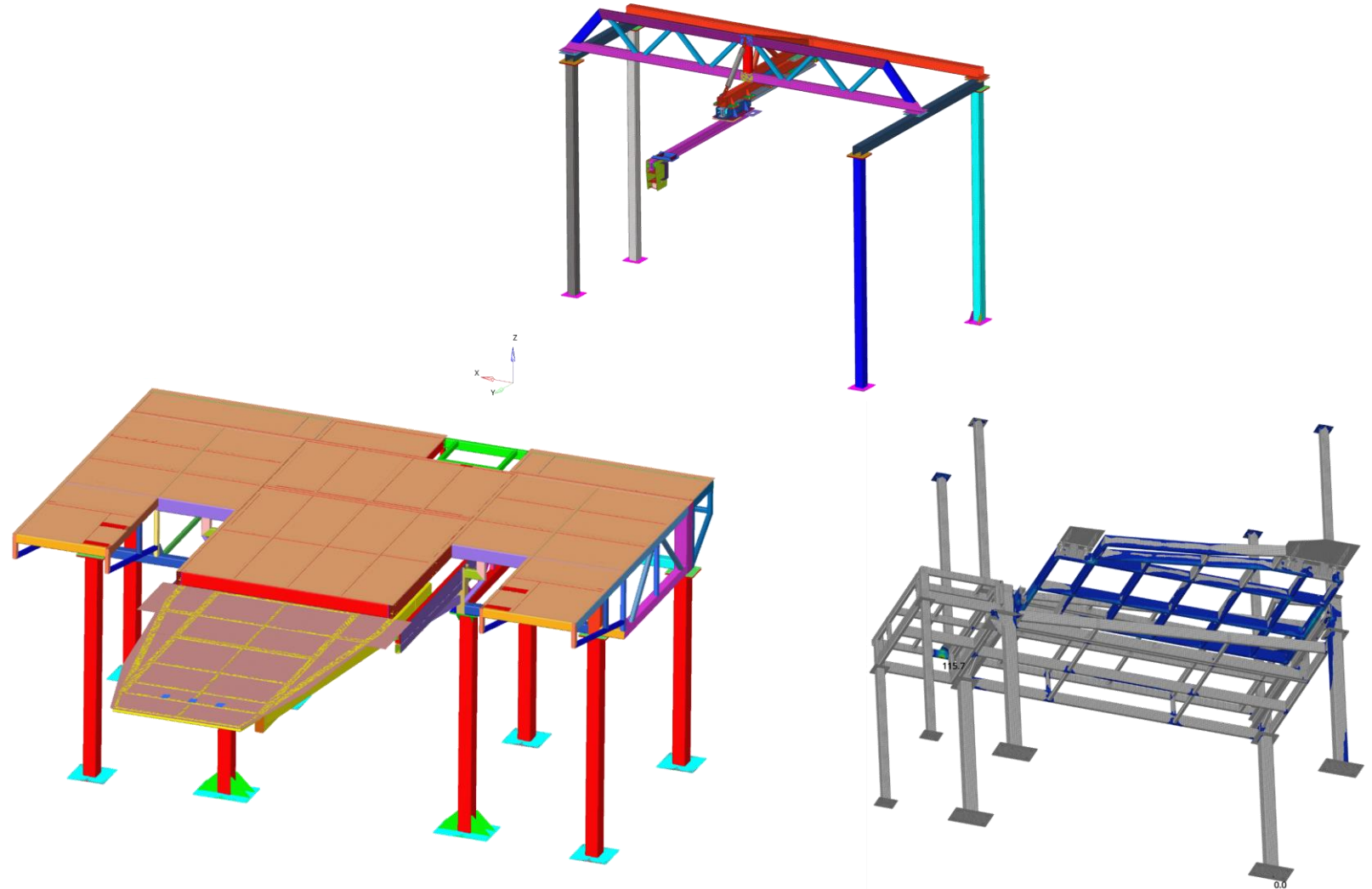


Maintenance platforms - FEM

Objective

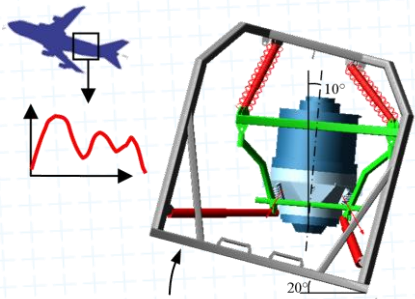
Structural integrity and displacements evaluation of platforms for maintenance of civil aircraft.

FEA methodology driven by the Eurocode norms for metal structures.

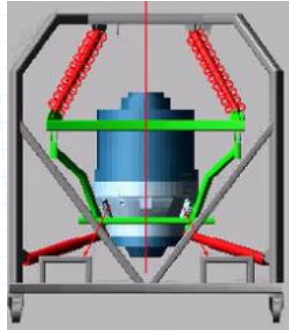


Acceptance Testing of transportation system - Drop test Acceptance testing

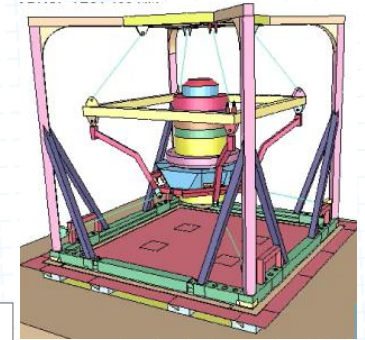
Early development phase tools: MBS Adams simulations
Air plane take off



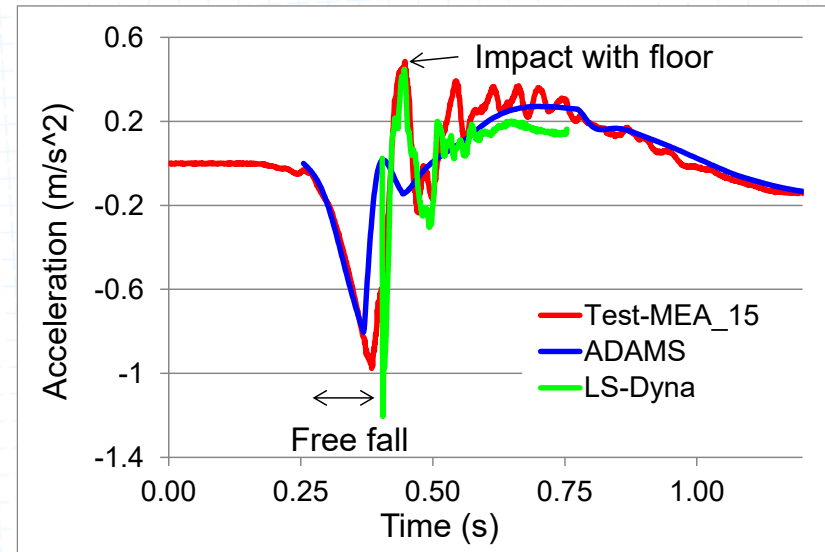
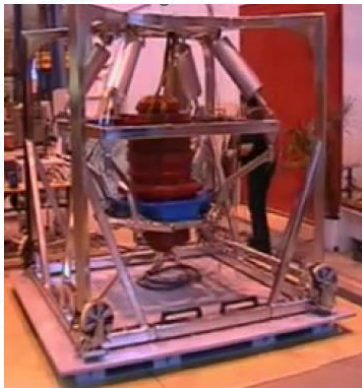
Drop test assessment



Detailed development phase tools:
FEA LS-Dyna simulations drop test

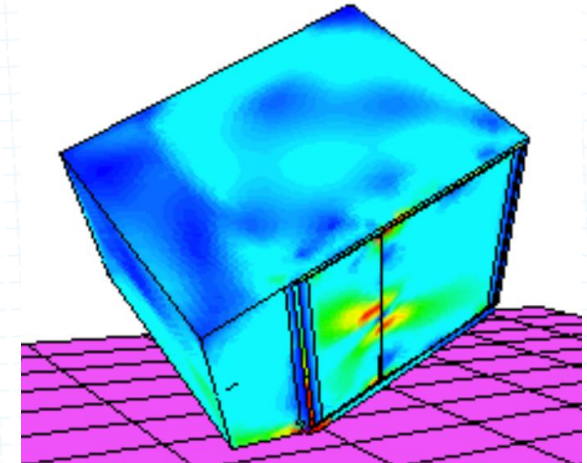
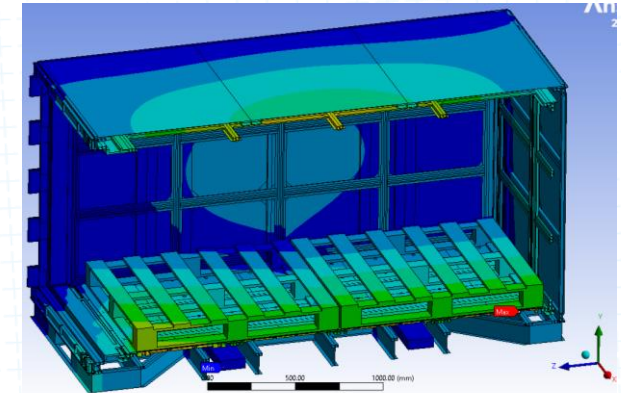


Physical experimental test



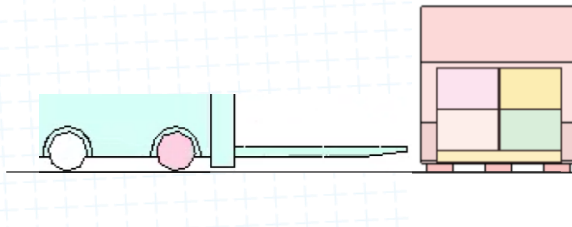
Container Shipment – Development and certification

- Container sizes has a tare weight of 50 to 2000 kg, the full weight including payload is 75 - 9000 kg.
- Comprehensive FEA is defined with global assessment as well as local assessment of:
 - Rivets and bolts. Typically found in aluminium frames as the primary means of connecting parts.
 - Contacts
 - Hinges and Joints
 - Composite material functionality. Monopan sandwich sheets included with equivalent material properties established with Ansys Material designer.
- Representative load cases defined to fulfil standard certification together with internal customer criteria.
 - Fork lift load cases
 - Drop test (corner, edge and flat)
 - Transportation vibration

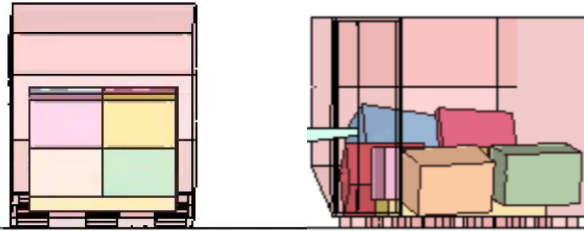


Container handling - Structural assessment of fork truck abuse

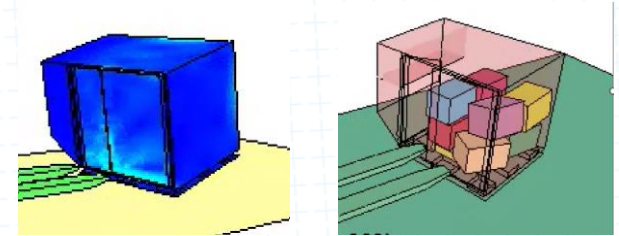
For truck running into container with packages standing on an edge



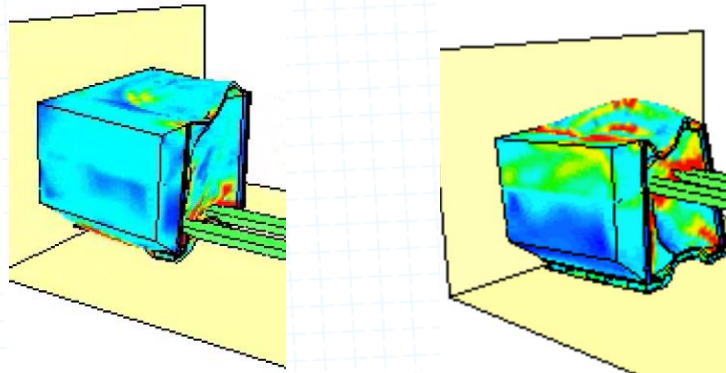
Results from two scenario:
Constrained packages Unconstrained packages



For truck running into container with unconstrained packages



For truck running into and crushing the container. Fork blades at different elevations



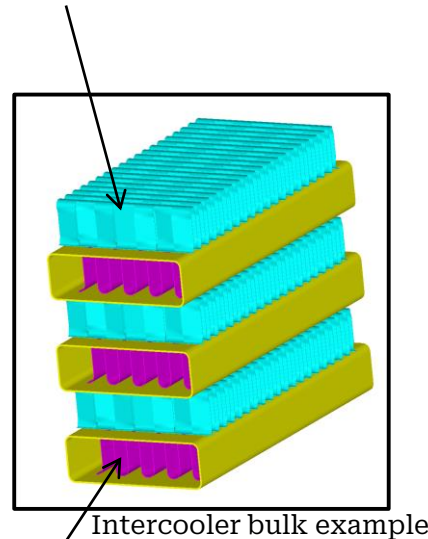
Transport
Energy
Electronics
Wastewater
H.V.A.C.
Biomedical
Process
Machinery

Fin Design for compact HE

Objective →

Optimize fins in Cold and Hot streams of a compact gas-gas intercooler so that cost can be reduced (reduced metal use) and improve efficiency.

Cold stream fins may change, but:
 - thermal efficiency should be increased at the same or smaller pressure drop;
 - constraints on geometrical settings.

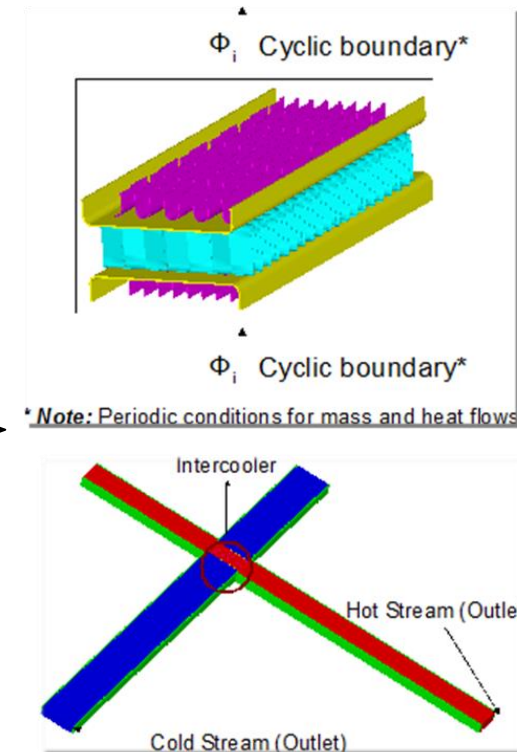


Hot stream fins may change but they are less important than the cold stream fins.

Complex geometries –
 Reduced computational molecule with around 4M grid nodes of structured, purpose built, mesh, for quality.

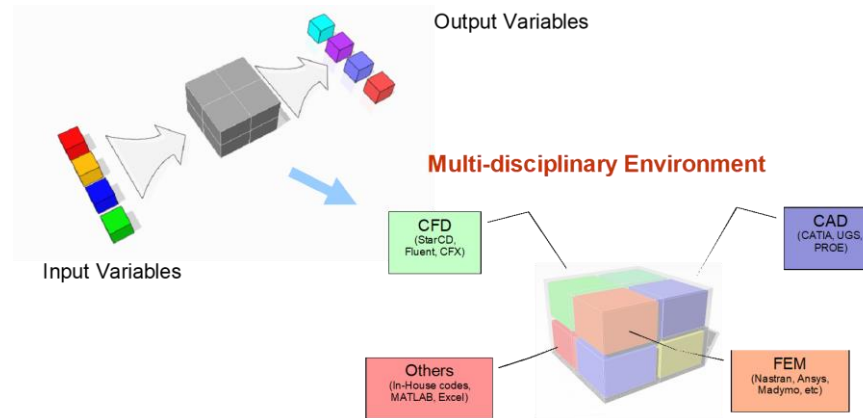


Improve computational efficiency



Fin Design with Automatic Optimization

Objective →
Devise
economical
optimization
procedure



Based on initial fin configuration, parametric runs were performed coupling an optimization tool, **modeFRONTIER**, with **STAR-CD**

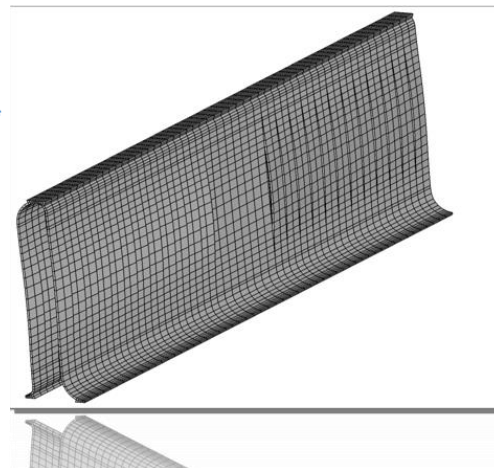
Optimization Objectives:

Maximize Thermal Efficiency*

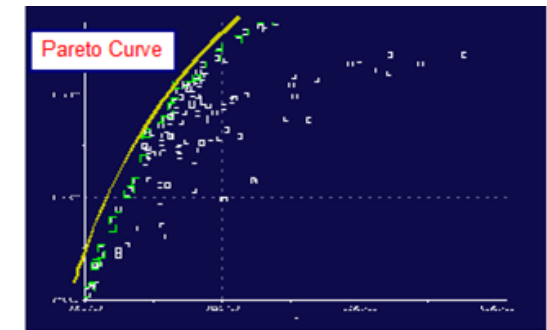
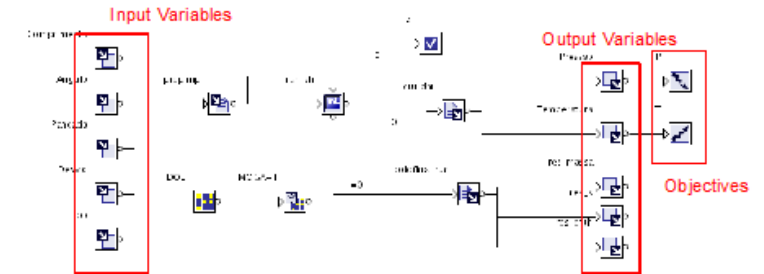
Minimize Pressure Drop

* defined as:

$$\eta = (T_{out} - T_{in}) / (T_w - T_{in})$$



Optimization Workflow



Points marked green are **Pareto points**, i.e., they are all **optimal designs**.

Pressure drop versus Outlet temperature

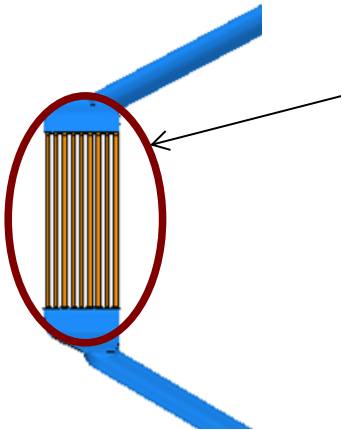
Over 150 runs performed



Potential for significant gains at a reduced computational cost

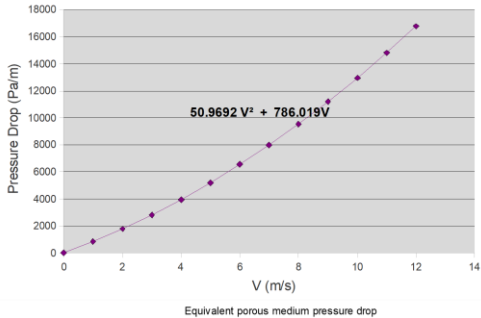
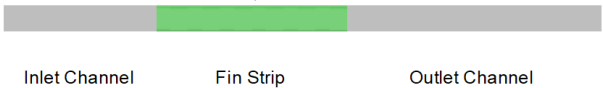
Full Intercooler Simulation – How-To

Objective →
Allow simplified
but accurate
full-intercooler
simulations



Cold and hot stream bulk simulated as a porous medium due to high computational cost

Coefficients
determined via
direct simulation.



Simulations possible for any
intercooler fins.

$$\frac{DP}{Dx} [Pa/m] = \frac{\mu}{xK1} V + \frac{\rho}{xK2} V^2 \text{ with } V [m/s]$$

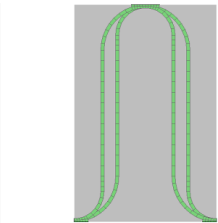
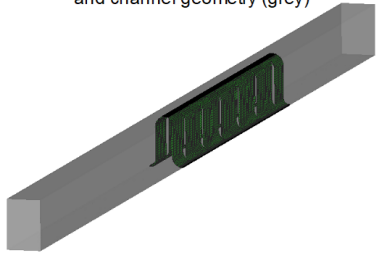


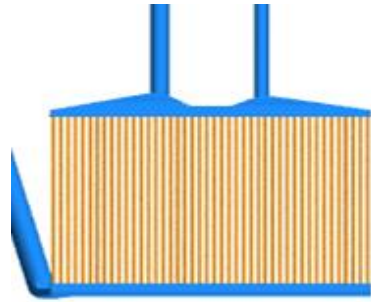
Figure 1 – Offset Fin (green)
and channel geometry (grey)



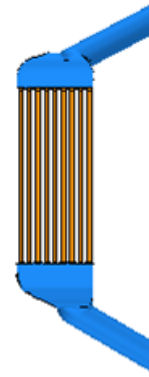
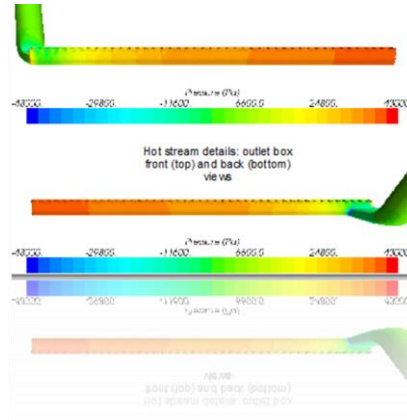
	Intercooler	"Mosaico"	"Downface"	"Fullface"	"Alumec"	"AirWater"
Hot Stream	Type	Offset	Offset	Offset	-	Louvered
	Height (mm)	7.2	7.2	7.2	-	7.5
	Half-Step (mm)	1.4	1.7	1.7	-	1.5
	# Steps	28	16	N.A.	-	N.A.
	Thickness (mm)	0.115	0.115	0.115	-	0.08
	xk1	1.31E-007	1.12E-007	1.12E-007	-	2.73E-008
	xk2	7.27E-002	8.00E-002	9.00E-002	-	1.12E-002
Cold Stream	Type	Louvered	Offset	Offset	Louvered	-
	Height	7.5	7.2	7.2	N.A.	-
	Half-Step	1.6	1.6	1.4	N.A.	-
	# Steps	94	148	N.A.	N.A.	-
	Thickness	0.08	0.115	0.115	N.A.	-
	xk1	3.71E-008	1.05E-007	1.31E-007	N.A.	-
	xk2	1.71E-002	8.29E-002	7.27E-002	N.A.	-

Intercooler Simulation

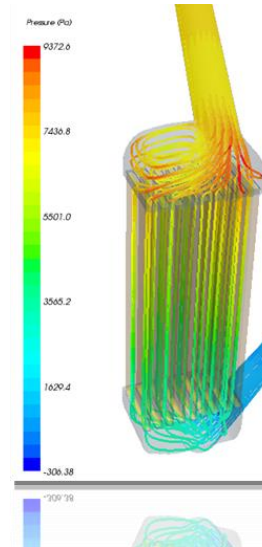
Objective →
Allow simplified
but accurate
full-intercooler
simulations



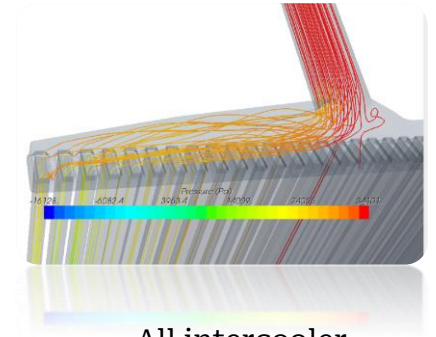
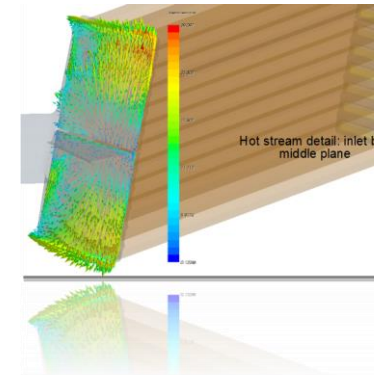
“Fullface”



“Mosaic”



“Downface”



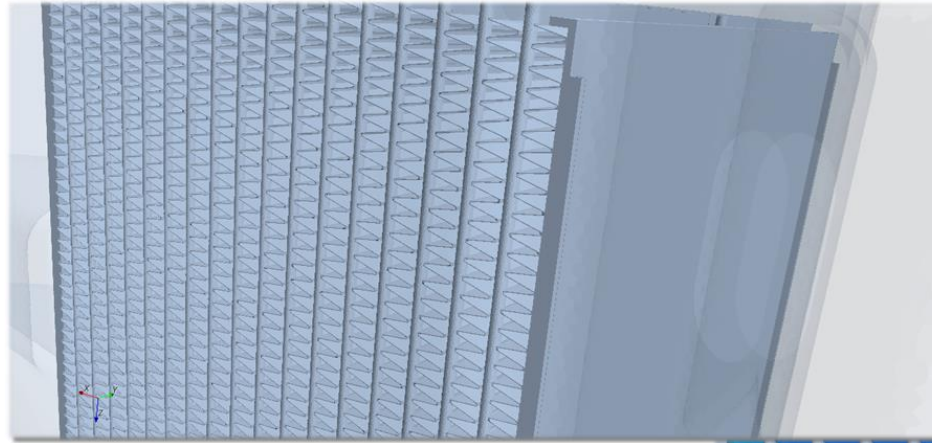
All intercooler
simulations showed good
agreement with available
experimental data.



