

# A Multi-Physics Eulerian Framework for Long-Term Contrail Evolution\*

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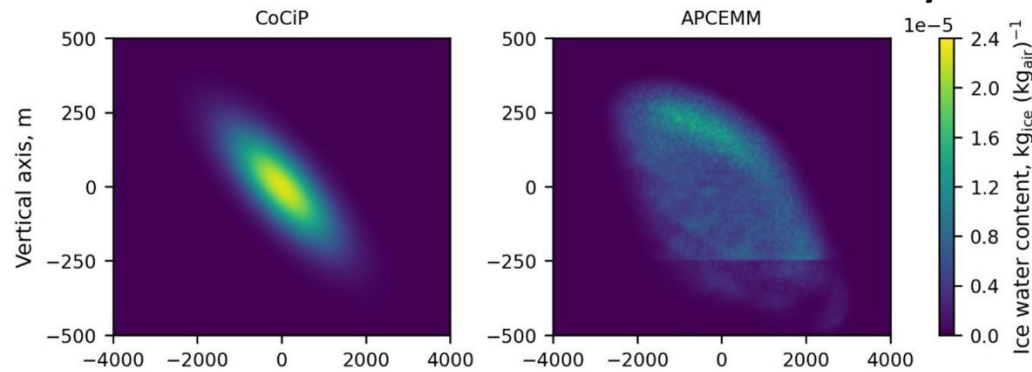
\*Jafarimoghaddam, A., & Soler, M. (2025). A Multi-Physics Eulerian Framework for Long-Term Contrail Evolution. *arXiv preprint arXiv:2509.00965*.

\*Jafarimoghaddam, A., & Soler, M. (2025). A Multi-Physics Eulerian Framework for Long-Term Contrail Evolution. Pre-print and interactive public peer review. *Atmo. Chem. Physics*. Egusphere-2025-4155

# Motivation

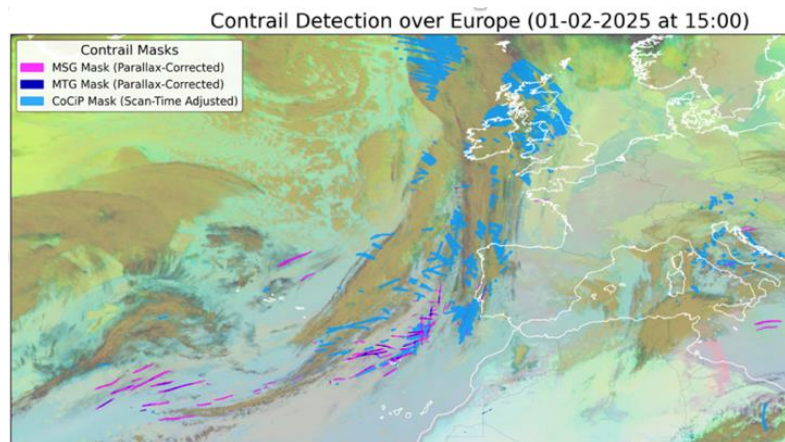
Current contrail climate impact estimation models being used in ATM studies exhibit significant discrepancies.