**Introduced new
simulation
methodology in
customer's R&D
department.**

Full Intercooler Simulation – PROGRESS

Objective →
Reduce
simplifying
assumptions

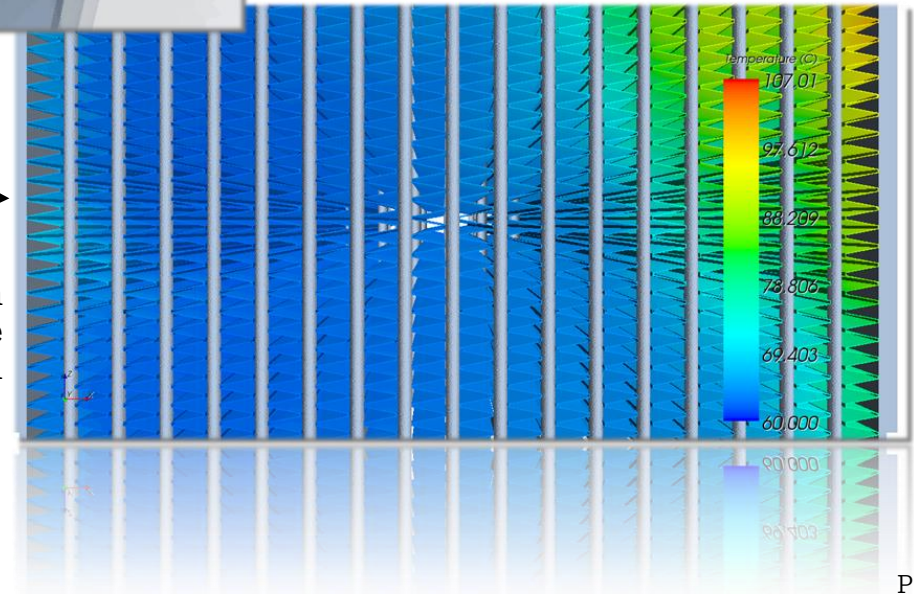


With time, increased
computational power has
allowed for the introduction of
fin geometries in full intercooler
simulations.



Increased **geometrical** and
physical fidelity

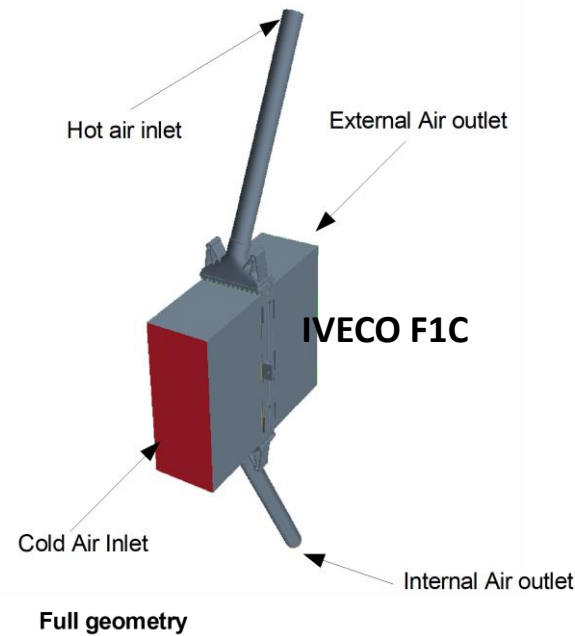
Fin
temperature
detail



Thermal Load Induced Solid Stresses

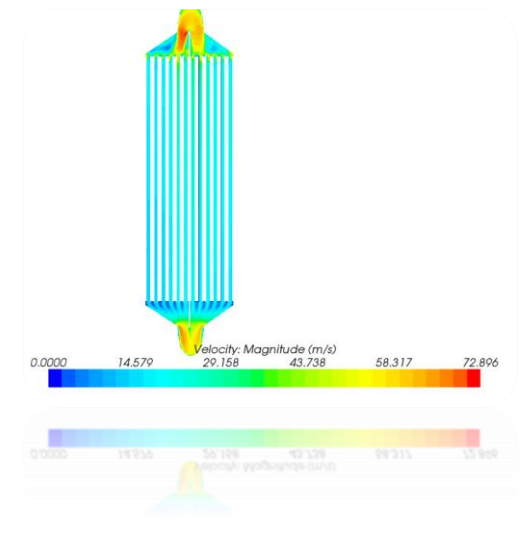
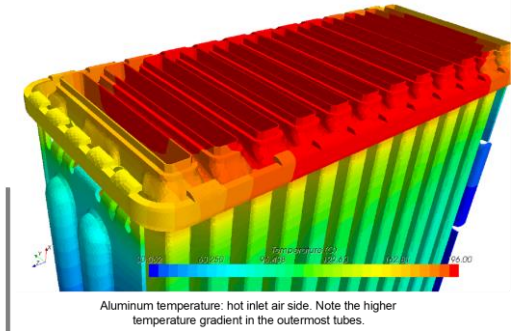
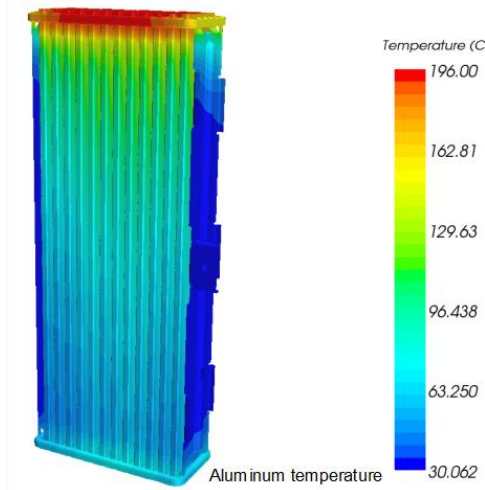
Objective →

Accurate temperature distribution in solid material to enable the computation of solid stresses and the identification of high-stress regions



NB: Just temperature is shown. Solid stresses computed in SI units, *i.e.*, *Pa*.

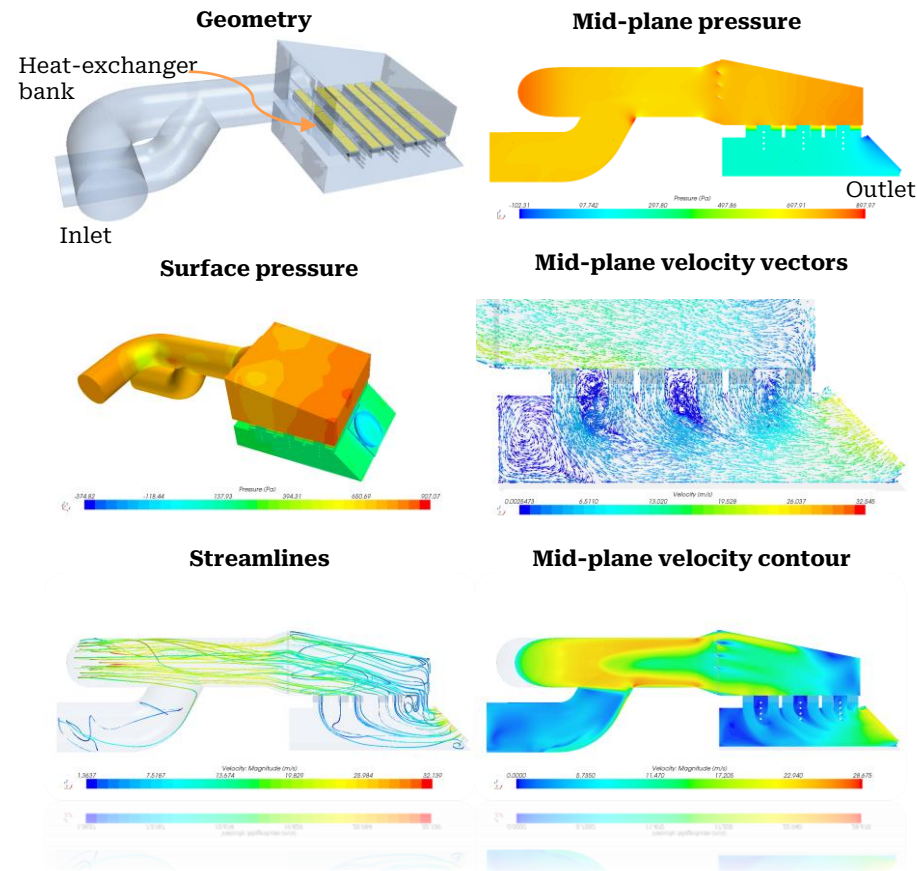
Complex geometry.
700000 polyhedral cells



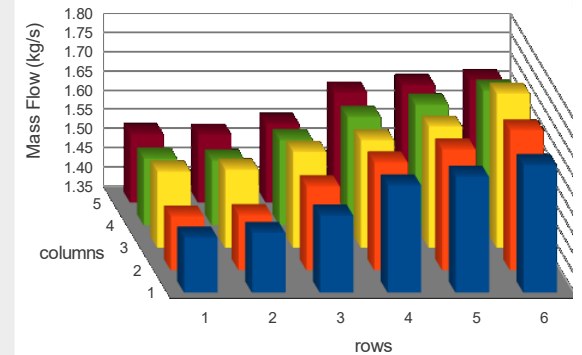
Industrial Waste Heat Recovery

Objective →

Optimize flow distribution across heat-exchanger bank for maximum efficiency



Mass-Flow distribution across heat-exchangers

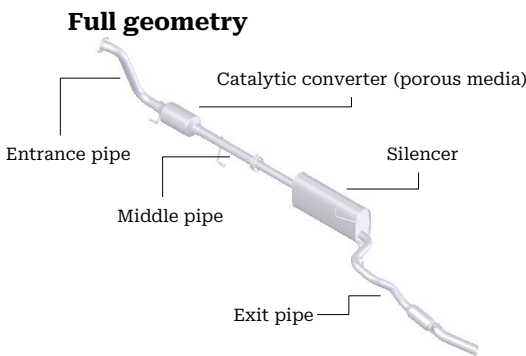


Facility built and in operation.

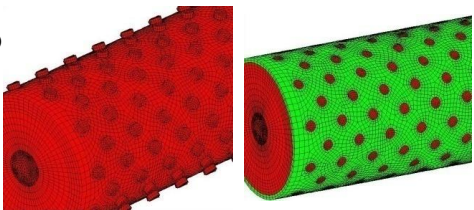


Automotive Exhaust Systems

Objective →
Determine
pressure drop and
heat-transfer on
exhaust system



Mesh at the silencer tubes, inc/holes.

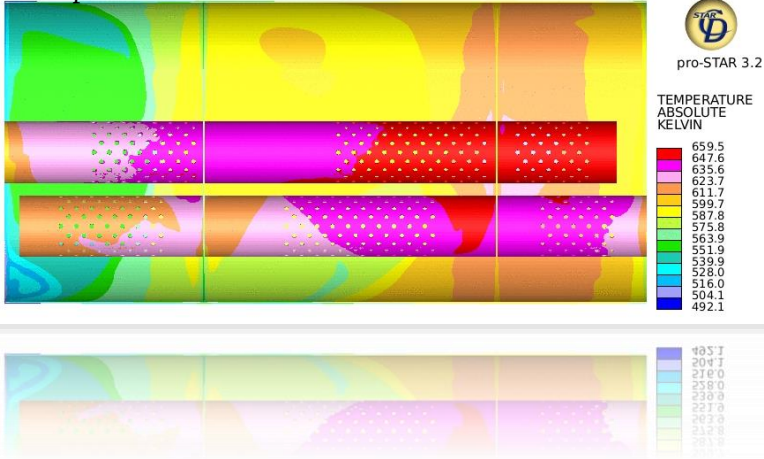


Range of turbulence models tested
Mesh studies for results
independence

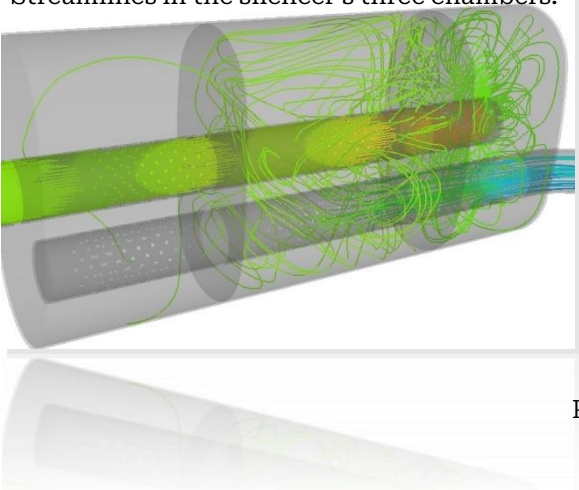
Pressure drop along the system

Component	Δp (bar)	%
System	0,353	100
Entrance pipe	0,005	1,4
Catalytic converter	0,057	16,1
Middle pipe	0,073	20,5
Silencer	0,198	55,9
Exit pipe	0,021	6,0

Temperature distribution at the inside walls of the silencer.



Streamlines in the silencer's three chambers.



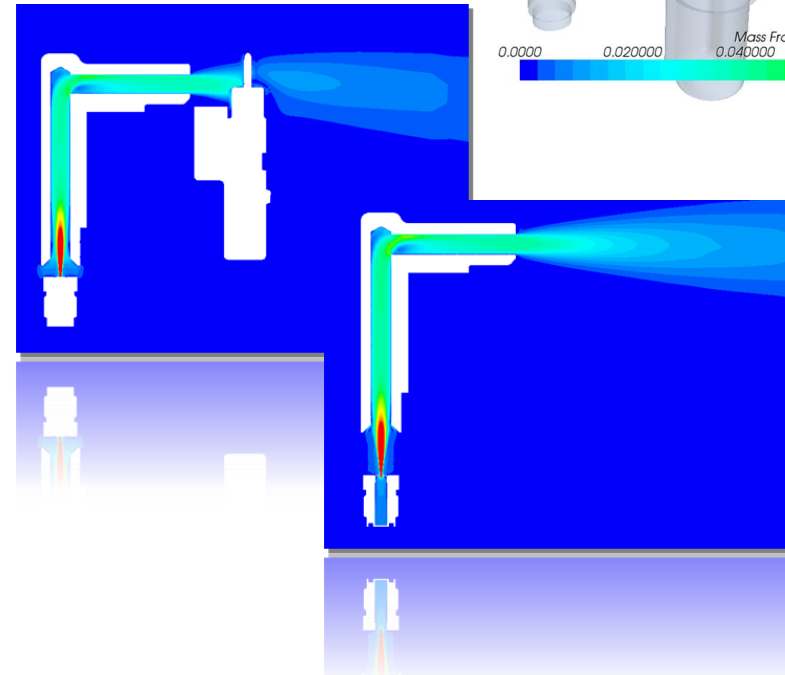
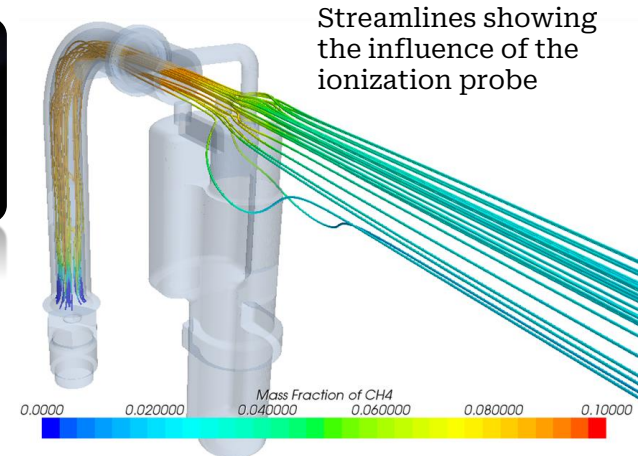
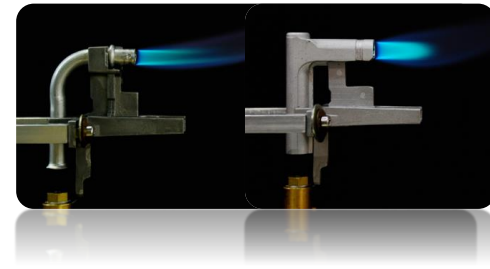
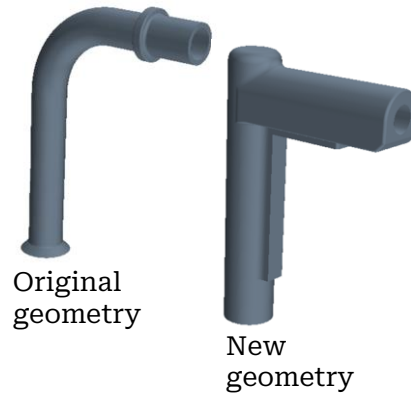
Boiler Pilot Flame Optimization – I

Objective →

Improve
mixture
fraction
uniformity at
pilot outlet

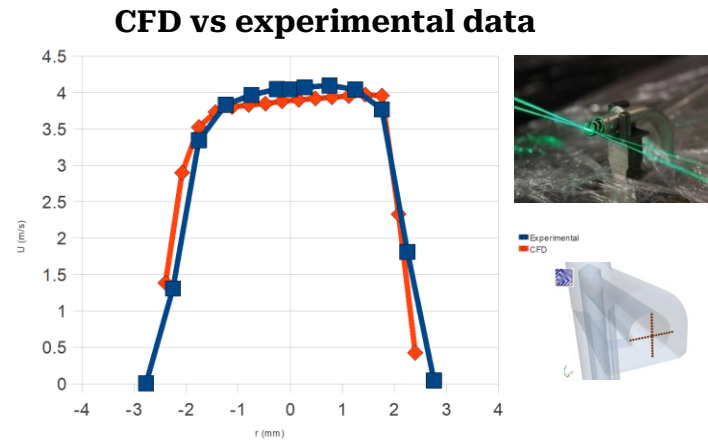
Parameters:

Geometry
Different injector distances
Presence of ionization probe
Different gases → methane/propane



Boiler Pilot Flame Optimization – II

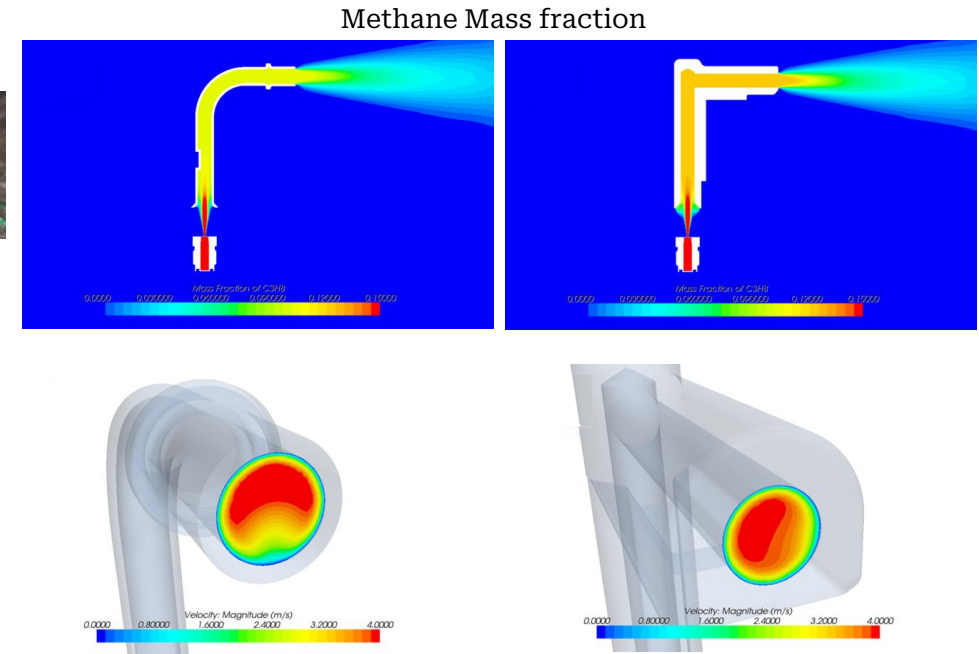
Objective →
Improve mixture
fraction
uniformity at
pilot outlet



Velocity along vertical
centerline (z)

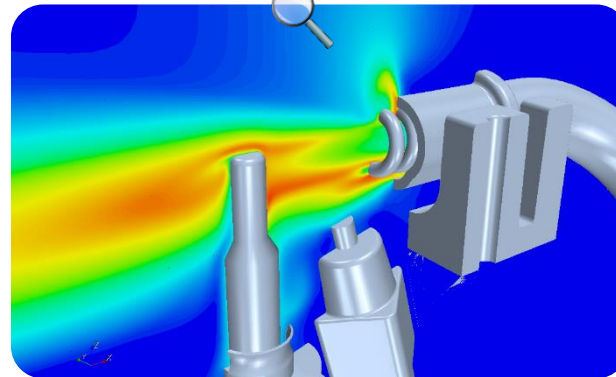
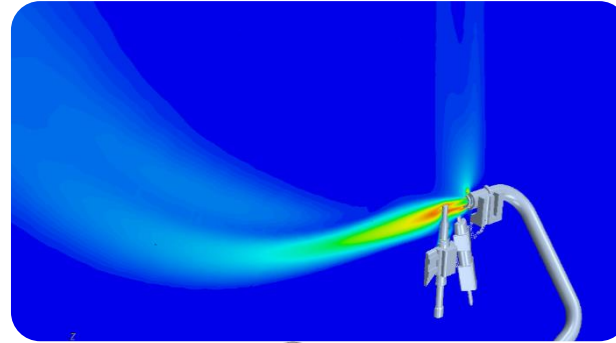
	Experimental	CFD	Diff (%)
Pilot 1	1.74	1.79	2.98
Pilot 2	1.97	2.04	3.62

CH_4 equivalence ratio Φ at pilot outlet

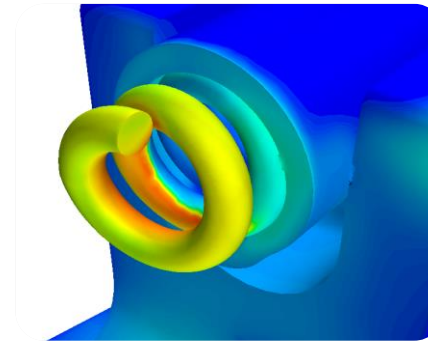


Boiler Pilot Flame Optimization – III

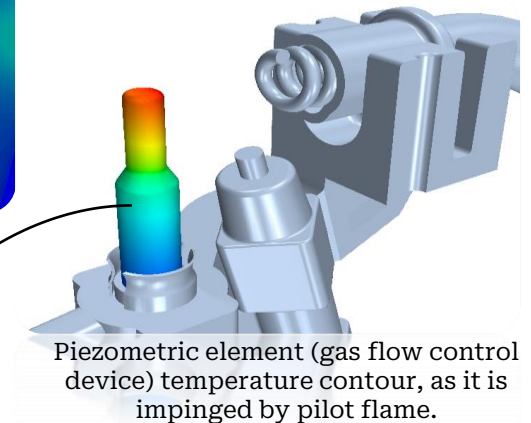
Objective →
Temperature analysis of piezometric element under operating conditions/verification of material compliance with operating limits established by manufacturer.



Gas temperature contour at symmetry plane.



Coil temperature during operation.

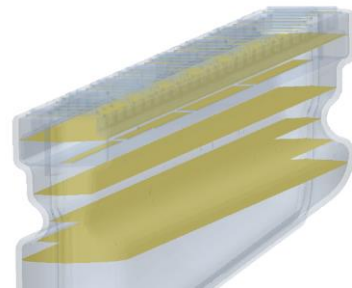


Piezometric element (gas flow control device) temperature contour, as it is impinged by pilot flame.

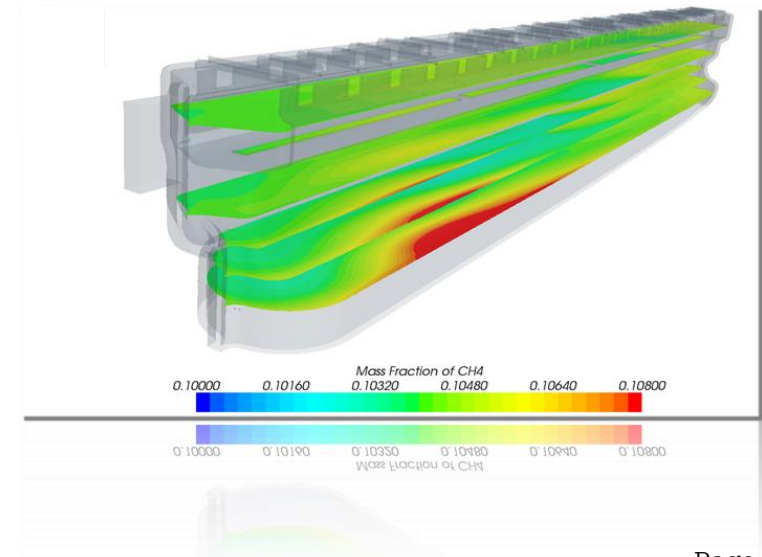
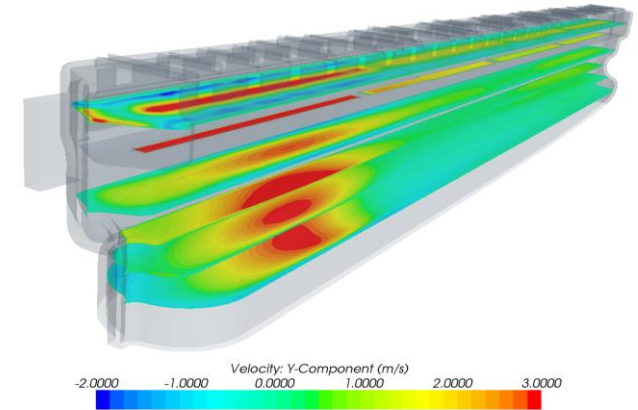
Material complied with specs, surface temperature below threshold.

Burner Flute Optimization – I

Objective →
improve
equivalence ratio
distribution at
flute exit with
new burner
shape to reduce
cost

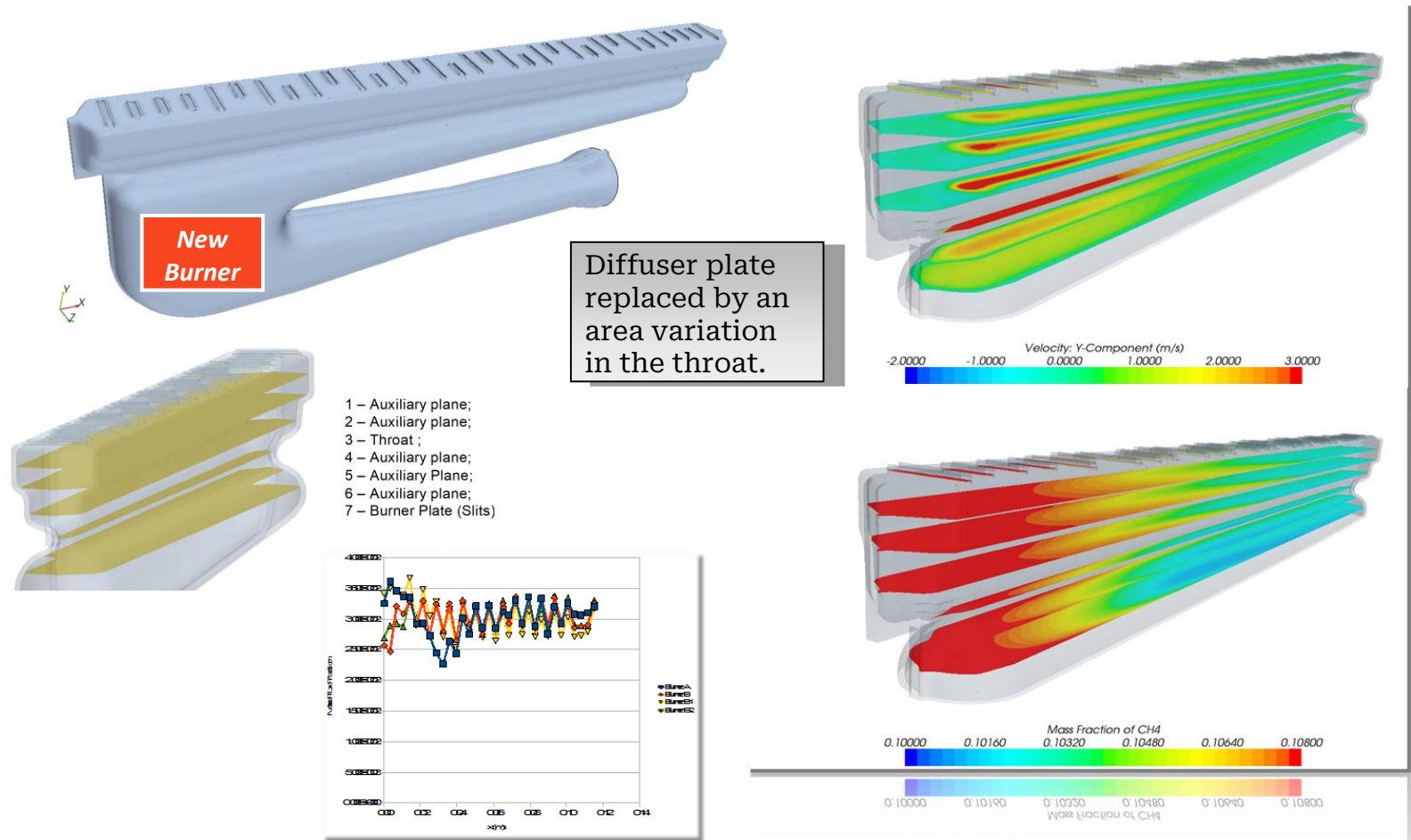


- 1 – Auxiliary plane;
- 2 – Auxiliary plane;
- 3 – Throat ;
- 4 – Auxiliary plane;
- 5 – Diffuser Plate;
- 6 – Auxiliary plane;
- 7 – Burner Plate (Slits),



Burner Flute Optimization – II

Objective →
improve
equivalence
ratio
distribution
at flute exit
with new
burner shape

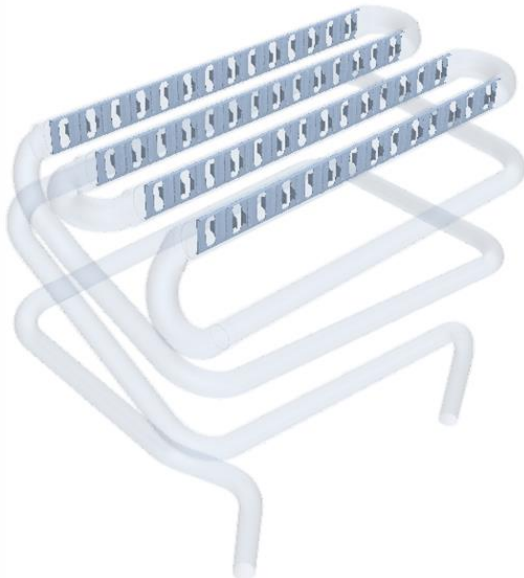
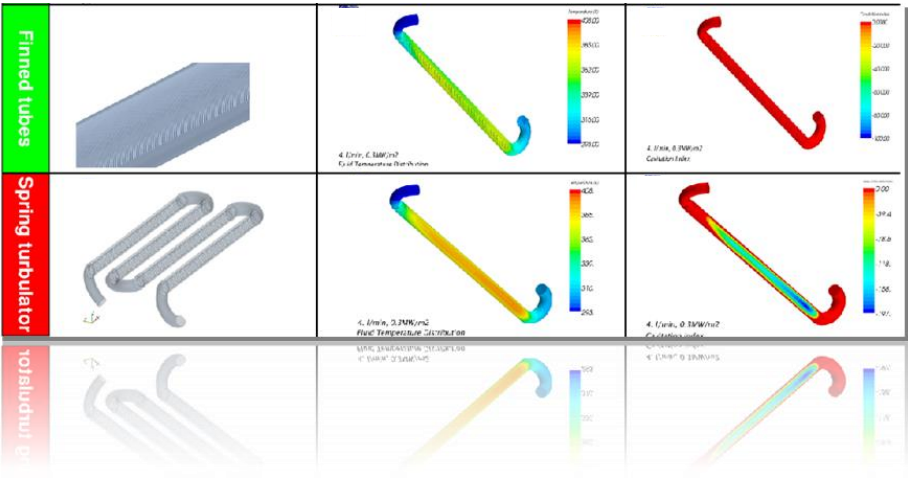


Boiler Turbulator

Objective →
 Replace/Remove
 Turbulator,
 proposing or
 trying out new
 shapes to reduce
 cost on a home
 appliance gas-
 liquid heat
 exchanger

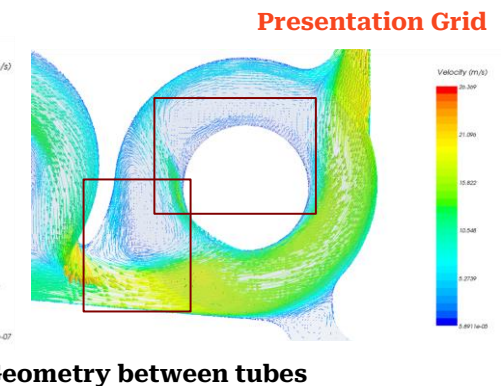
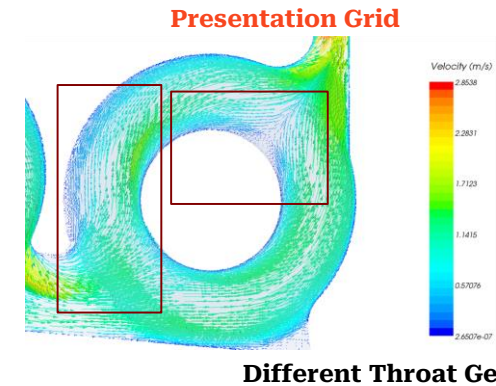
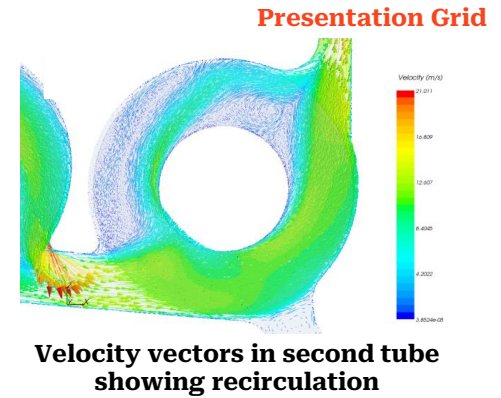
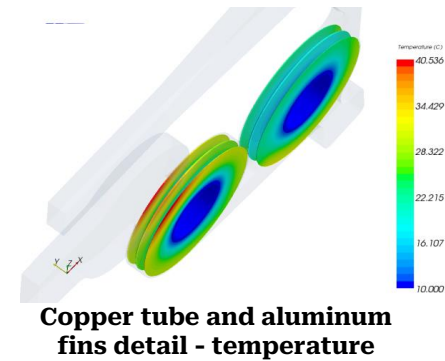
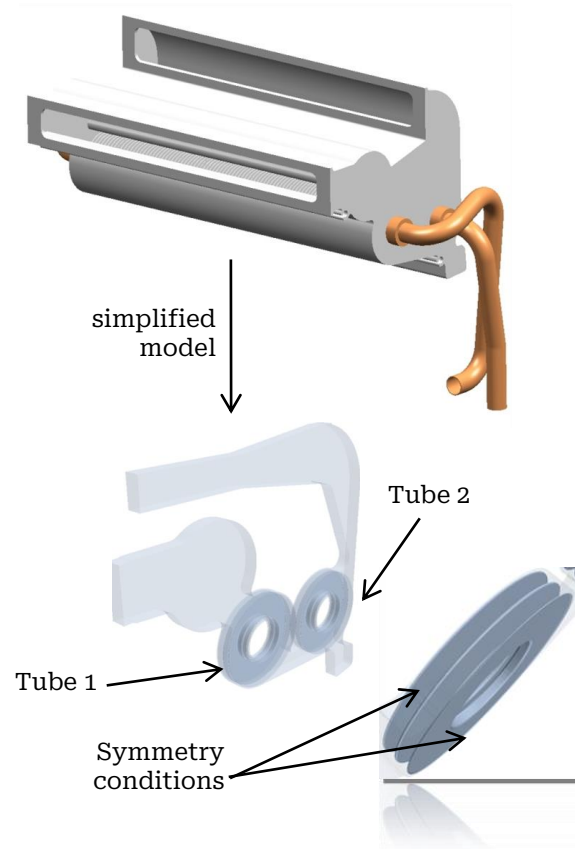
Turbulator function:

- **Heat transfer enhancement**
- Reduce cavitation/boiling inside the tubes
- Reduce vibration and acoustic noise
- Increase durability



Condensation Heat Exchanger – I

Objective →
Improve
efficiency of
condensing
heat-exchanger



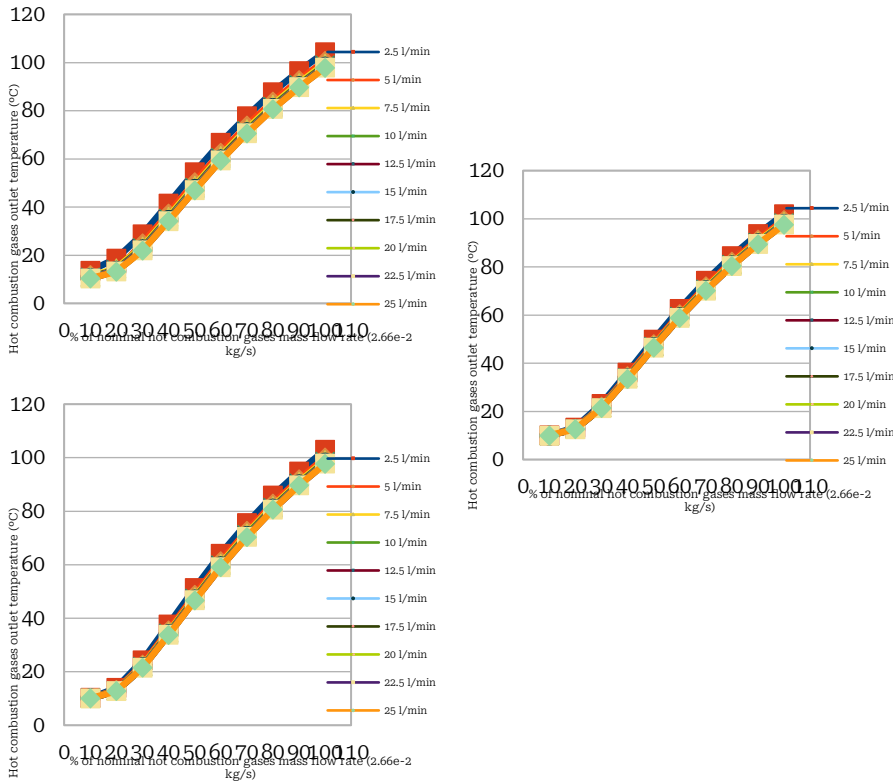
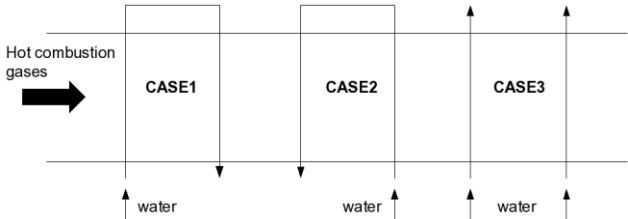
Condensation Heat Exchanger – II

Objective →
Improve efficiency of condensing heat-exchanger when CFD is too expensive through alternative design approach: study water flow influence and overall heat exchanger performance for several water and hot combustion gases flow rates.

	Exchanged Heat (W)					
	T _w =10	% Total	T _w =20	% Total	T _w =40	% Total
Tube 1	53.53	61.71	51.17	61.78	46.48	61.78
Tube 2	33.21	38.29	31.66	38.22	28.76	38.22
Total	86.74	100	82.82	100	75.24	100

	Heat Transfer Coefficient U (W/m²·K)		
	T _w =10	T _w =20	T _w =40
Tube 1	46.36	46.53	46.97
Tube 2	45.38	45.60	46.46

While exploring the possible design envelope for the heat exchanger, CFD results were used as inputs to ε-NTU **analytical** methodology

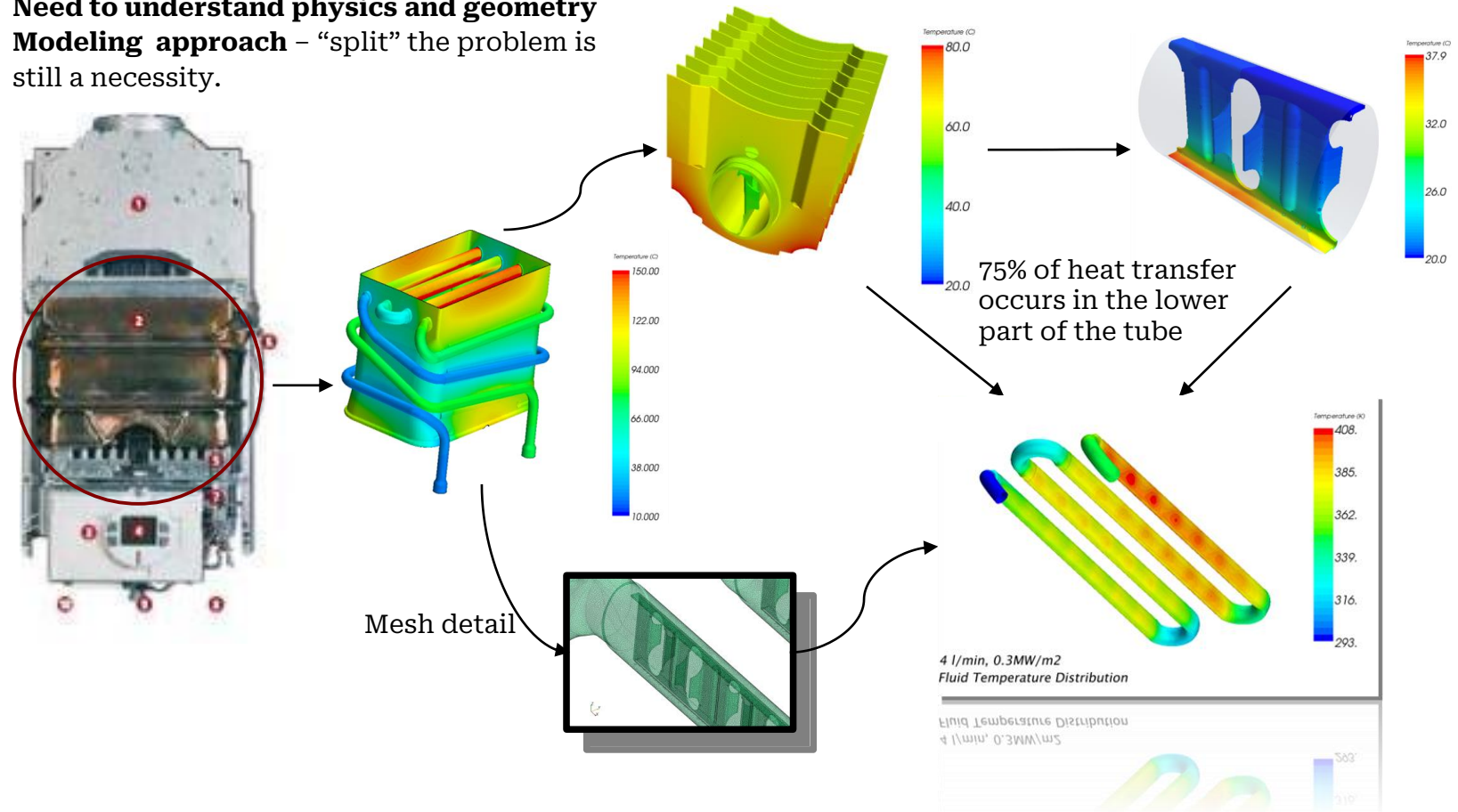


Combustion Chamber

Objective →

Full representation of a wall-standing domestic water heater

Need to understand physics and geometry
Modeling approach – “split” the problem is still a necessity.

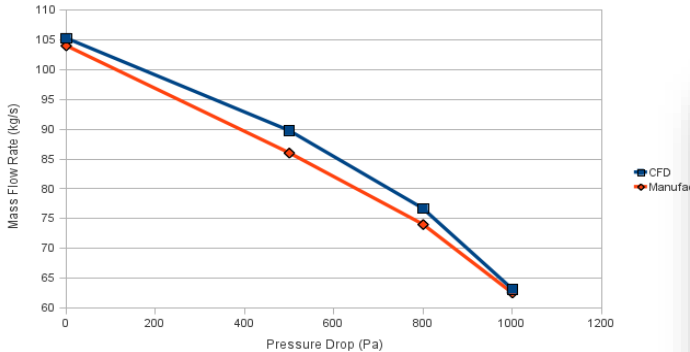


Mechanical Air Supply Simulation

Objective →
Evaluate ventilator performance and include its effects on downstream components

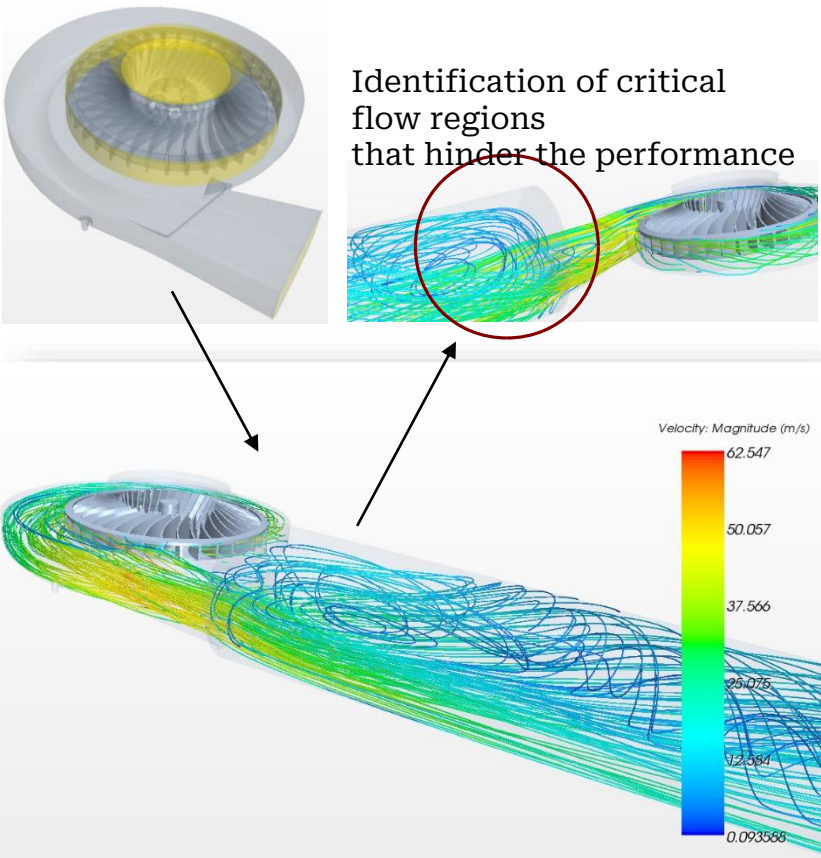
	Mass Flow Rate (kg/s) through ventilator			
	0 Pa	500 Pa	800 Pa	1000 Pa
CFD	105.26	89.74	76.66	63.15
Manufacturer	104.00*	86.00	74.00	62.50
Diff (%)	1.21	4.35	3.59	1.04

* Extrapolated from manufacturer's curve



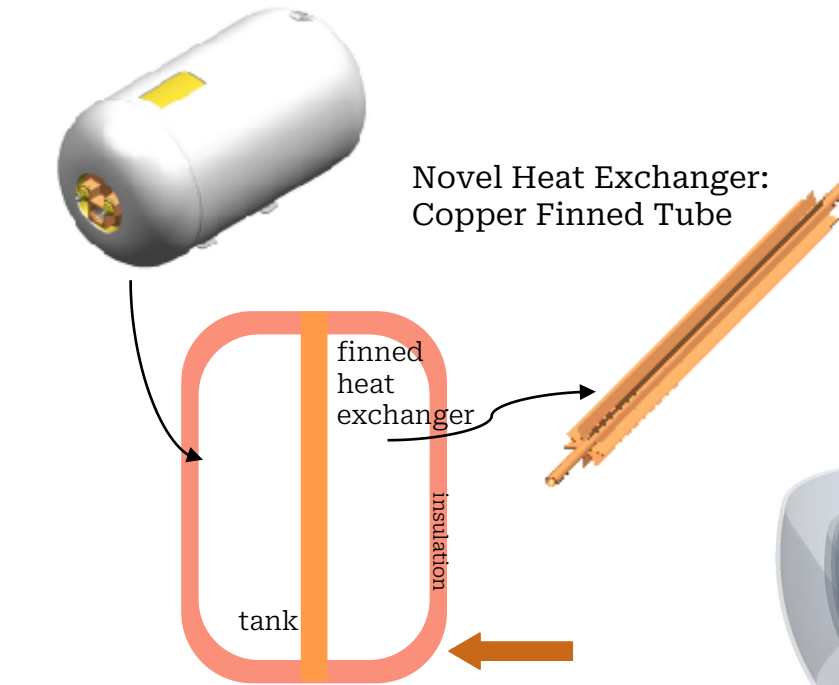
Comparison between CFD predicted mass flow rate and manufacturer curves

Validation of methodology by comparison with manufacturer's experimental data.

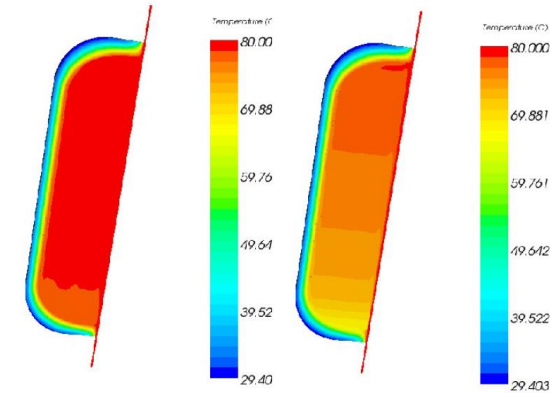


Long Run Thermal Simulations

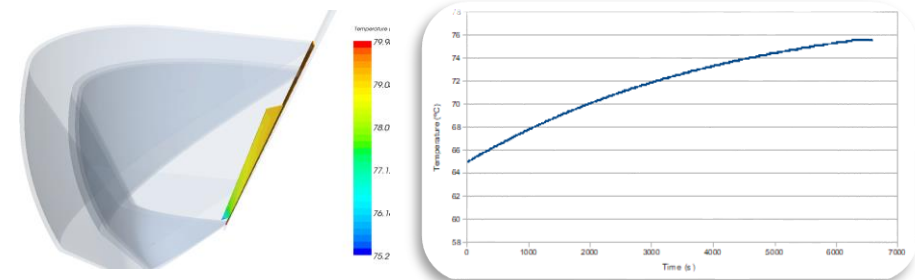
Objective → Study transient thermal performance of a Hot Water Storage tank and characterize stratification.



Thermal inertia very high. A new approach was necessary to simulate 24h of real time. Matlab/Simulink based



Tank temperature results – steady state simulation (left); transient simulation after 1h50m of simulated time (right)

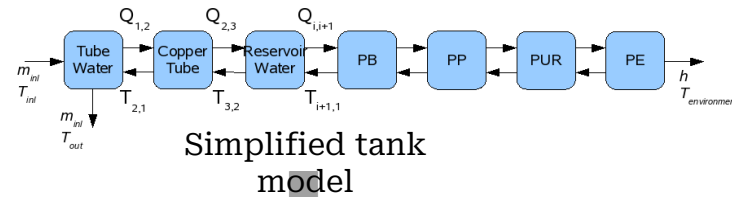


Transient simulation after 1h50m of simulated time: finned tube temperature (left) and evolution of reservoir water averaged temperature (right).

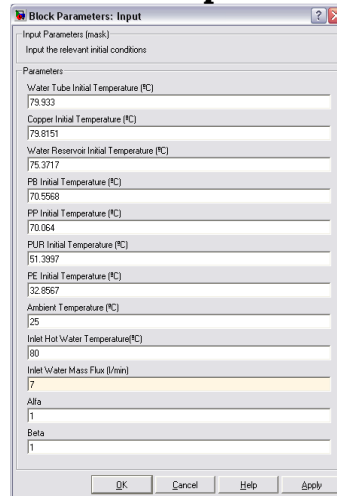
1D Thermal Simulations

Objective →

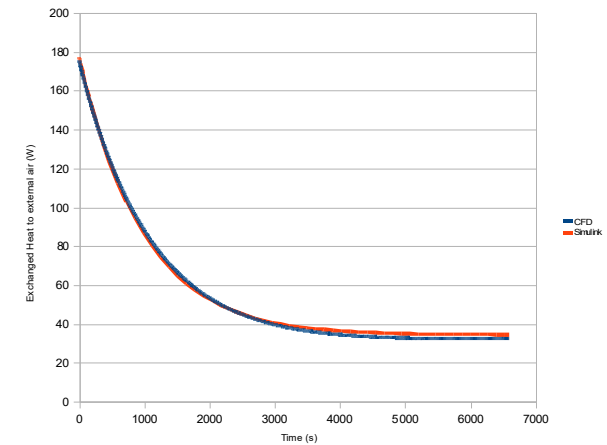
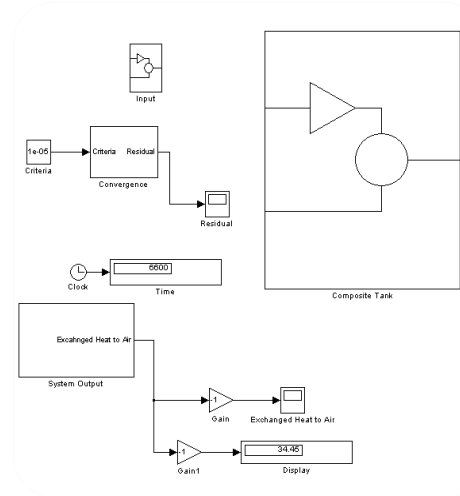
A simplified **Matlab/Simulink** model was developed to represent the tank and simplify transient calculations.