**Predicted lifetimes and RF of CoCiP & APCEMM differ by factors of 2-5**



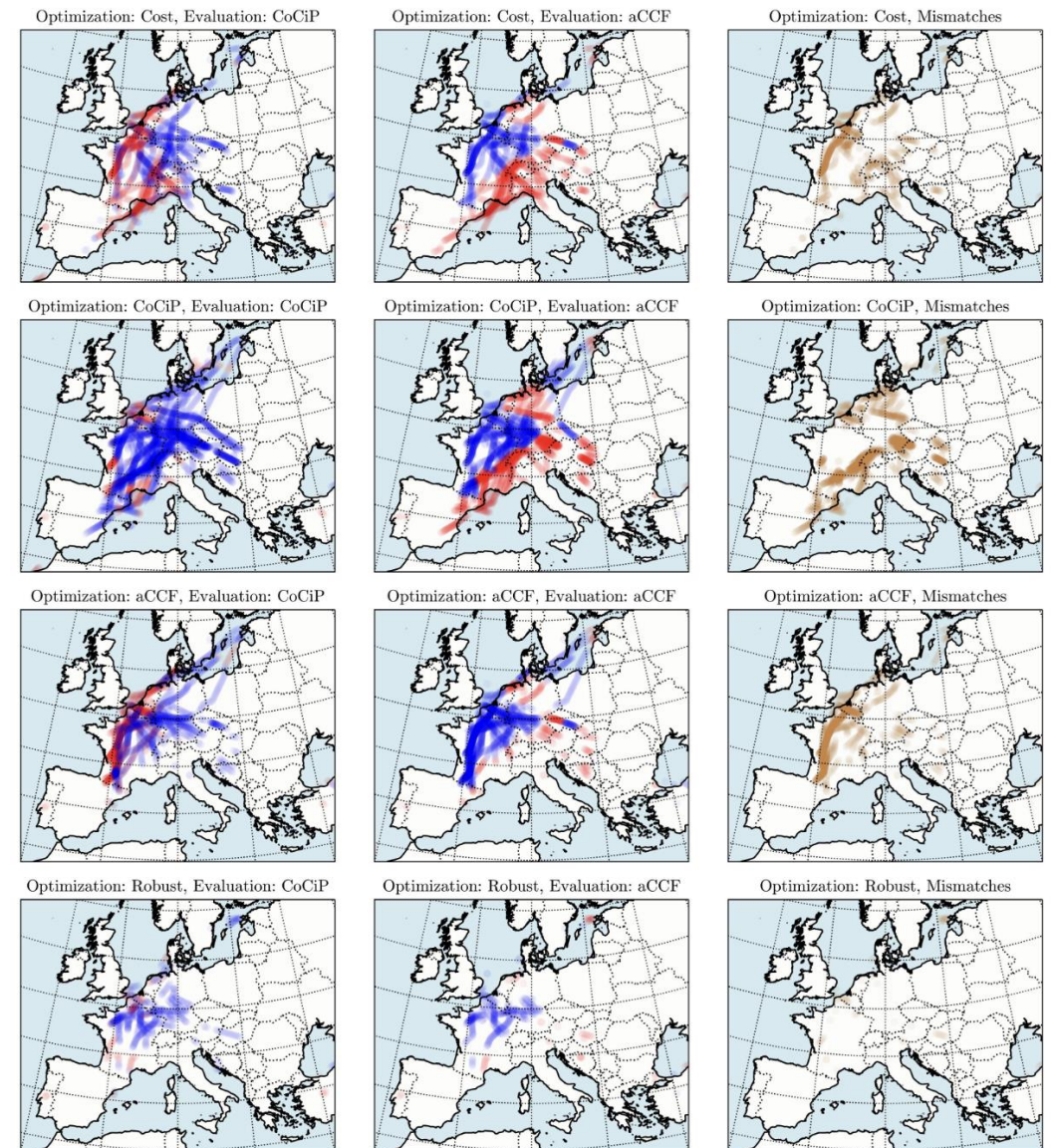
Akhtar Martínez et al. (2025). Contrail models lacking post-fallstreak behavior could underpredict lifetime optical depth. EGU Sphere, 1-26.

**Data-Driven detections and Models differ.**



Contrails detected by a deep learning model using data from Meteosat Second Generation (MSG) and Meteosat Third Generation (MTG), compared to those simulated by CoCiP. (Ortiz, Soler et. al, 2025 at EGU)

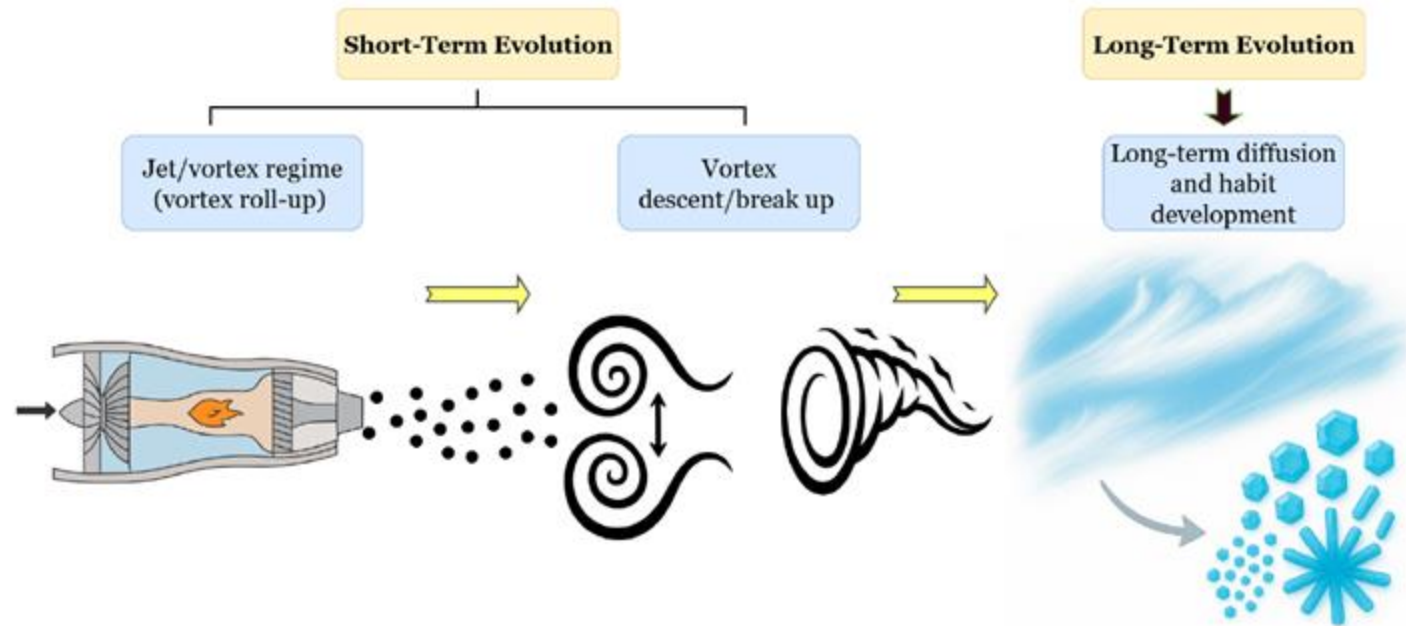
**Contrail Avoidance strategies sensitive to model uncertainties**