Simulink input



Simulink model



Model validation: Exchanged Heat to External air, CFD vs Simulink results for 1h50m of simulated time.

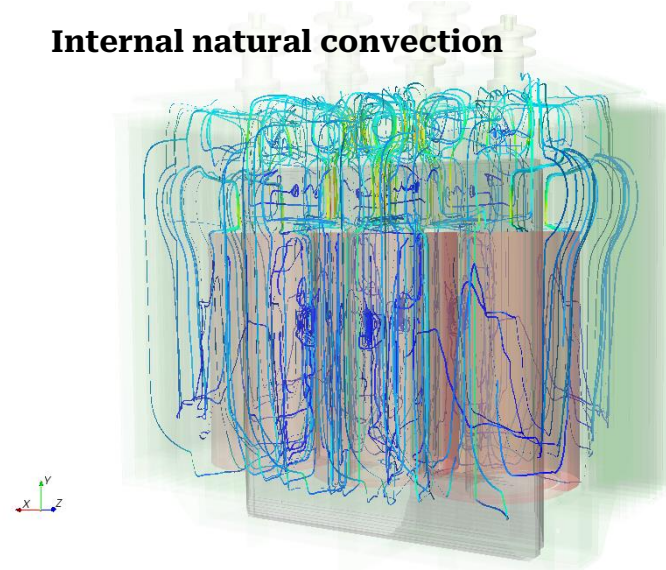
Allows substantial savings in simulation time (hours vs weeks).

Transformer

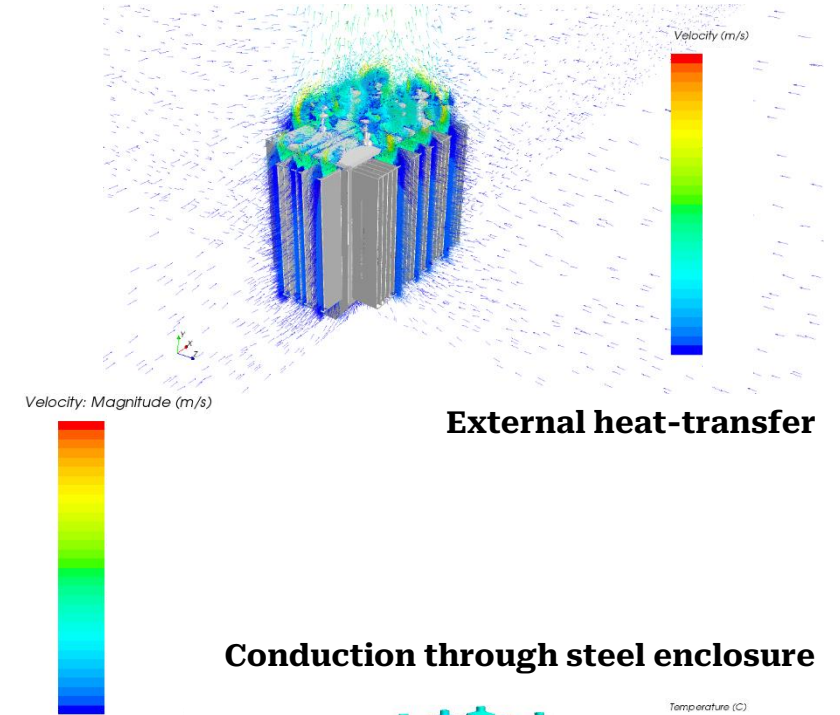
Objective →

Manage thermal load of power transformer, considering all heat transfer modes and physical domains

Internal natural convection

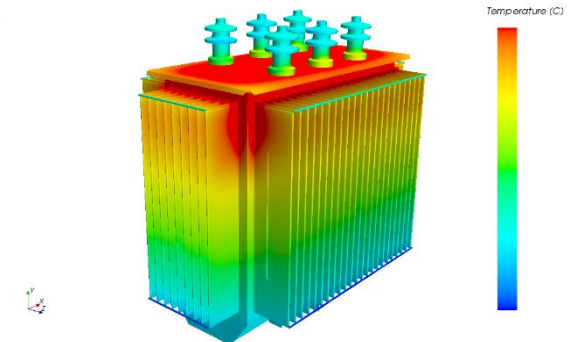


Electromagnetic effects were not considered but all heat dissipation and insulation components were modelled to adequately model reality.



External heat-transfer

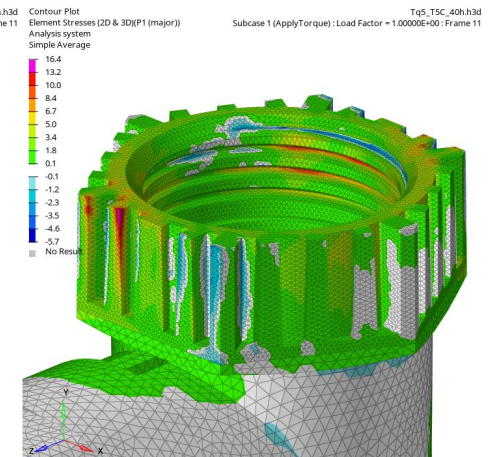
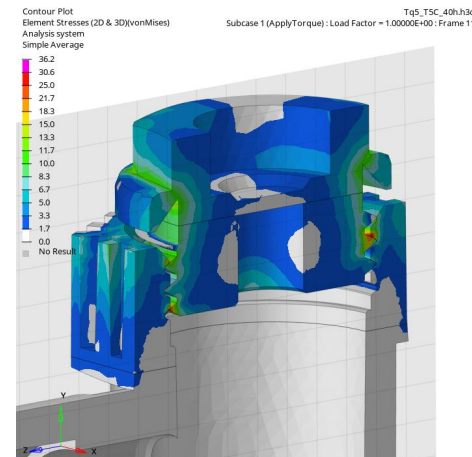
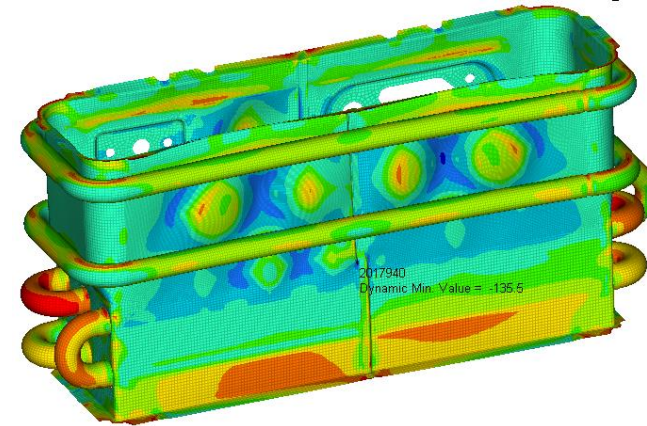
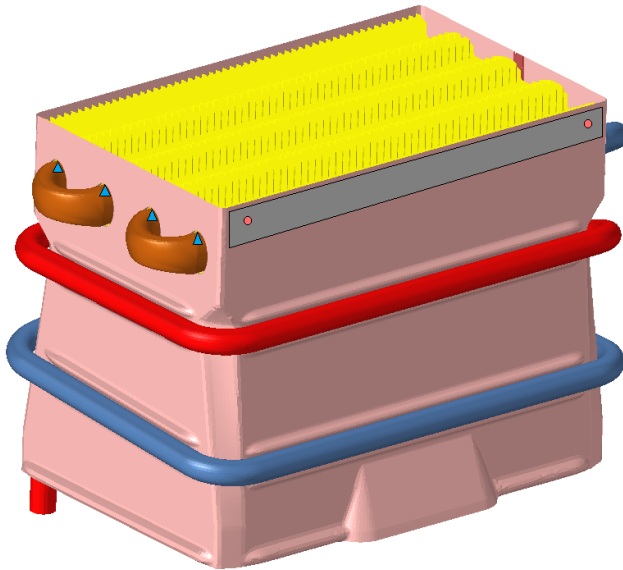
Conduction through steel enclosure



Water heater - FEM

Objective

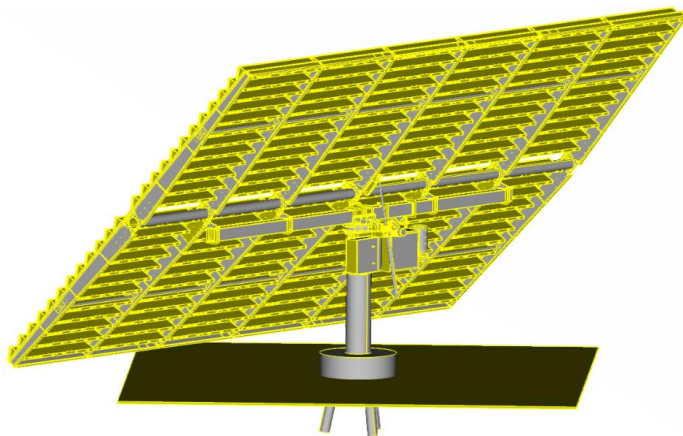
Thermal and structural optimization, fatigue life analysis of water heaters and hydraulic components.



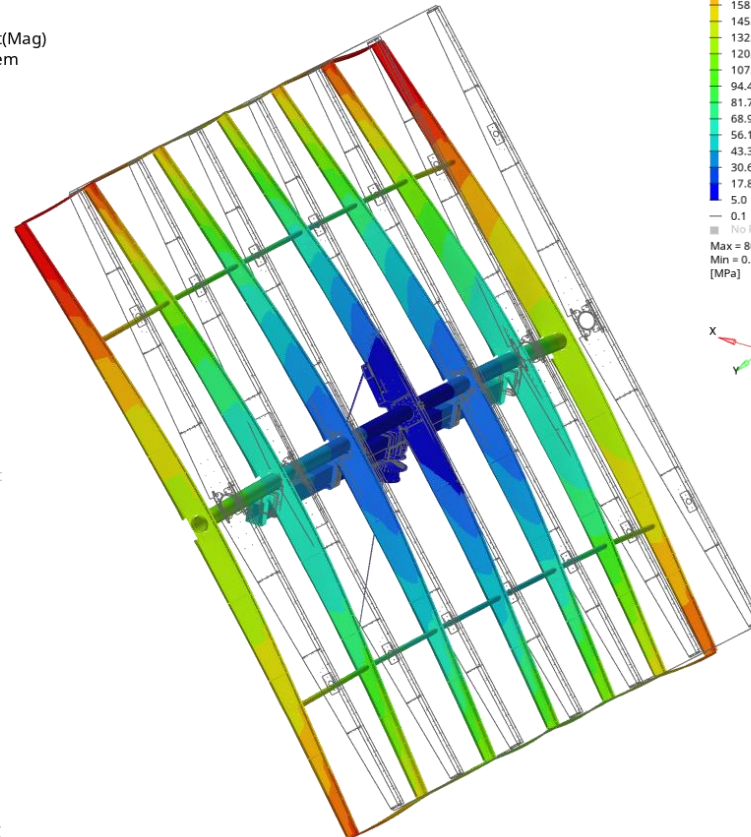
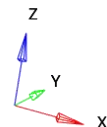
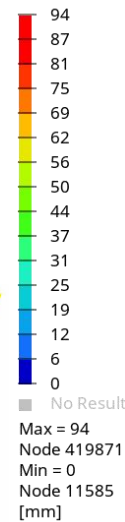
Hydrogen generator - FEM

Objective

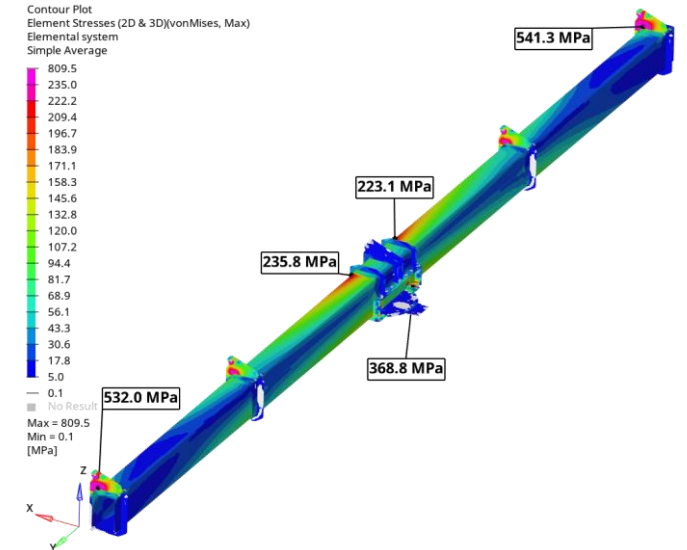
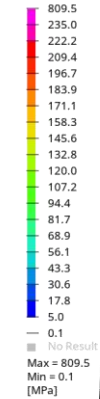
Structural validation and optimization of an innovative semi-movable solar hydrogen generator concept.



Contour Plot
Displacement(Mag)
Analysis system



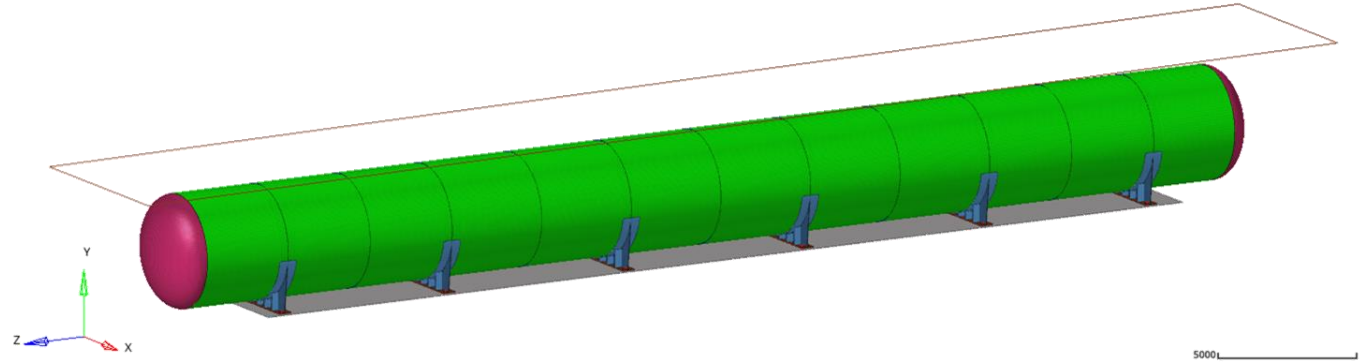
Contour Plot
Element Stresses (2D & 3D)(vonMises, Max)
Elemental system
Simple Average



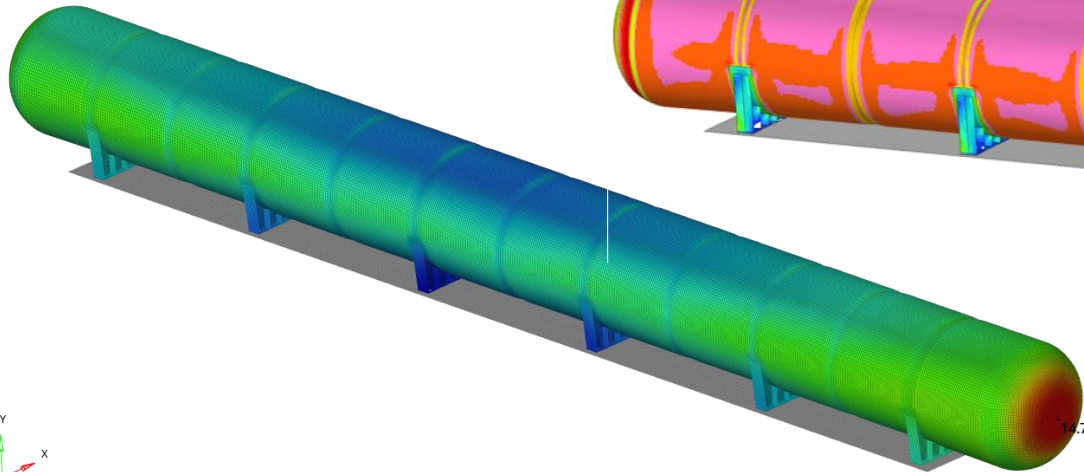
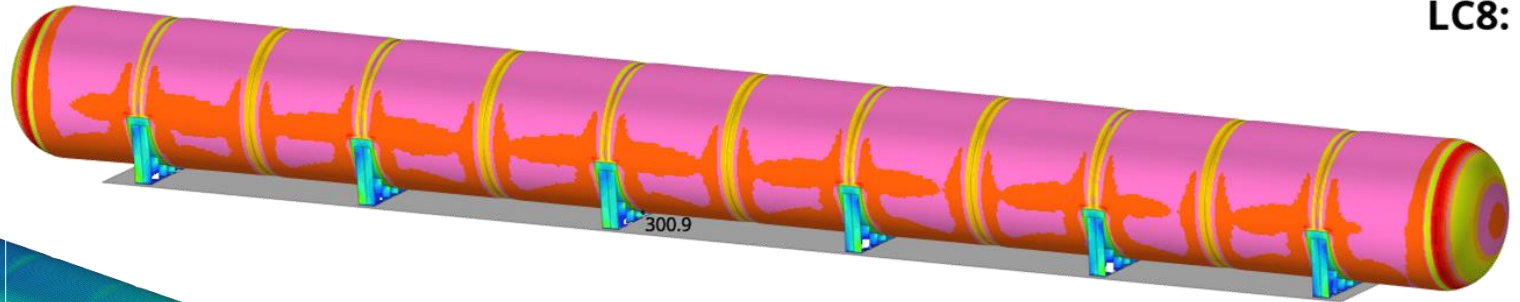
Mounded pressure vessels - FEM

Objective

Mounded pressure vessels structural validation for test loads, operative loads and seismic loads.



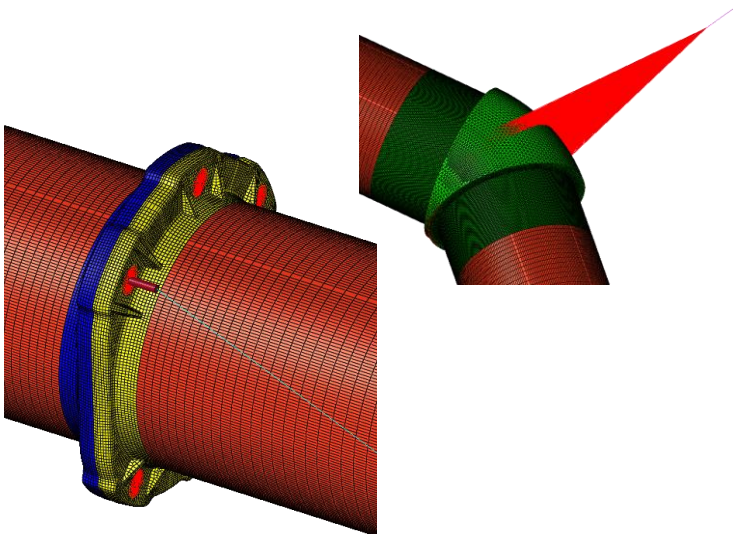
LC8:



Floating solar plant - FEM

Objective

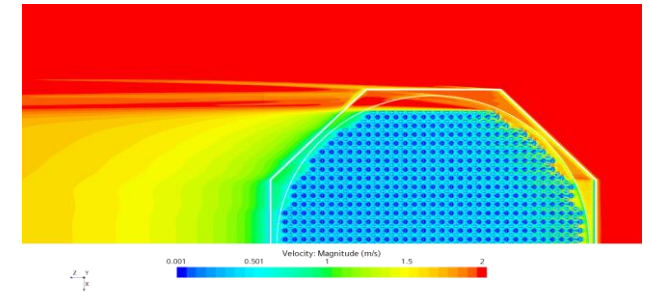
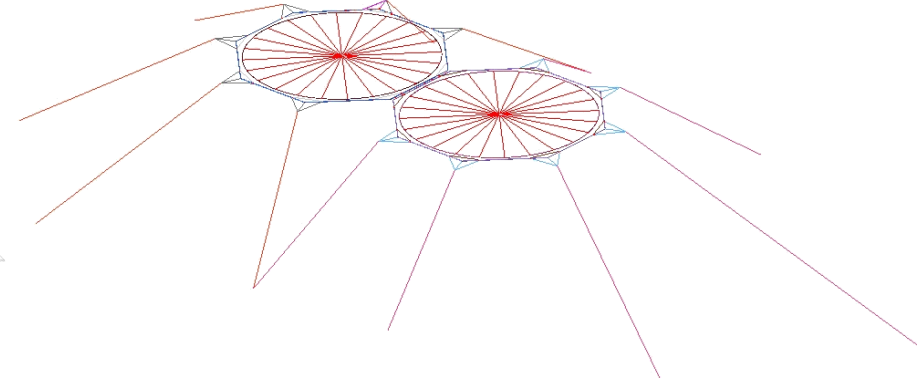
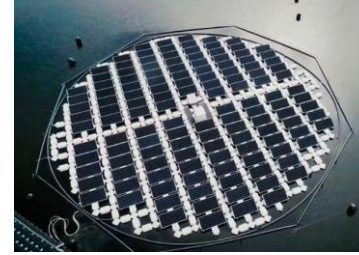
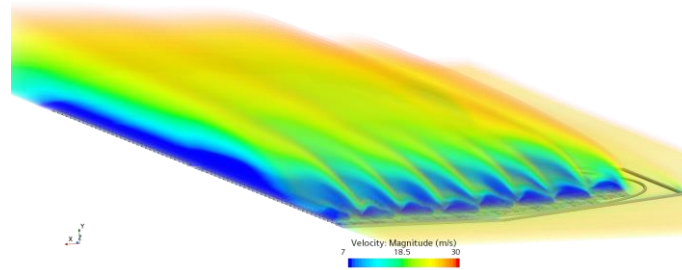
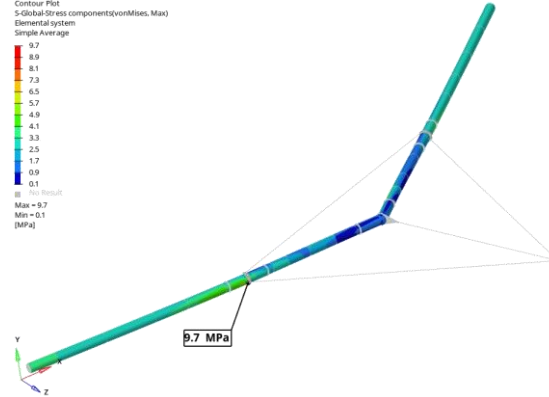
Aerodynamic and hydrodynamic forces calculation (CFD), mooring reaction forces and structural calculations of an innovative floating solar plant concept.



Contour Plot
S-Global Stress component (vonMises, Max)
Elemental system
Simple Average

9.7
8.9
8.1
7.3
6.5
5.7
4.9
4.1
3.3
2.5
1.7
0.9
0.1

Max = 9.7
Min = 0.1
(MPa)

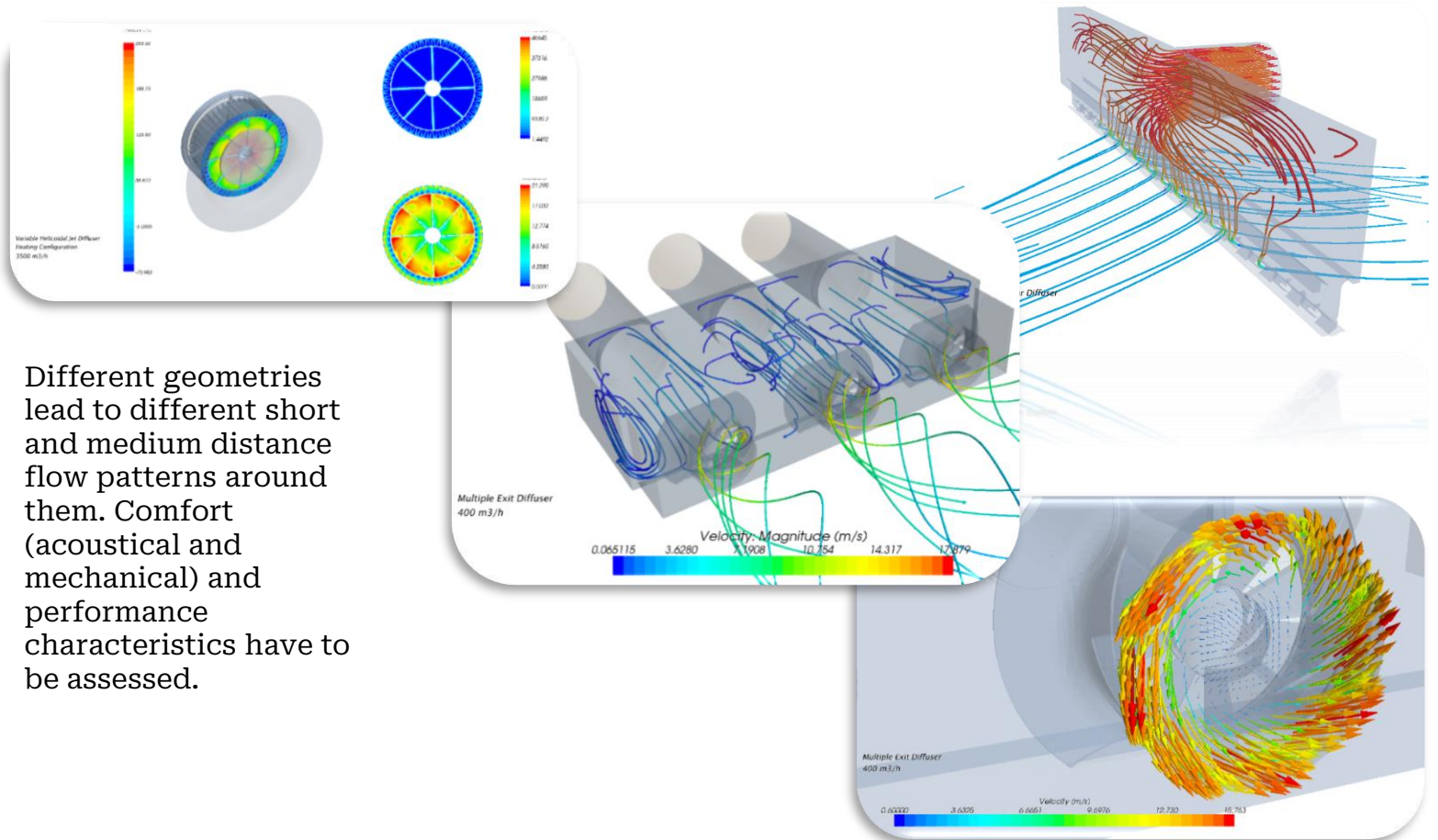


Transport
Energy
Electronics
Wastewater
H.V.A.C.
Biomedical
Process
Machinery

Ventilation Components

Objectives →

- Provide detailed insight into convective and diffusive transport mechanisms;
- Aid in the development of new, high-tech, insuflation registers.



Underground Car Park Ventilation

Objectives →

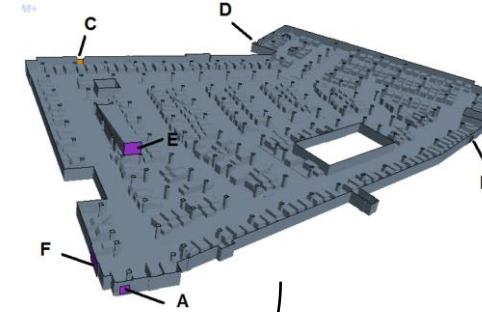
- Validate simulation methodology against experimental values;
- Develop and deploy automatic optimization technique to better explore design space

Level of interest in car park, zoned

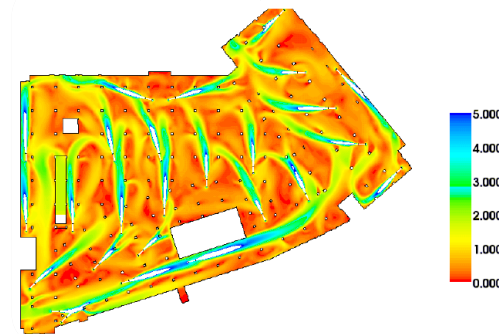


Underground car parks are normal fixtures in large commercial spaces. Besides insuflation and extraction fans, full-scale air motion can be secured through additional fans placed in the ceiling. Their number and placement is critical.

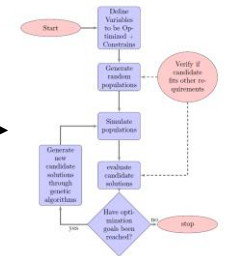
Car park (full) with inlet and outlet boundaries



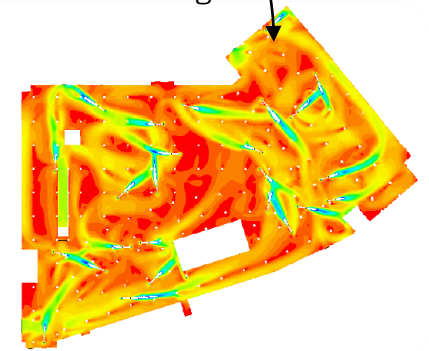
Usual iterative design approach



Automatic Optimization



Optimization based on minimizing maximum air-age.



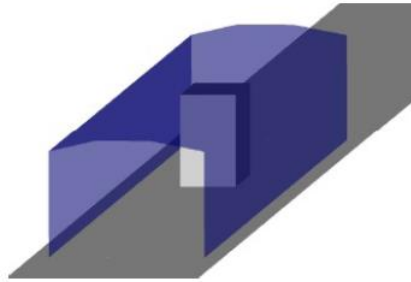
Road Tunnel Safety

Objective →
Benchmark CFD
simulation
approach as a
Design Tool for
Tunnel Engineers

Runehamar Fire Tests Simulations



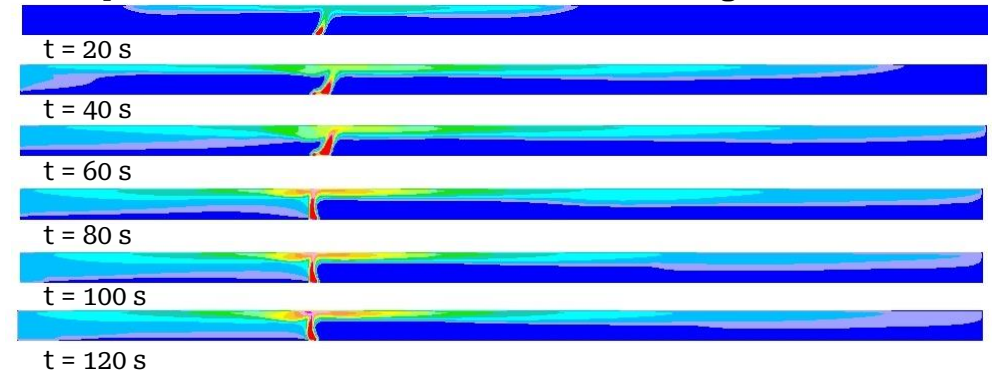
Fire source and protective lining



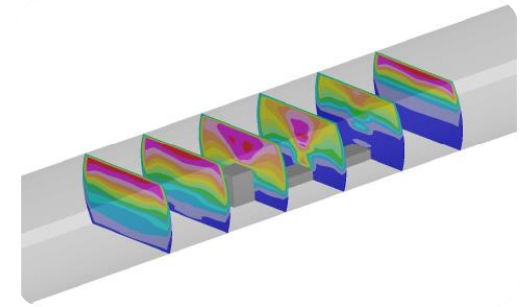
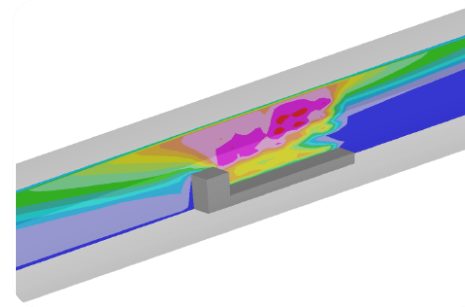
HGV with wood pallets load on fire:

1. Peak HRR of 200MW;
2. $T_{\max} \sim 1300^{\circ}\text{C}$

Temperature contours at mid-section for increasing time:



Good agreement with experimental results!

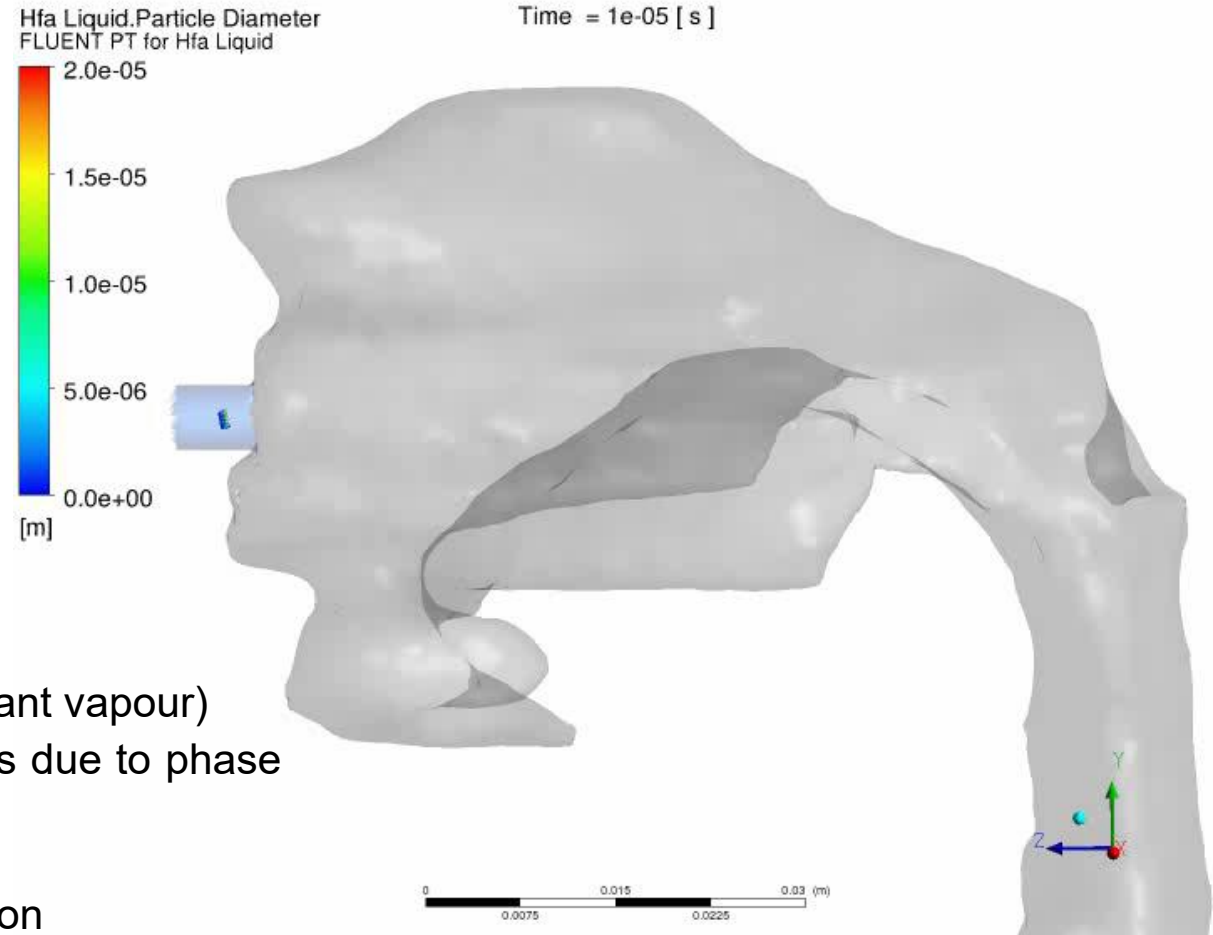


Transport
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Machinery

pMDI spray



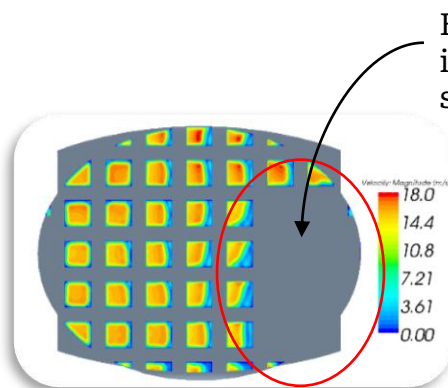
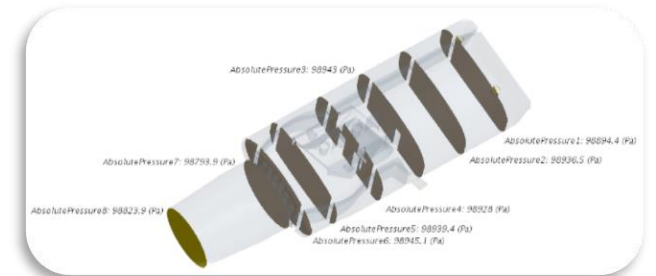
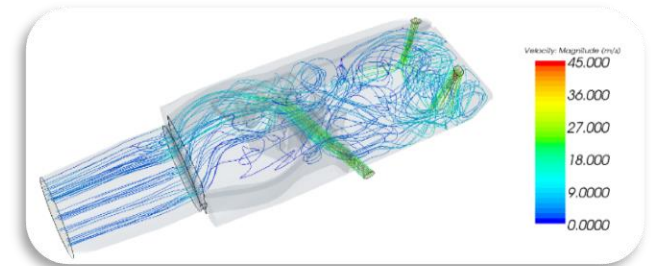
- 2-way coupling (droplets also affect carrier fluid)
 - Momentum transfer (in both directions)
 - Mass transfer (droplets evaporate into propellant vapour)
 - Heat transfer (heat is taken from surroundings due to phase change)
- Gas mixture (air + propellant)
- Models available for droplet break-up and collision
- Atomization process is very complex (assume particle size distribution at nozzle exit)



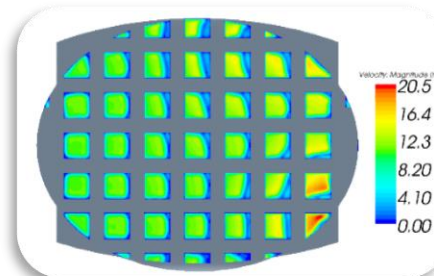
Dry Powder Inhaler (DPI)

Objectives →

- In-depth analysis of fluid flow pattern, totally impossible otherwise;
- Insure effectiveness and stringent efficiency targets;
- Meet cost targets with simplest solution possible.



Blockage is easily incorporated into the simulation process.

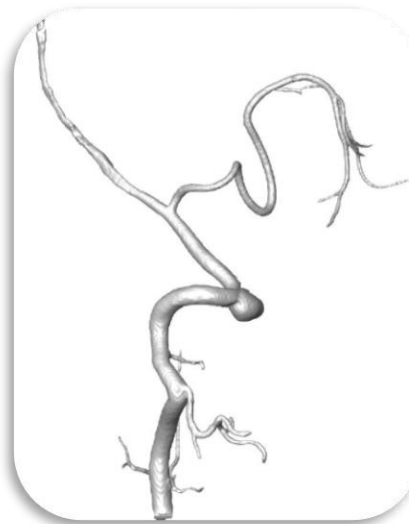


Aneurysm Hemodynamics

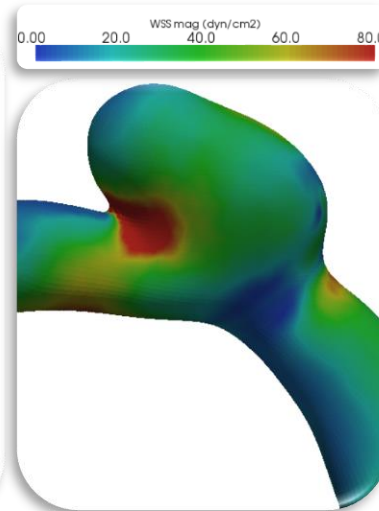
Objective

→ Assess impact of biomechanical parameters on and near vessel walls in the genesis, development and rupture of cerebral aneurysms using patient-specific 3D geometries.

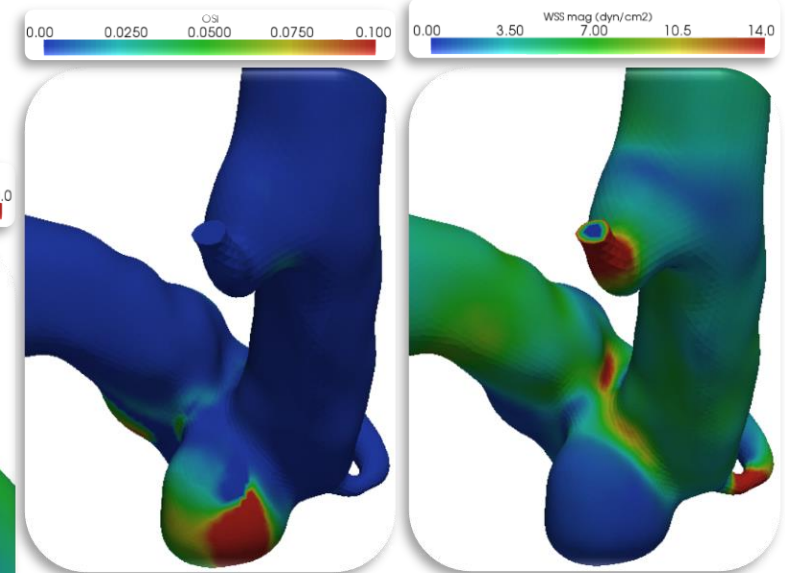
Cerebral aneurysms are more likely to arise at regions with a combination of high WSS and its gradients, such as bifurcations and strong curvatures.



Real life geometry.



Wall shear-stress (WSS)



Oscillatory Shear Index (OSI)

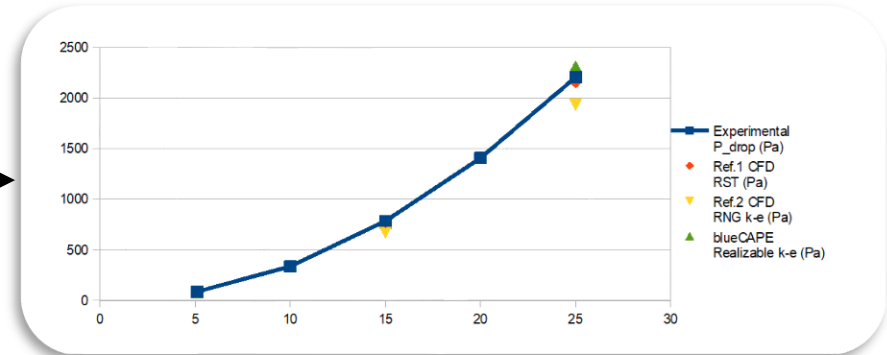
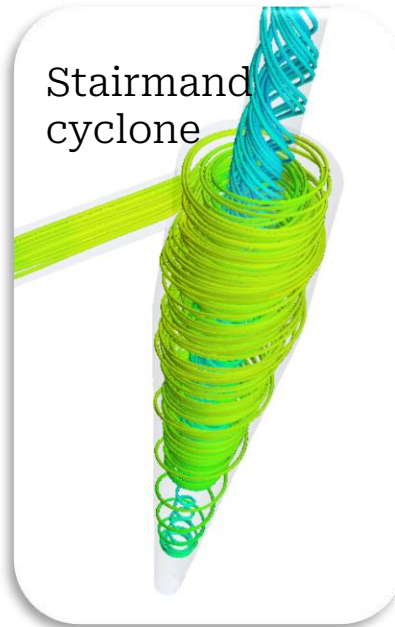
Wall shear-stress (WSS)

Generally, WSS is higher in the neck region and minimal inside the aneurysm, whereas OSI reaches high values both in the neck region and in the aneurysm.

Transport
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Machinery

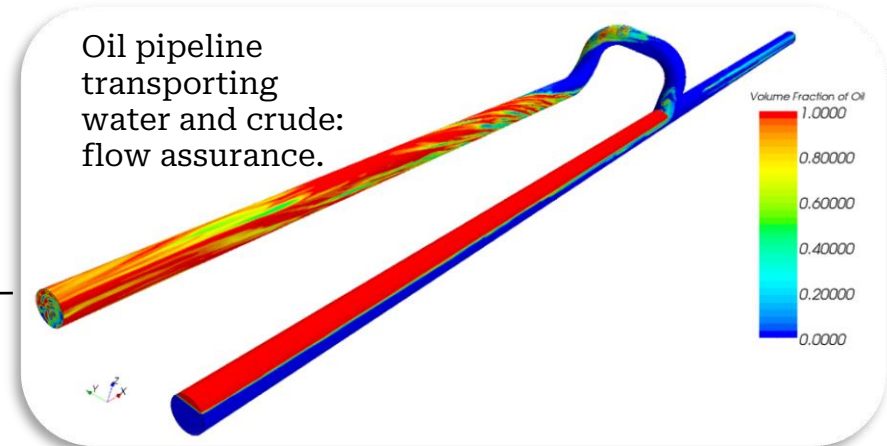
Separation Processes

Objective →
Evaluate
efficiency of
separation
processes



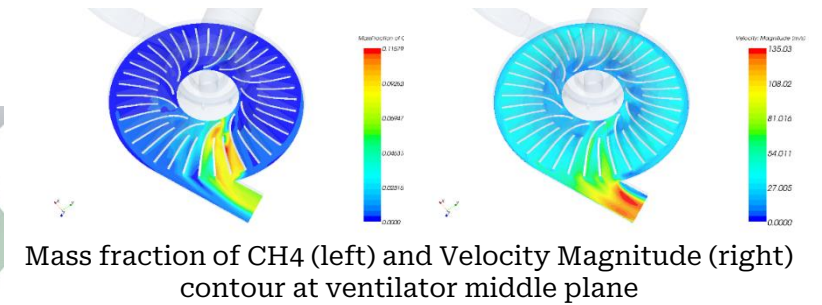
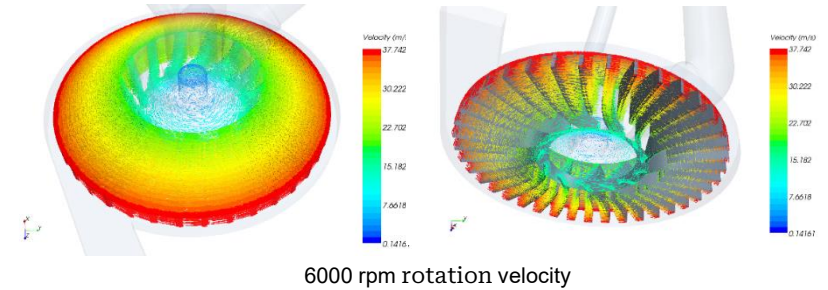
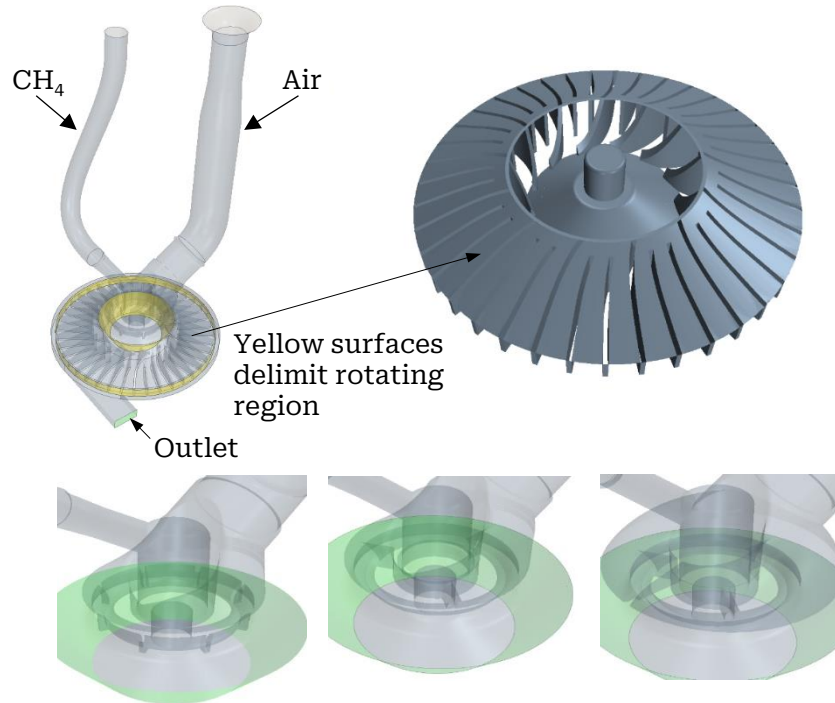
Accurate Results!

Provides insight into
existing or planned
networks, thus validating
solutions and saving costs.



Advanced Mixing

Objective →
Evaluate suction
and mixing
ability of
Methane injector



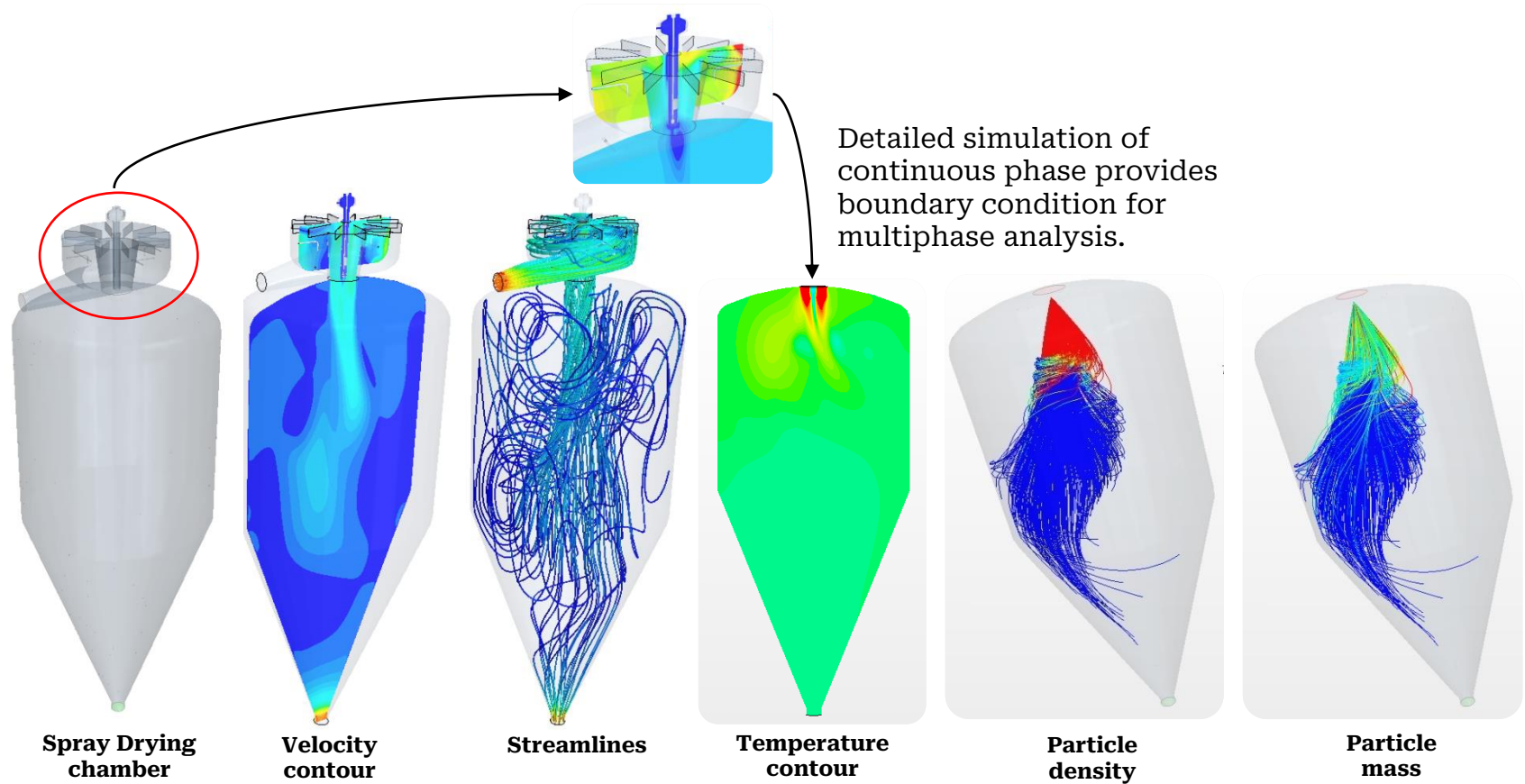
©

Evaluation of different mixer concepts:
→ Pressure drop
→ Mixture quality

Two methodologies to simulate rotation:
MRF – Moving Reference Frames
RBM – Rigid body motion (moving mesh)