Simorgh, Abolfazl and Simorgh, Abolfazl and Soler, 2025, Manuel, Feasibility of Integrating Multiple Climate Impact Estimation Models to Enhance Confidence in Environmentally-Friendly Aircraft Trajectory Optimization (January 10, 2025). Available at SSRN: <http://dx.doi.org/10.2139/ssrn.5409422>

# Contrail Modelling (Contributions)

Contrails undergo multiple regimes/stages right after their birth to eventually becoming cirrus clouds.



Existing Contrail Models:

Are Lagrangian models  
Do not incorporate habit development  
Do not incorporate multi-phase flow settling

COCIP

(Schumann, 2012)

APCEMM

(Fritz et al., 2020)

CFD approaches (LES & RANS)

(Unterstrasser & Gierens, 2010 –I,II–)

(Lewellen, 2020)

## Phase 1: Short-Term

- Ice-Particle Transport (**Macrophysics**)
- Induced Engine Jet Flow (**Macrophysics**)
- Ice-Particle Growth (**Microphysics**)
- Nucleation (**Microphysics**)
- Aggregation (**Microphysics**)

## Phase 2: Long-Term

- Ice-Particle Transport (**Macrophysics**)
- Ice-Particle Growth (**Microphysics**)
- Habit Development (**Microphysics**)
- Aggregation (**Microphysics**)
- Multi-Phase Flow Settling (**Macrophysics**)

Our model is:

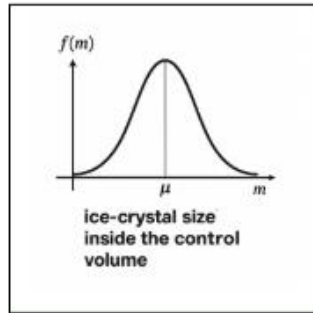
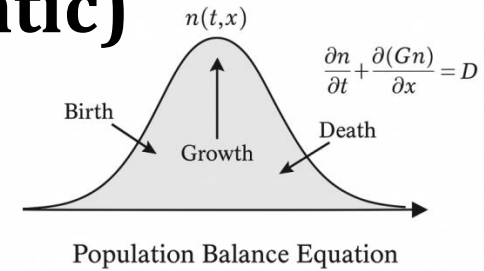
- Focus only on long-term
- Eulerian
  - Quasi Analytic representation of the sol.
  - Includes habits and multi-phase flow settling.



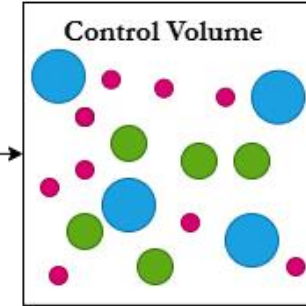
# Advection-Diffusion Contrail Modelling (Schematic)

Population  
Balance Eq. (PBE)

$$\frac{\partial f}{\partial t} + \mathbf{v}_p \cdot \nabla f = -\frac{\partial}{\partial m}(\dot{m} f) + \nabla \cdot (\tilde{D} \nabla f) + S_f,$$



$$\frac{\partial f}{\partial t} + \mathbf{v}_p \cdot \nabla f = -\frac{\partial}{\partial m}(\dot{m} f) + \nabla \cdot (D \nabla f)$$



Zeroth Moment  
(Number Concentration)