Spray Drying

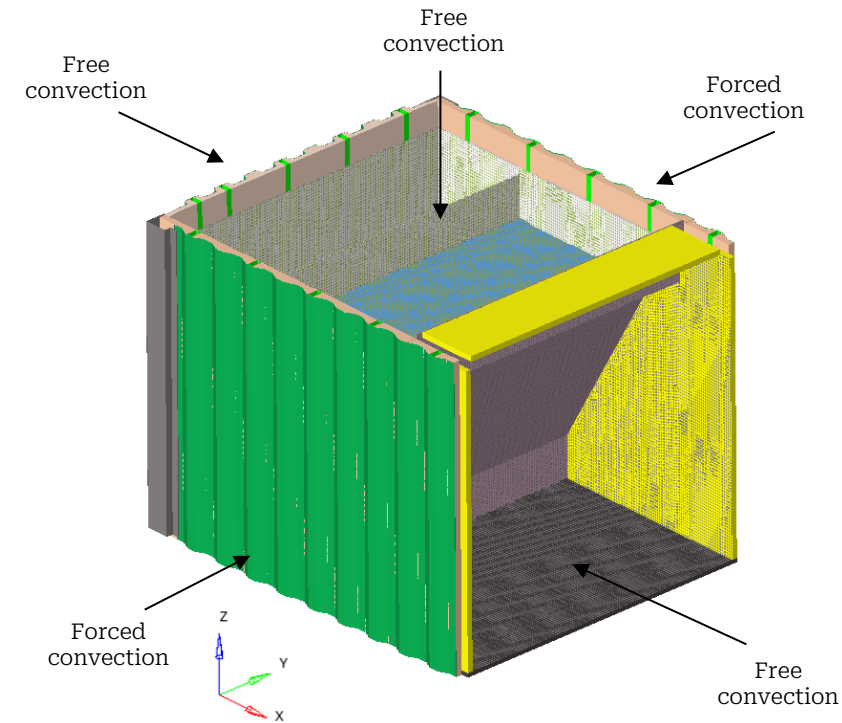
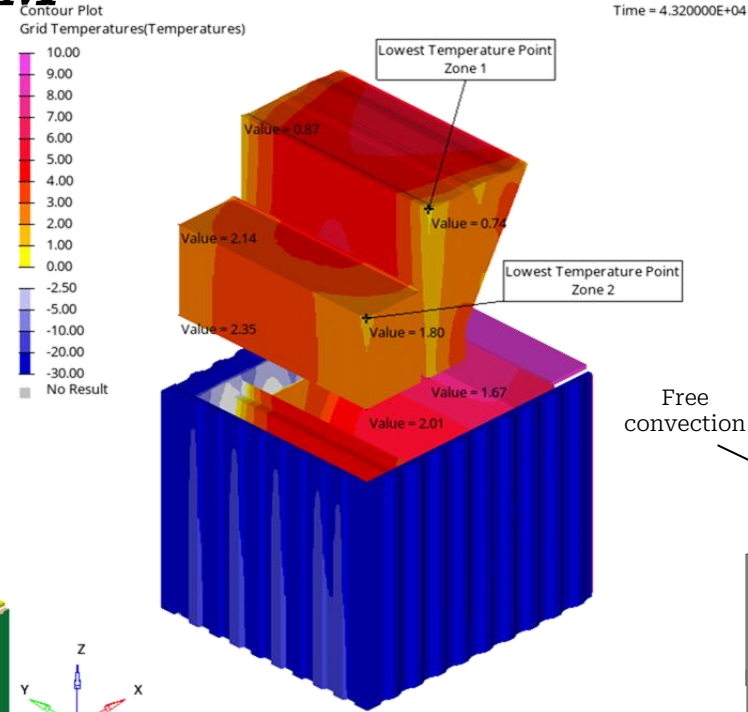
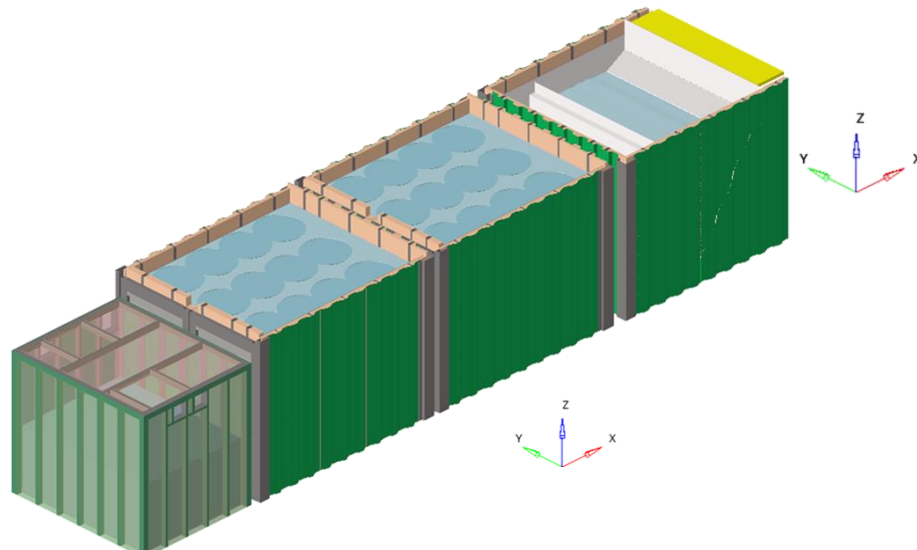
Objective → Evaluate efficiency of spray drying chamber with two-way coupling between continuous and disperse phases.



Portable water tank - FEM

Objective

Study the temperature evolution of the water in a portable water tank and guarantee that no freezing occurs during the required field operation.

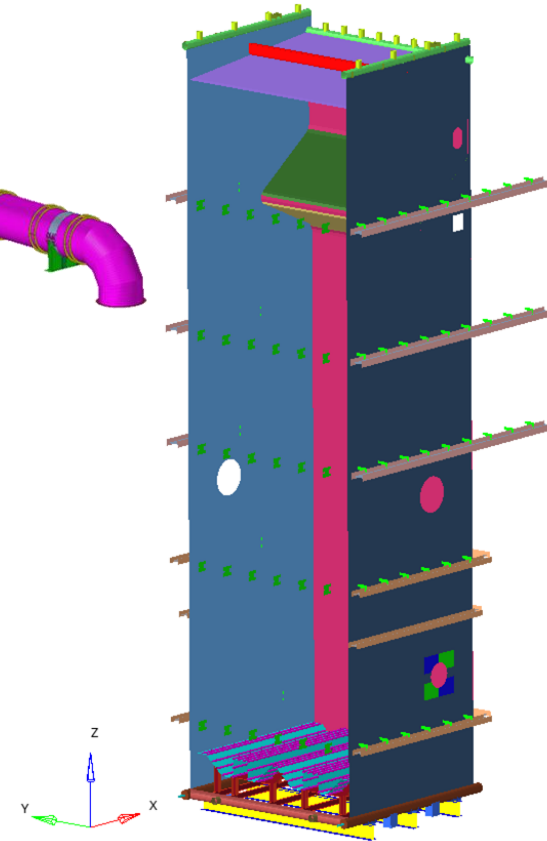
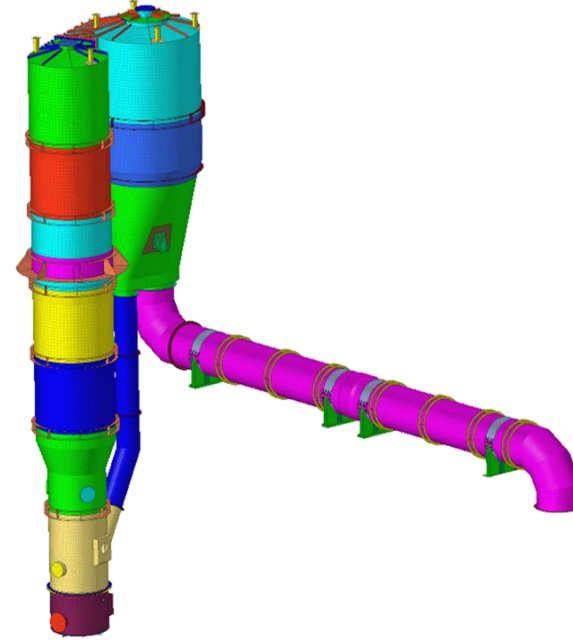
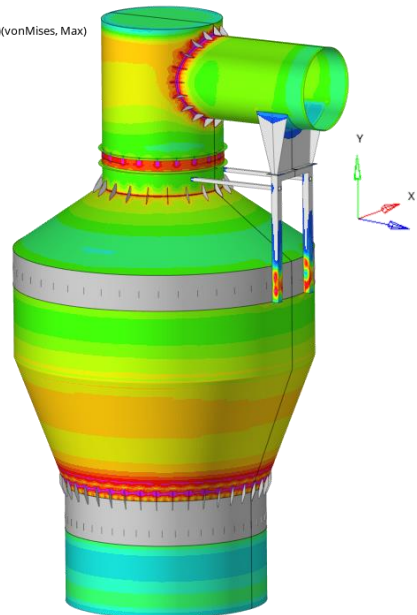
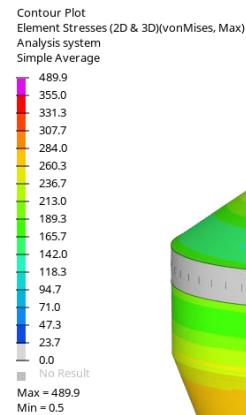


Industrial furnaces - FEM

Objective

Evaluate the structural integrity and stability of big structures under thermal loads, seismic loads and other loads.

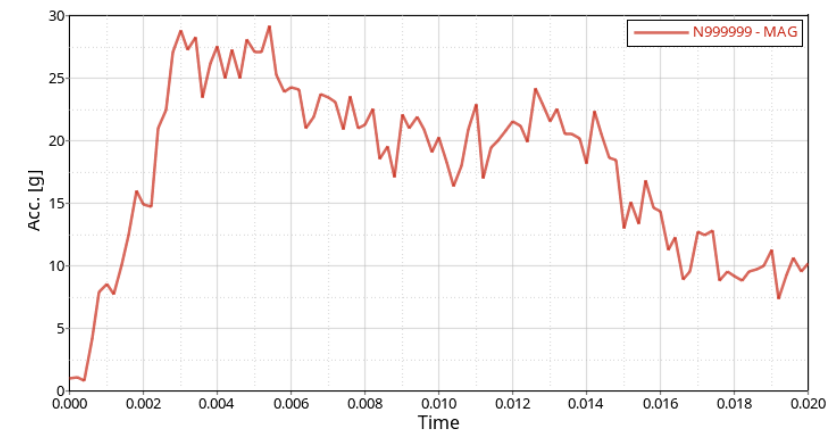
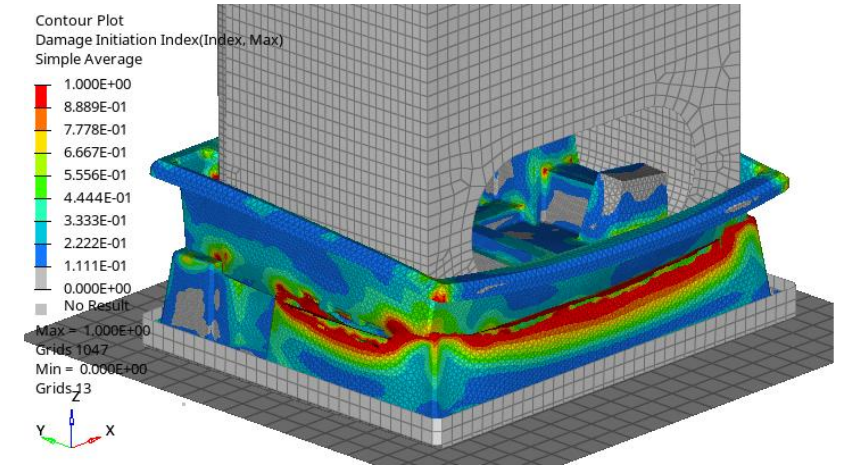
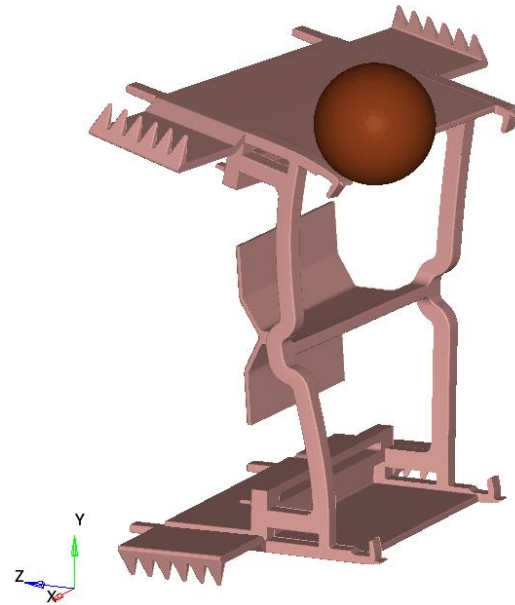
FEA simulations coupled with CFD simulations or subject to the Eurocode norms.



Packaging – Drop test - FEM

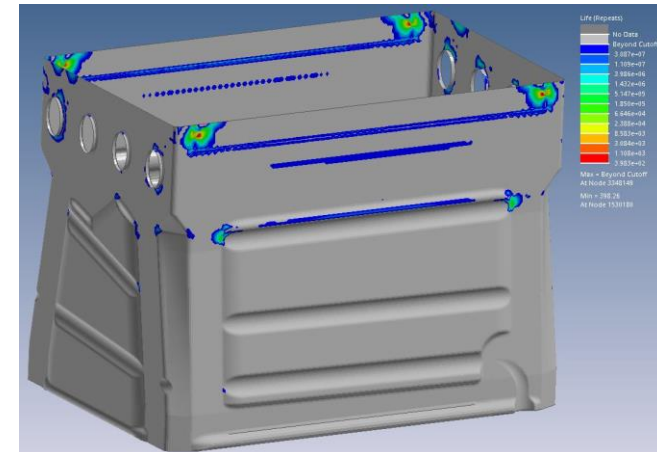
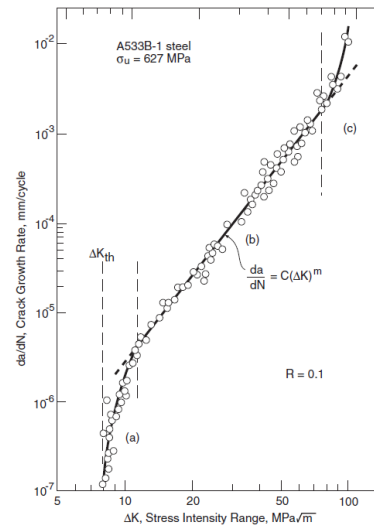
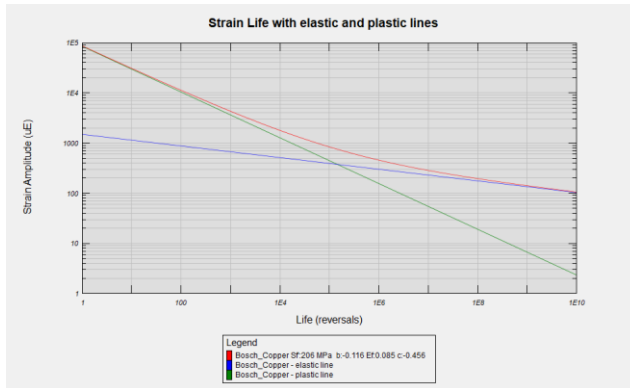
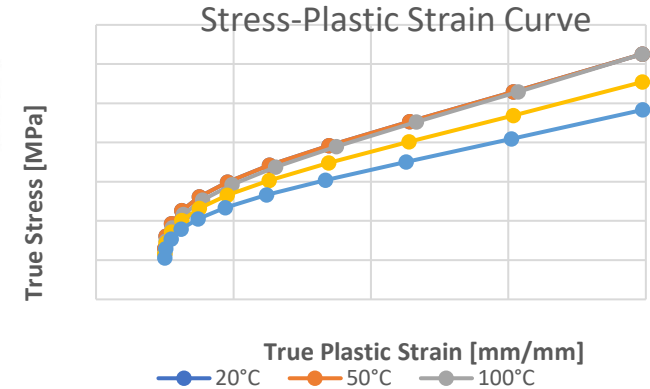
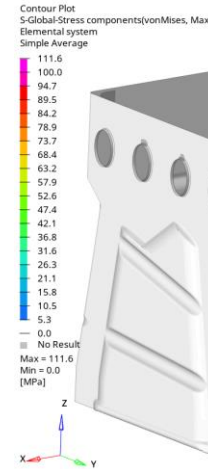
Objective

Evaluate different packaging and parts performances simulating dropping scenarios through explicit dynamic analyses.



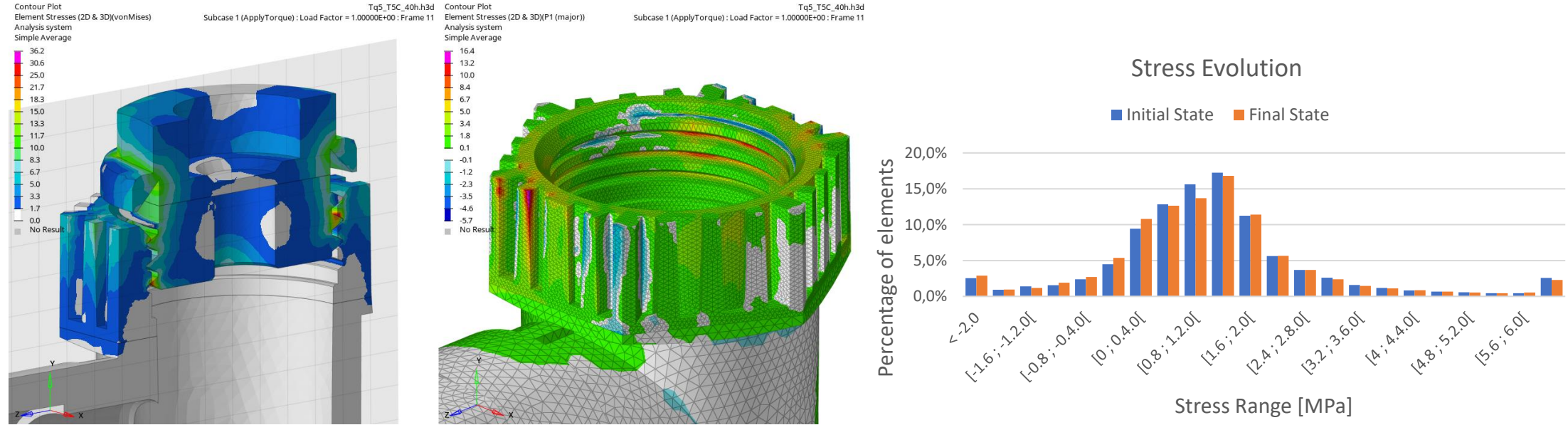
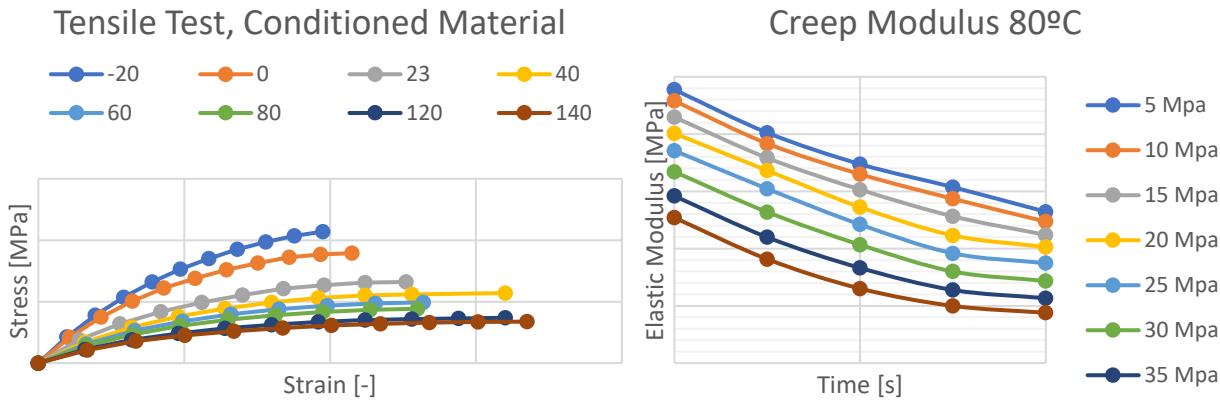
Heat exchangers - FEM

- Transient Heat Transfer analysis
 - 1-way coupled with CFD simulations
- Transient non-linear structural
 - Temperature dependent material's properties
- Low cycle fatigue analysis
- Crack propagation



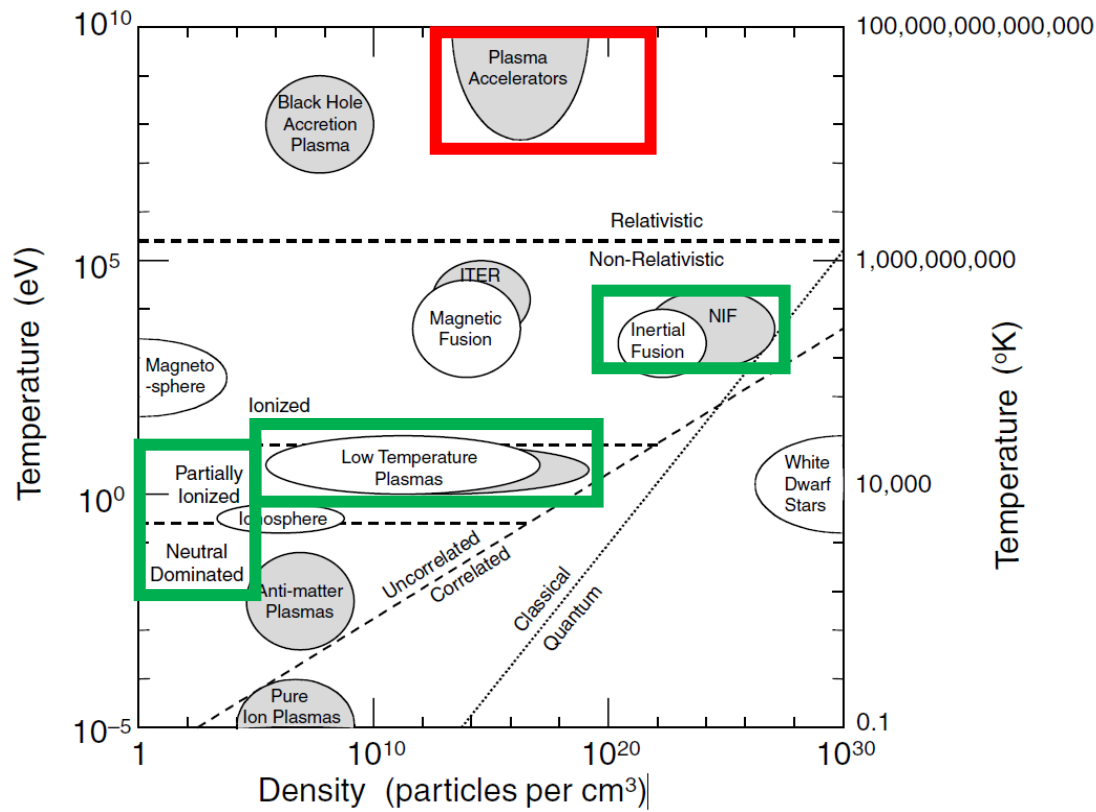
Polymeric components - FEM

- Visco-elasto-plastic material modelling
- Steady-state thermal analysis
- Static non-linear structural
 - Contacts
 - Pre-loaded threaded connection
- Creep and stress relaxation transient

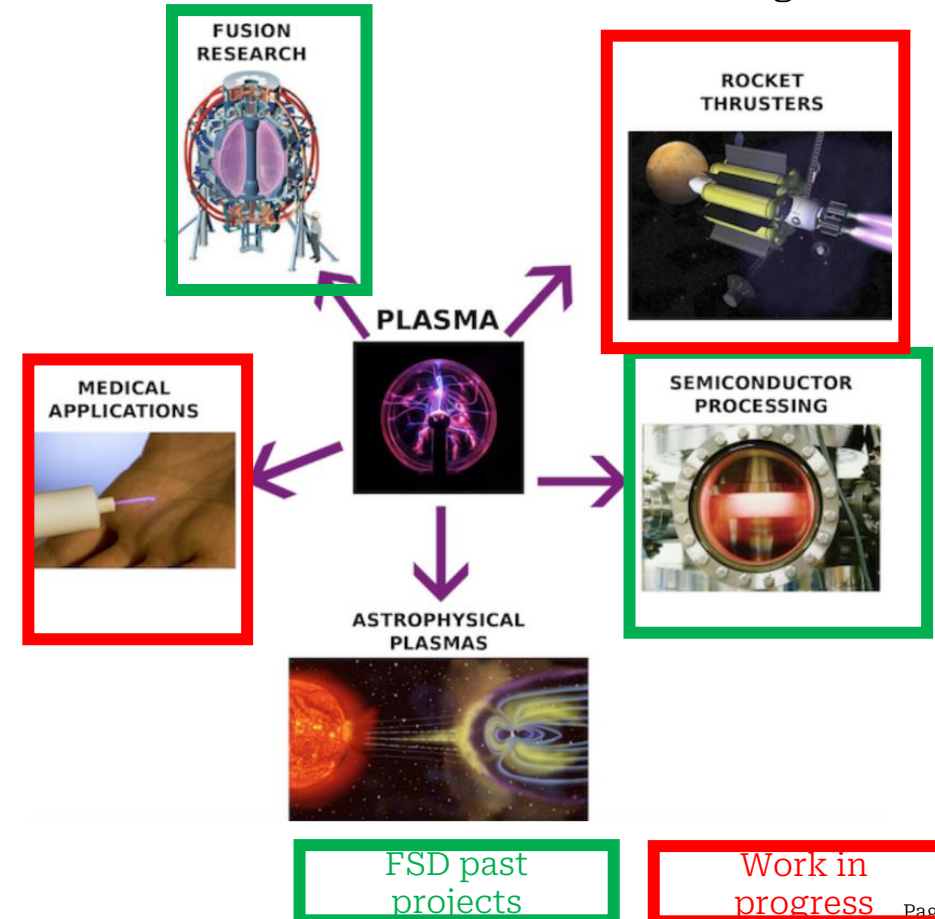


Plasma competence: Modelling of plasma sources and plasma based technologies

Plasma can occur in different conditions

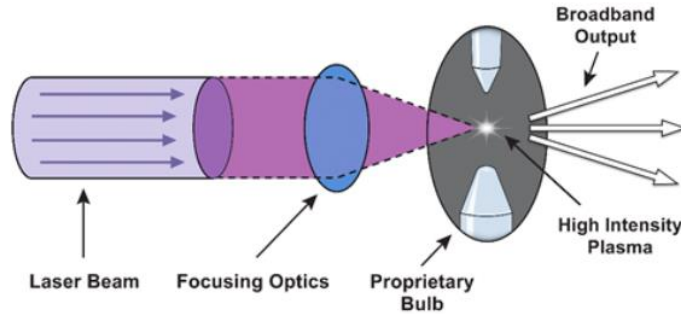


Plasma is used for different technologies



Laser produced plasma sources for broadband emission

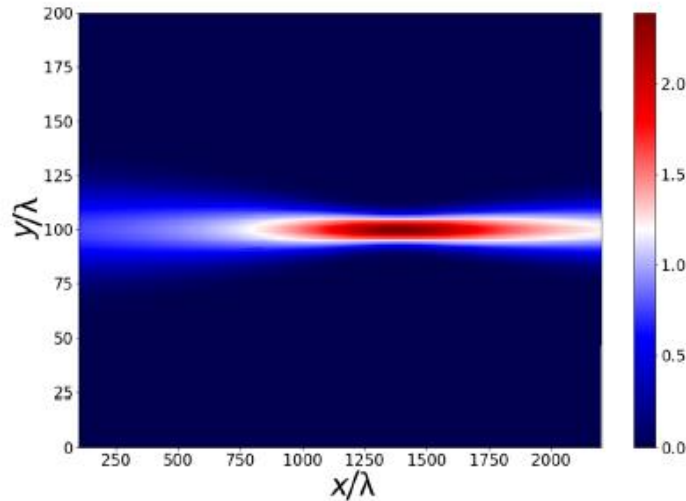
Improvement of source emission via radiative hydrodynamics simulations



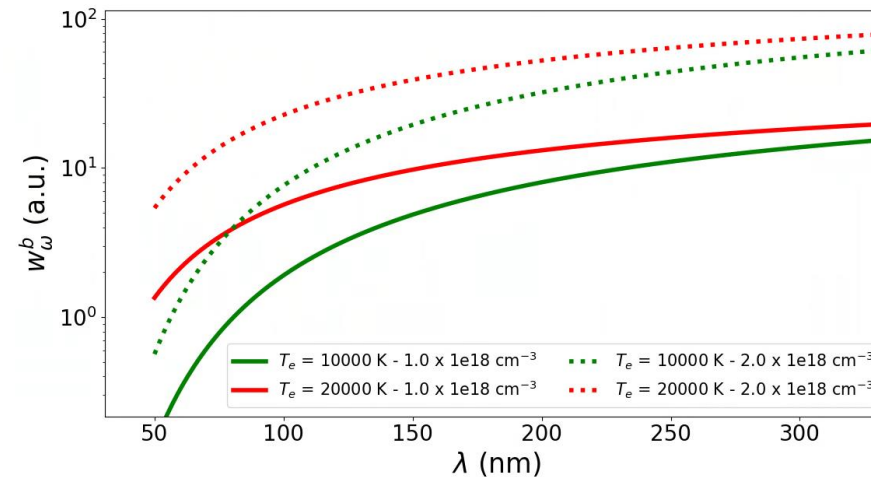
Plasma: single fluid conservation equations
Laser light: ray-tracing equations
Radiation: multigroup equations

Plasma-laser coupling: inverse Bremsstrahlung
Plasma-radiation: EOS and opacity

Laser plasma coupling evolution



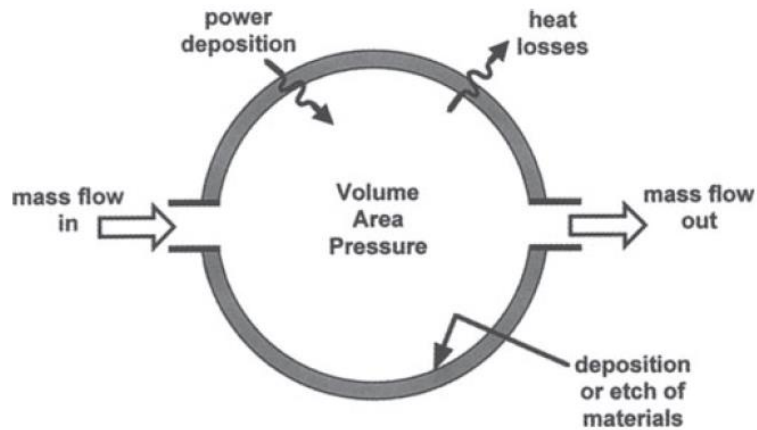
Plasma emission in the VUV regime



Best combination of initial gas density and laser parameters to increase VUV emission

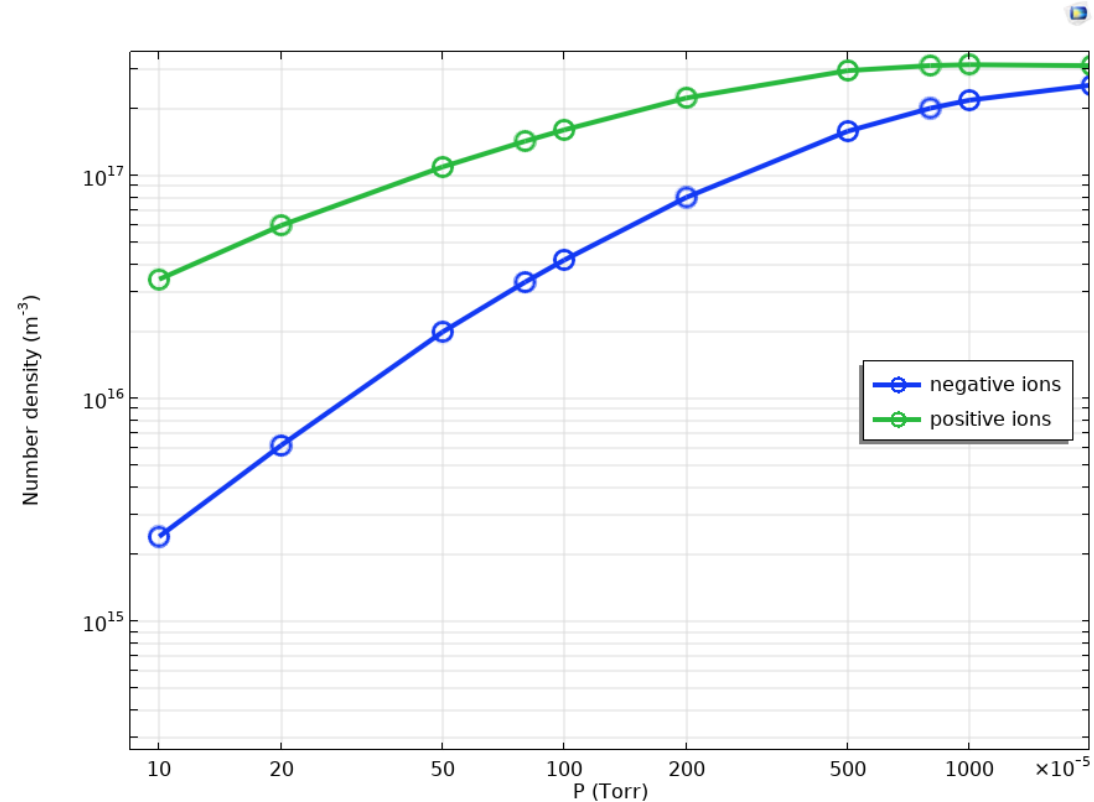
Chlorine etching of silicon with ICP reactors

0d modelling: Finding the range of parameter operation over large interval of pressure



Numerically cheap for large parameter study
Good if chemistry is complicated to understand trends

Plasma chemistry
38 bulk reactions + 8 surface reactions



Negative and positive ions density saturates when approaching 0.1 Torr

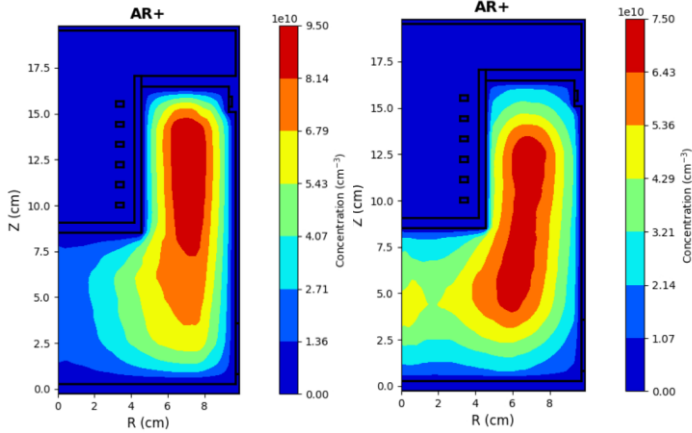
Capacitive coupling of ICP coils at low current

Hybrid modelling of ICP including capacitive coupling retrieves theoretical results

$I = 0.1 \text{ A} - W = 4 \text{ W}$

CC on

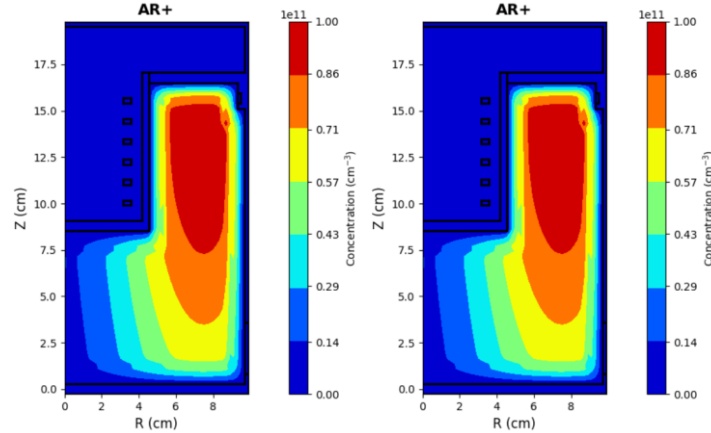
CC off



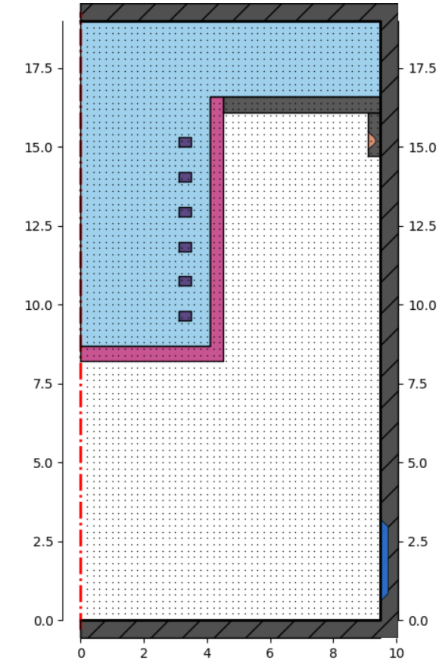
$I = 10 \text{ A} - W = 400 \text{ W}$

CC on

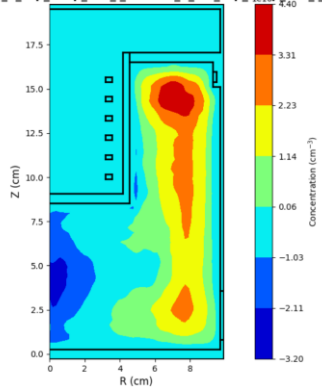
CC off



Reactor geometry

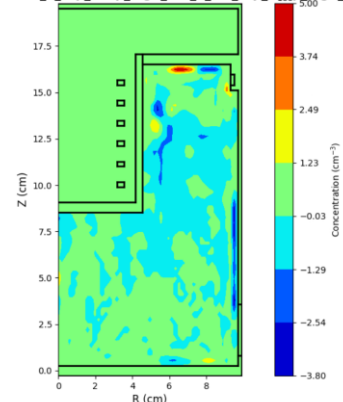


Diff. Plot: E (f_1_ccp_coup_low_i_NEW - f_1_NO_ccp_coup_low_i_NEW)



Max
difference
~50%

Diff. Plot: E (f_1_ccp_coup_high_i - f_1_NO_ccp_coup_high_i)

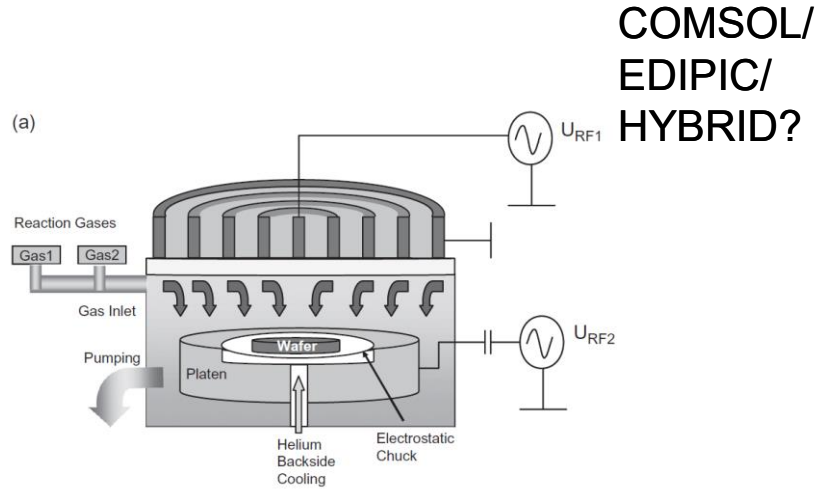


Max difference
~0.05%

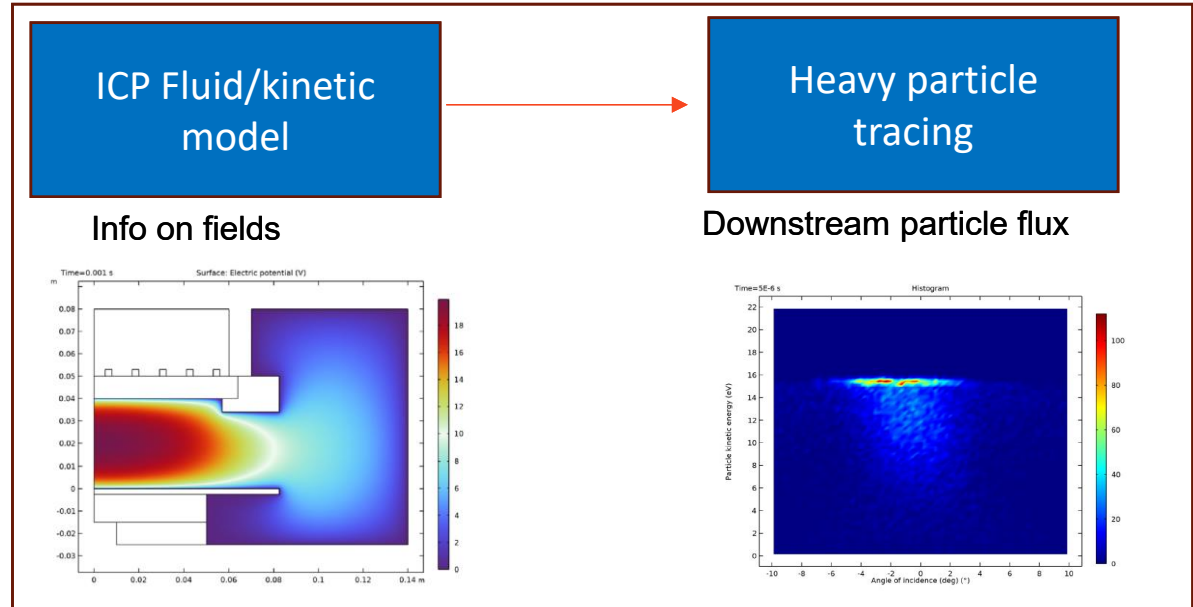
Capacitive coupling plays
important role at low
currents, observed via
hybrid modelling

Multi-scale modelling of plasma etching – JUST STARTED

Coupling MHD and molecular dynamics tools to obtain information on feature profile modification

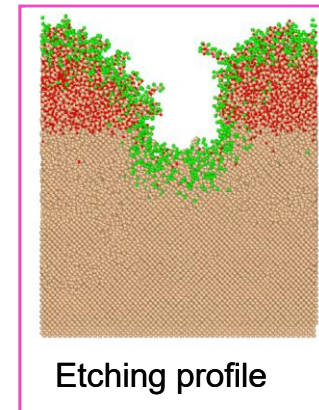


COMSOL/
EDIPIC/
HYBRID?



Varying gas flow and density, and RF power

Molecular dynamics simulation predicting the profile modification based on molecular interaction among substrate, coating and ions.



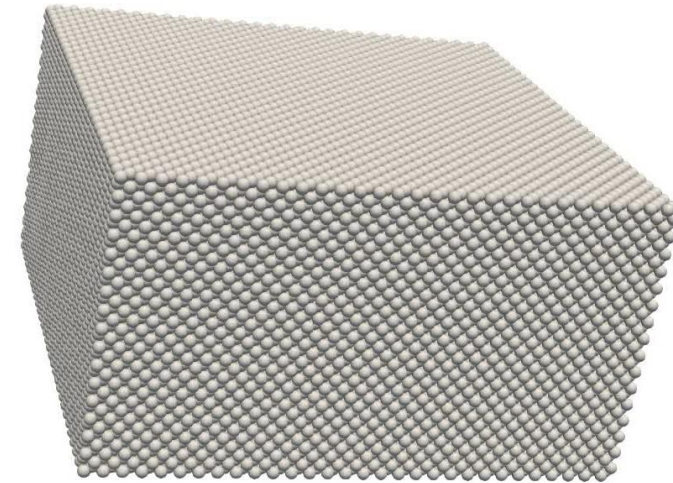
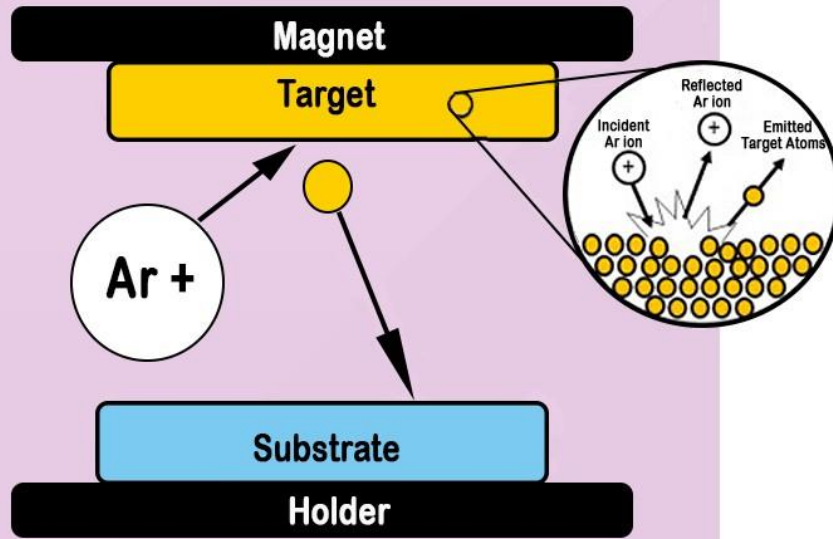
LAMMPS

Molecular Dynamics for PVD with Sputtering

FS x DYNAMICS

Sputtering is a physical vapor deposition (PVD) process used to create thin films on a substrate. In this project, FS Dynamics experts analyze different parameters to improve the thin film deposition of titanium on top of the nickel substrate.

Only for illustration purposes



Simulation is performed using Opensource code LAMMPS. However, different applications might require different software solutions. And our team of expert can advise.

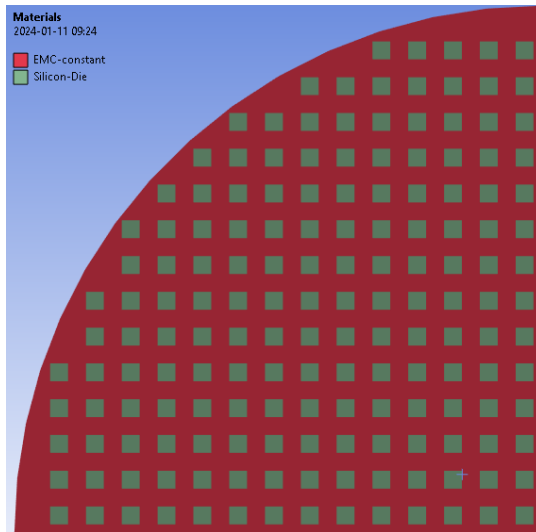
Transport
Energy
Electronics
Wastewater
H.V.A.C.
Biomedical
Process
Machinery

Wafer Warpage Prediction

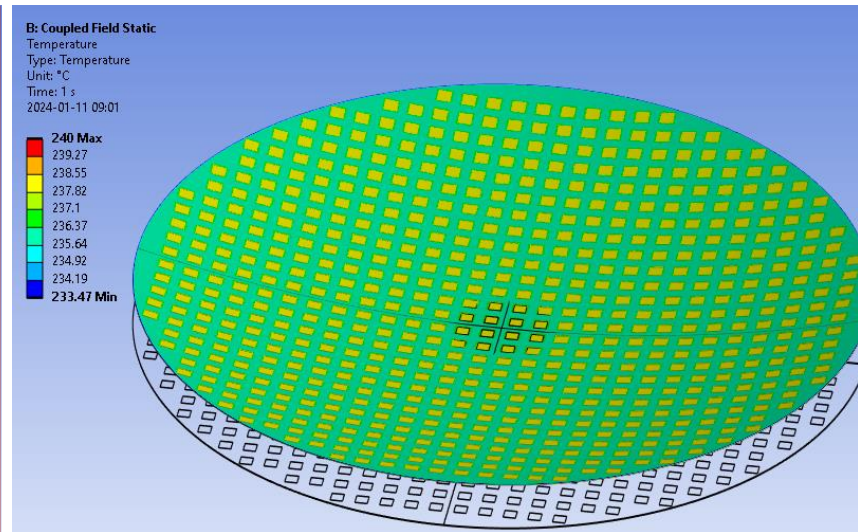
Prediction of wafer warpage has emerged as a critical aspect in ensuring the success of the chip packaging process. Understanding and accurately predicting this warpage is essential for several reasons:

reliability and performance, yield enhancement, advanced packaging technologies, Cost Efficiency and Process Optimization.

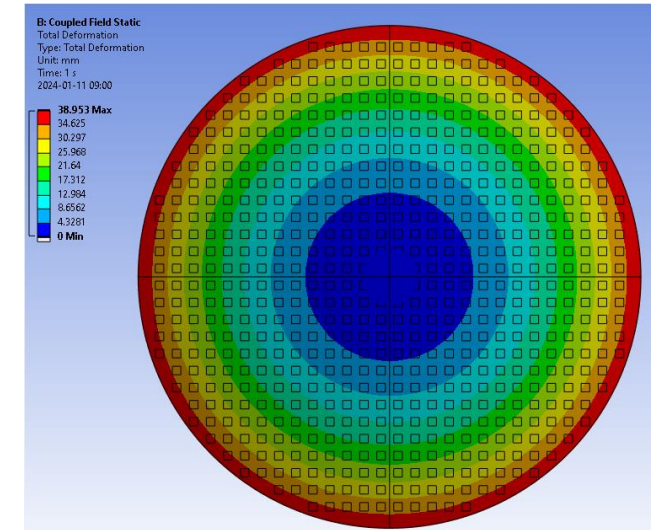
Geometry/Layout



Temperature



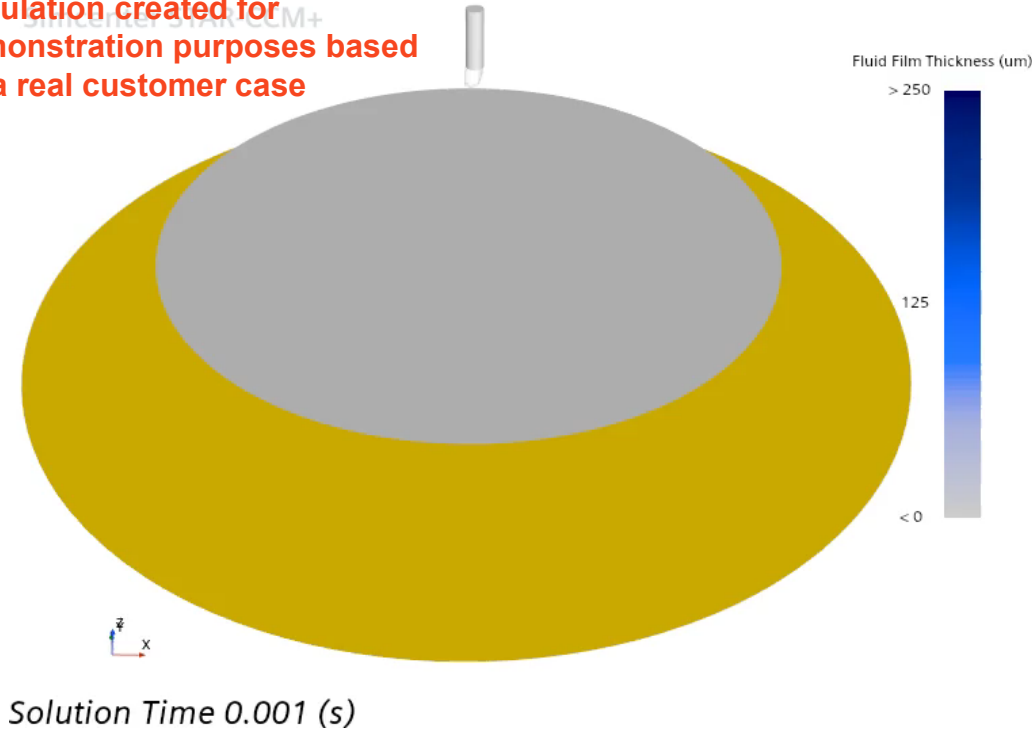
Deformation



Finite element analyses (FEA) facilitate prediction with high confidence by use of high fidelity in geometrical models, material characteristics, process and environmental boundary conditions. FEA also serves as a foundation for validation with experimental data.

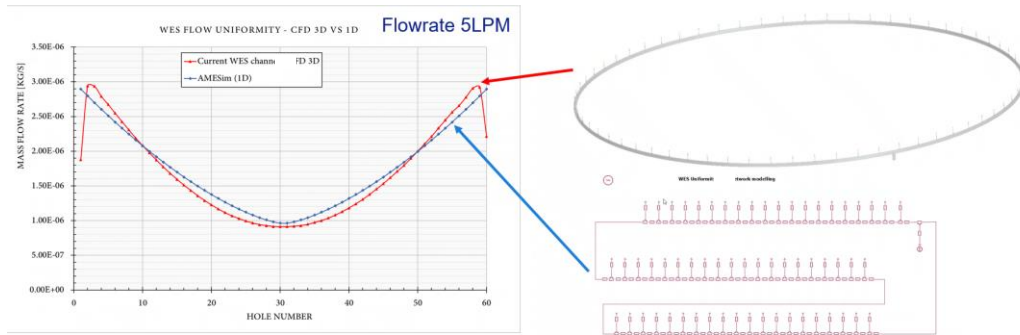
Objective → Evaluate the film thickness as function of different parameters.

Simulation created for
demonstration purposes based
on a real customer case



In this study, it was evaluated the fluid film thickness as function of angular speed of wafer, liquid flow velocity, nozzle motion and distance from the wafer.

The 1D network Multiphysics modelling are powerful and fast tools to assess performance of the system. In the examples below, the focus is on flow. However, it can be easily extended to flow with heat transfer, mechanical actuators and more.

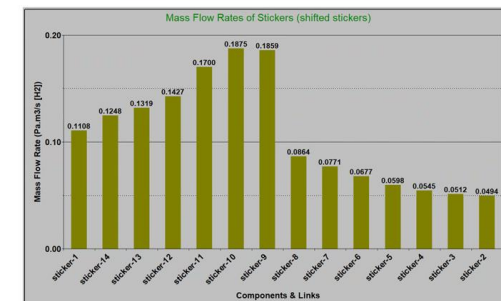
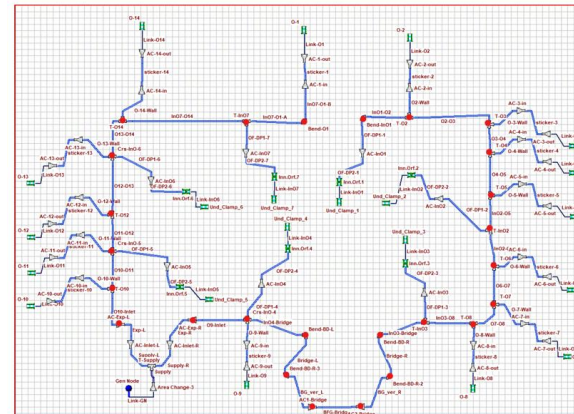


- The 1D approach provides an averaged mismatch of 4% wrt 3D CFD;
- The higher deviation are present in the extremities due to 3D effect which cannot be captured by the 1D approach;
- 1D approach is very flexible, allowing us to make sensitivity analysis/optimization of multiple parameters in seconds (depending on the complexity of the model).

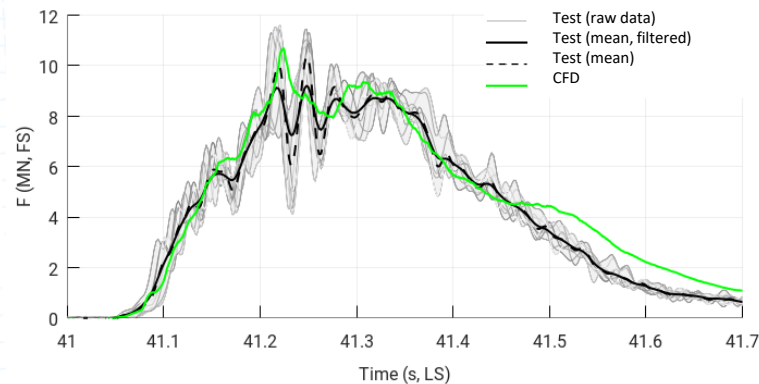
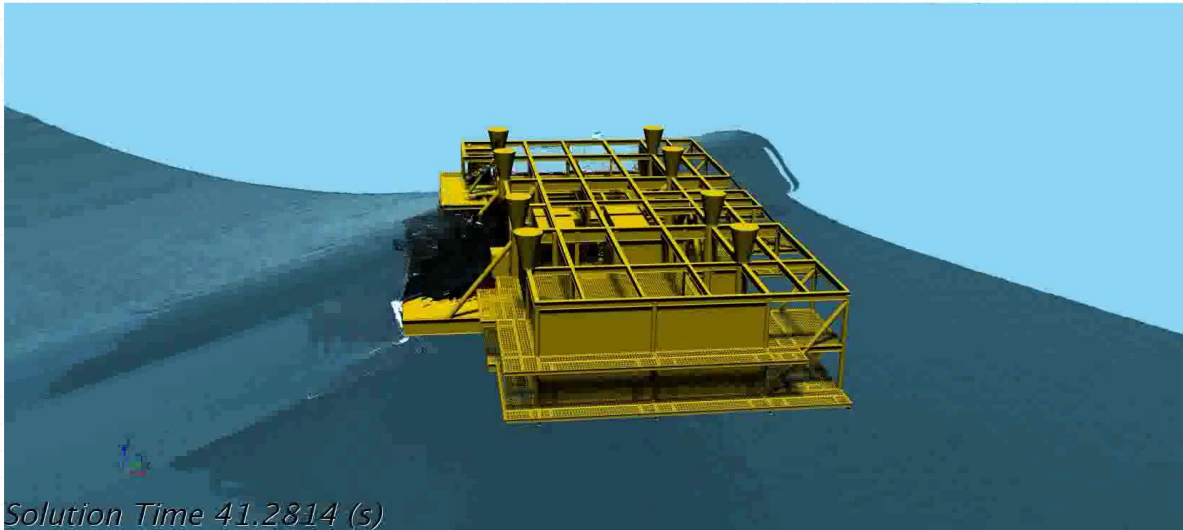
In this case, a more complex network of channels, flow restrictions and volumes are created in 1D to represent the 3D design.

The objective was to assess the level of uniformity.

<< In this example, flow uniformity is critical for the performance of the system. In order to verify if the 1D approach would be enough, a 3D CFD was performed and compared with the 1D tool.



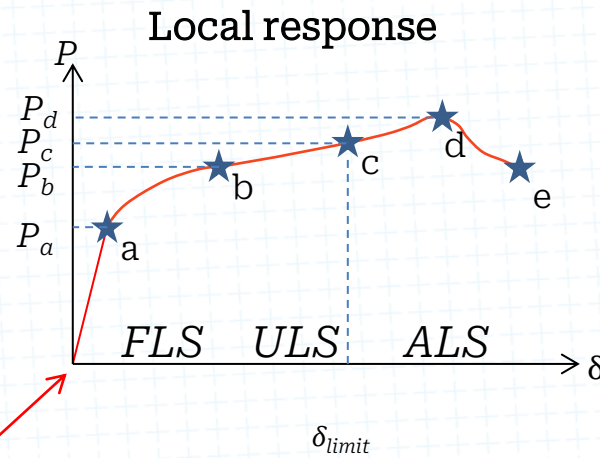
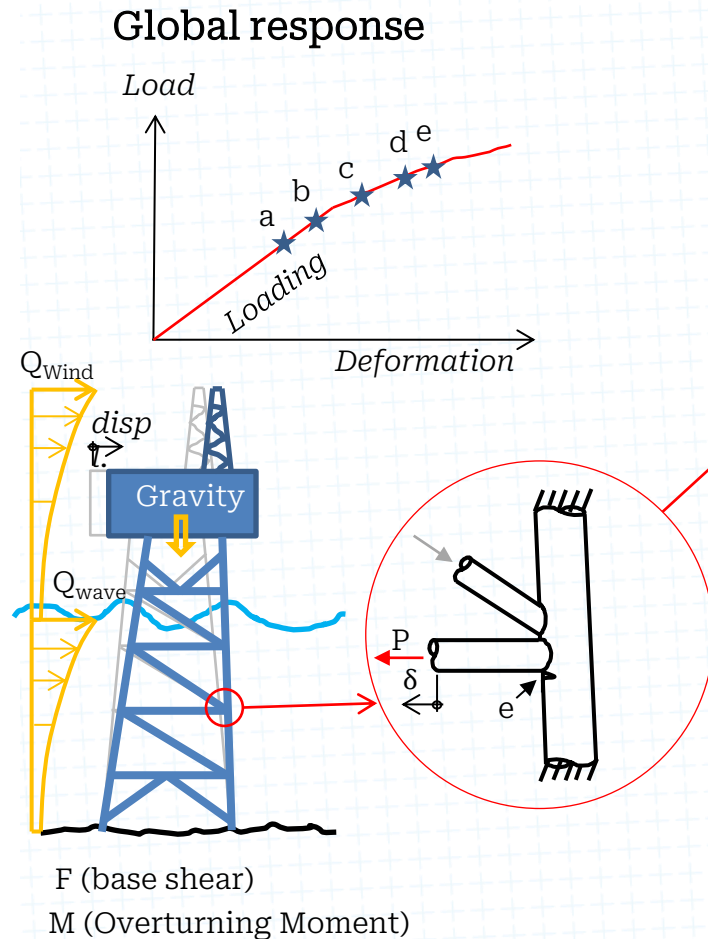
CFD Wave load validation for complex structures



Validated CFD methodology for Wave loads

- Method
 - Numerical schemes for discretization and time integration
 - Meshing approach and resolution
 - Time step optimization
- Surface elevation
 - Comparisons with measured wave gauges (2D flume and 3D basins with regular, irregular and breaking waves)
 - Comparisons with HD video
 - Comparisons with theoretical linear irregular waves (spectrum)
- Kinematics
 - Comparisons with PIV and LDA data
- Loads
 - Comparisons with measured loads on scale models (regular and breaking waves)

Structural response modeling

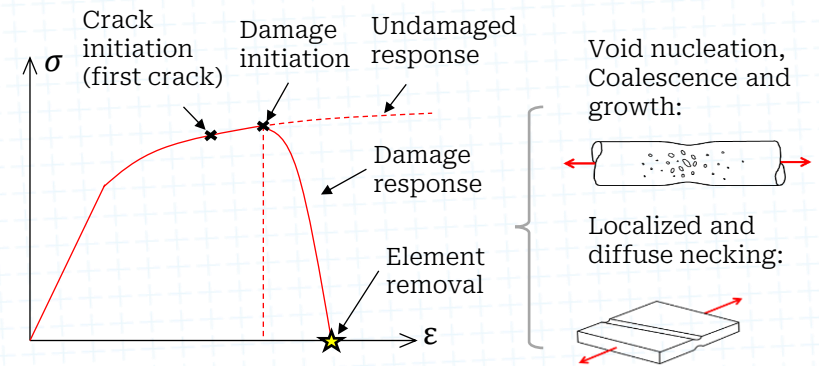


Failure limits:

- initiation of material yielding
- crack initiation
- deformation limit
- ultimate capacity
- tensile failure

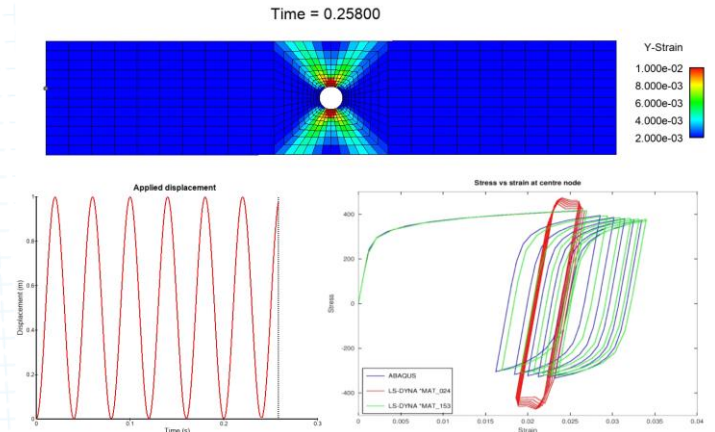
Structural damage evolution

Capturing effects of material degradation with use of damage initiation and damage evolution



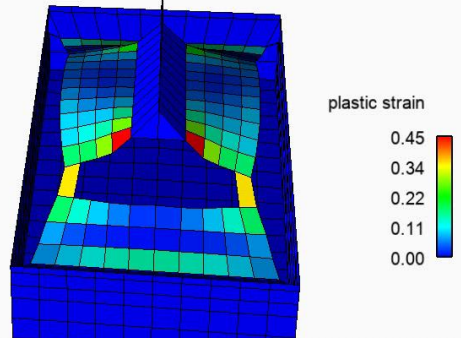
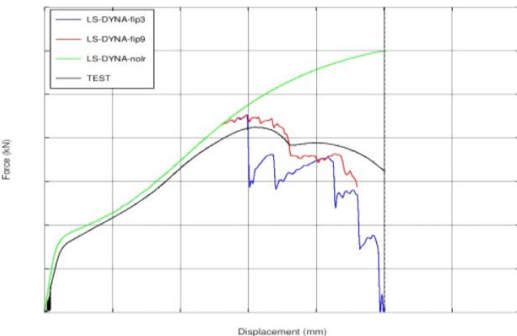
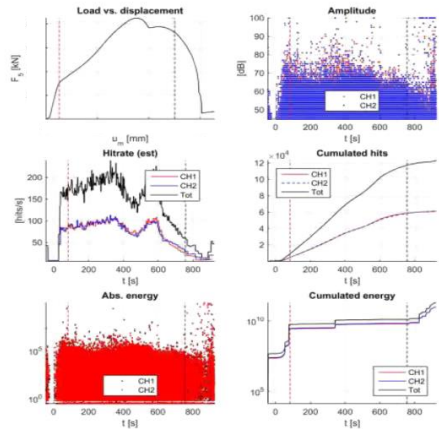
Non-linear Material modeling

Capturing effects of cyclic loading with use of Non-linear kinematic hardening such as the Chaboche material model



Validation of Structural response – methodology calibration

Methodology Calibration



Calibration and Validation: © Eriksson M., Nyberg M., Andersen M., Tychsen J. and Nielsen J., "Validated Methodology for Assessment of Welded Steel Structures by Nonlinear Finite Element Analysis", *International Journal of Offshore and Polar Engineering*, Vol. 34, No. 2, June 2024, pp. 191–198.

<https://doi.org/10.17736/ijope.2024.ty14>

Validated FEA methodology for welded details

- Based on an extensive testing campaign involving
 - 16 test series with various failure mechanisms
 - Varying levels of Bending in combination with Tension
 - In-plane shear failures
- Calibration adhering to ISO 19902:2020

Calibration includes

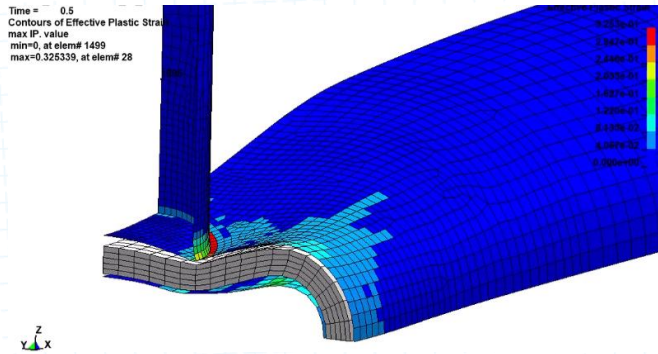
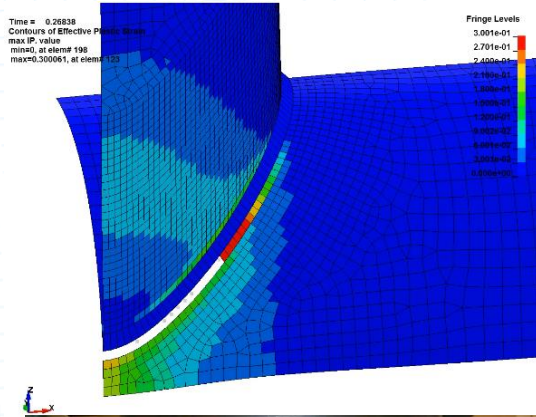
- Material
 - Stress-strain curve
 - Failure strain (eroding)
 - Number of layers to element failure
- Shell definition
 - Element formulation
 - Number of through thickness integration points
- Mesh resolution
 - Along welds
 - Over gaps
 - At weld terminations

Weld modelling Failure criteria/limits

- Mean and characteristic strain limits:
 - Crack initiation / Local necking (degrading fatigue properties)
 - Ultimate tensile failure

Validation of Structural response – methodology validation

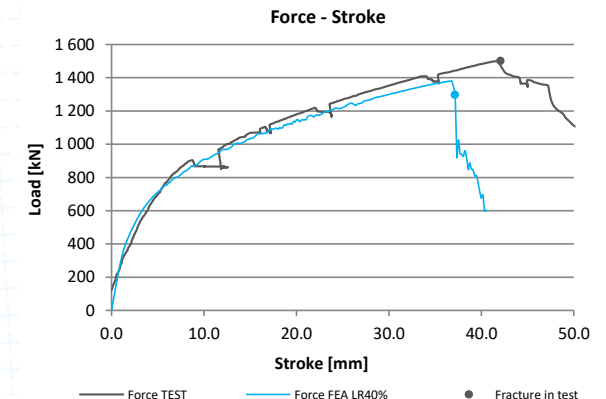
Methodology Validation



Calibration and Validation: © Eriksson M., Nyberg M., Andersen M., Tychsen J. and Nielsen J., “Validated Methodology for Assessment of Welded Steel Structures by Nonlinear Finite Element Analysis”, *International Journal of Offshore and Polar Engineering*, Vol. 34, No. 2, June 2024, pp. 191–198.
<https://doi.org/10.17736/ijope.2024.ty14>

Validation of the methodology's performance and generalizability

- Reassessment of independent dataset from previously performed validation of Tubular joints and members
- Confirmation of welded section modelling and failure criteria/limits
- Weld modelling rules for tubular joints
 - Both with and without grout

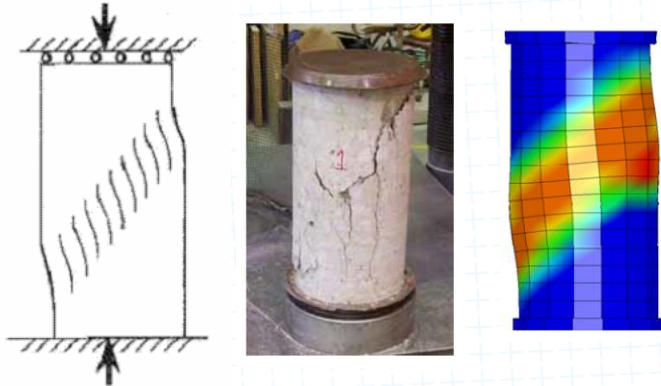


Grout model calibration for grout reinforced jacket legs

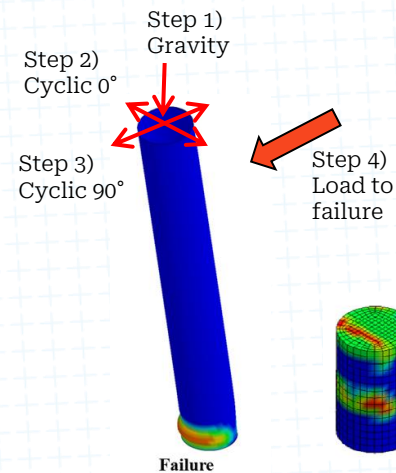
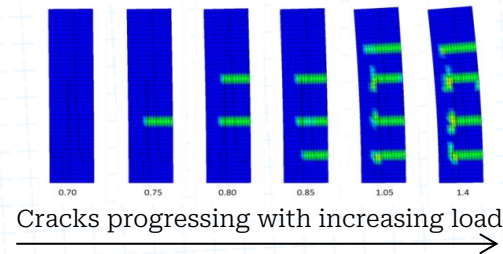
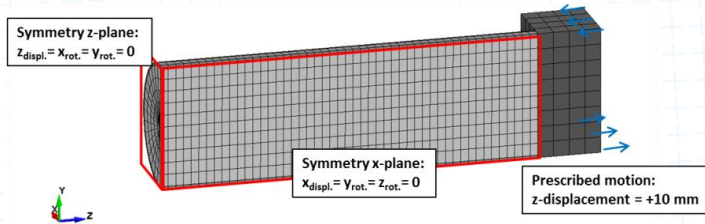
Project description:

Enhance the accuracy of the grout representation in grout reinforced jacket legs analysis models. Correlation against test with and without grout.

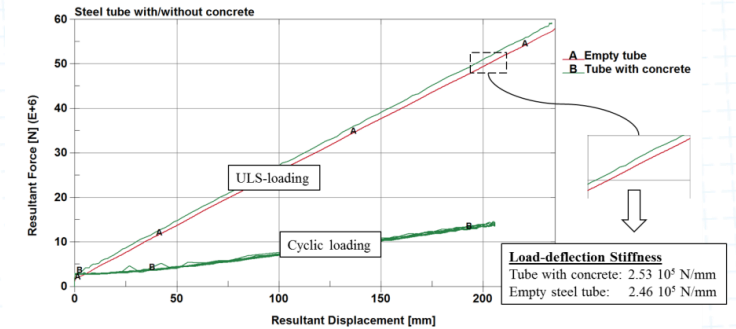
Compression



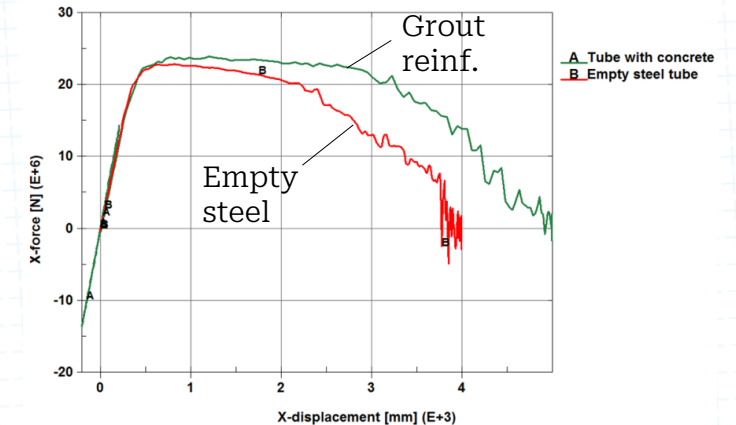
Bending



Ultimate load scenario:



Ultimate load capacity:



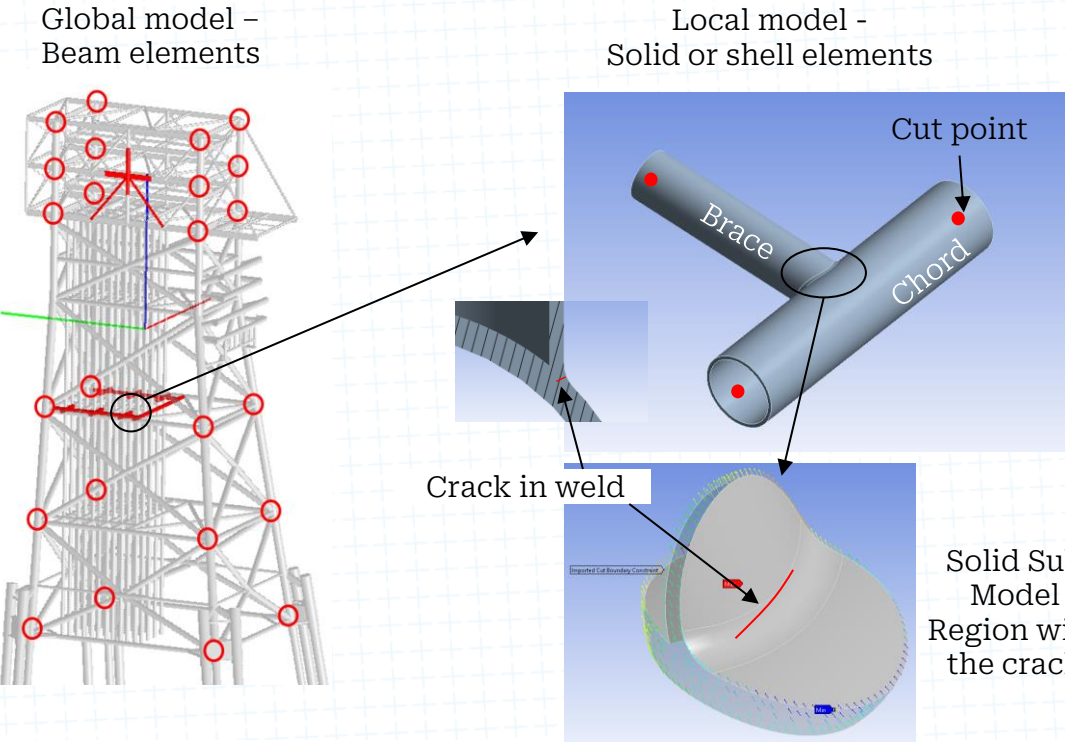
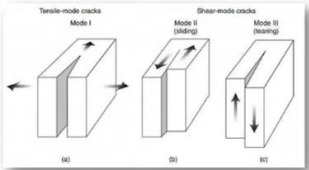
Crack growth assessment within tubular joint weld detail

Project description:

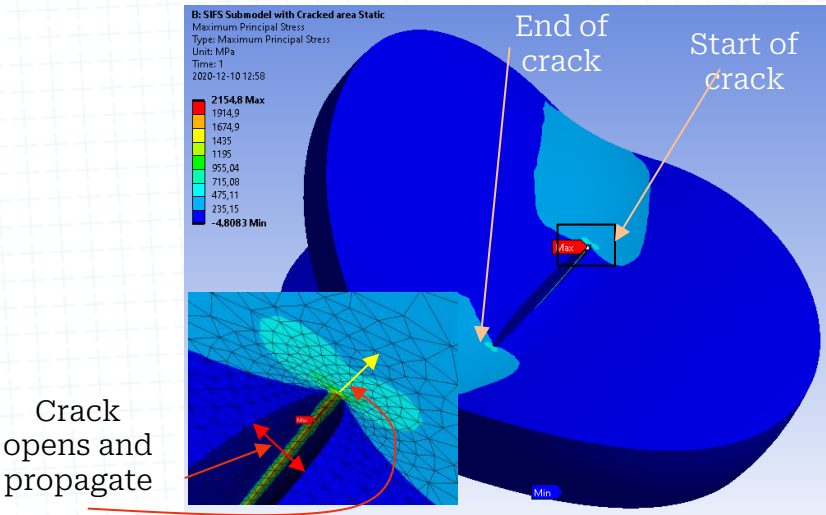
In case when structures are subject to cyclic loading, it is of interest to know the interaction between crack extension rate and the number of load cycles. Preexisting cracks may propagate when certain loading conditions are reached or when certain localized conditions are met.

Fracture Mechanics Modes

- Three primary modes of fracture:
- Mode I: tensile or opening mode – generally most critical
 - Mode II: sliding or shear mode
 - Mode III: tearing mode



Solid Sub Model Crack growth results



THANK YOU!

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Phone: +49 151 4315 7230

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