First Moment  
(Mass Concentration)

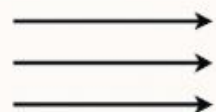
Macroscale Ice-  
Particle Modeling

Wind Model

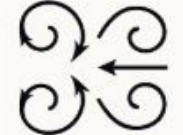


Vortex cores

Anticyclonic



Free stream  
segments



Dipoles and  
sheared zones

$$\mathbf{u}(\mathbf{x}) = \mathbf{u}_\infty + \sum_{l=1}^{M_d} \mathbf{M}_l^{(d)} + \sum_{k=1}^{M_d} \mathbf{M}_k^{(v)}$$

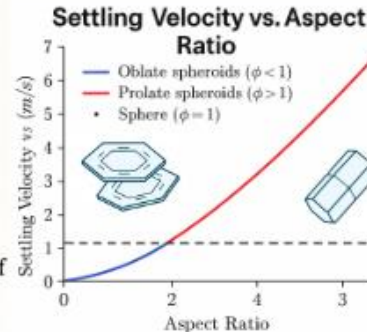
Multi-Phase Flow Settling Velocity

Settling velocity

Bulk speed

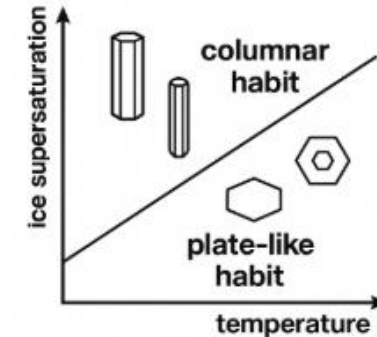
Initially  
zero

Terminal velocity reaches that of  
terminal velocity (which is the  
characteristic single particle speed  
falling in an unbounded fluid)



Ice Particle Microphysics

ice crystal habit



$$\frac{d\phi}{dv} = \frac{\Gamma(T, s_i) - 1}{\Gamma(T, s_i) + 2} \frac{\phi}{v}$$

$$\frac{dm}{dt} = \rho_{ice} f_v(v, \phi, \mathbf{x})$$

# Problem Statement: Ice Particle Transport

Starting with PBE:

$$\frac{\partial f}{\partial t} + \mathbf{v}_p \cdot \nabla f = -\frac{\partial}{\partial m}(\dot{m} f) + \nabla \cdot (\tilde{\mathcal{D}} \nabla f) + S_f,$$

Together with the particle velocity  $\mathbf{v}_p$  (long-term regime):

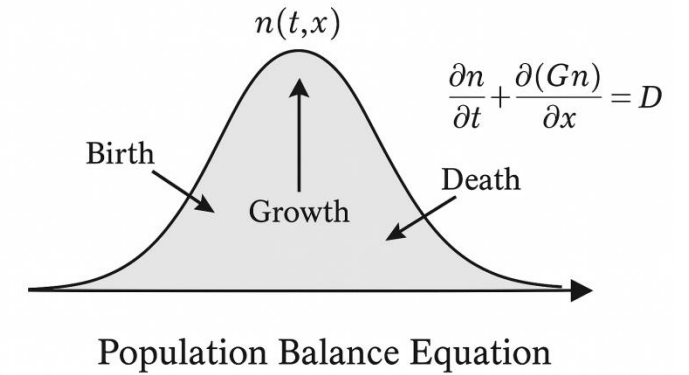
$$\mathbf{v}_p = \mathbf{v}_{slp} + \underbrace{(w_x, w_y, w_z)^\top}_{\substack{\text{background velocity} \\ \text{(wind components)}}} \approx (0, 0, v_s)^\top + \underbrace{(w_x, w_y, w_z)^\top}_{\text{background velocity}} = (w_x, w_y, w_z + v_s)^\top.$$

We can derive the moment equations as:

$$\frac{\partial c_N}{\partial t} + \mathbf{v}_p \cdot \nabla c_N = \nabla \cdot (\tilde{\mathcal{D}} \nabla c_N) + S_{c_N}$$

$$\frac{\partial m}{\partial t} + \mathbf{v}_p \cdot \nabla m = \tilde{\mathcal{D}} \nabla^2 m + (\nabla \tilde{\mathcal{D}}) \cdot \nabla m + \frac{2\tilde{\mathcal{D}}}{c_N} \nabla m \cdot \nabla c_N + \rho_{dep} f_v + S_{c_M}$$

where,  $m(\mathbf{x}, t)$  is the representative particle mass in control volume, and  $c_N(\mathbf{x}, t)$  is number concentration.



# Problem Statement: Ice Particle Growth and Habit Development

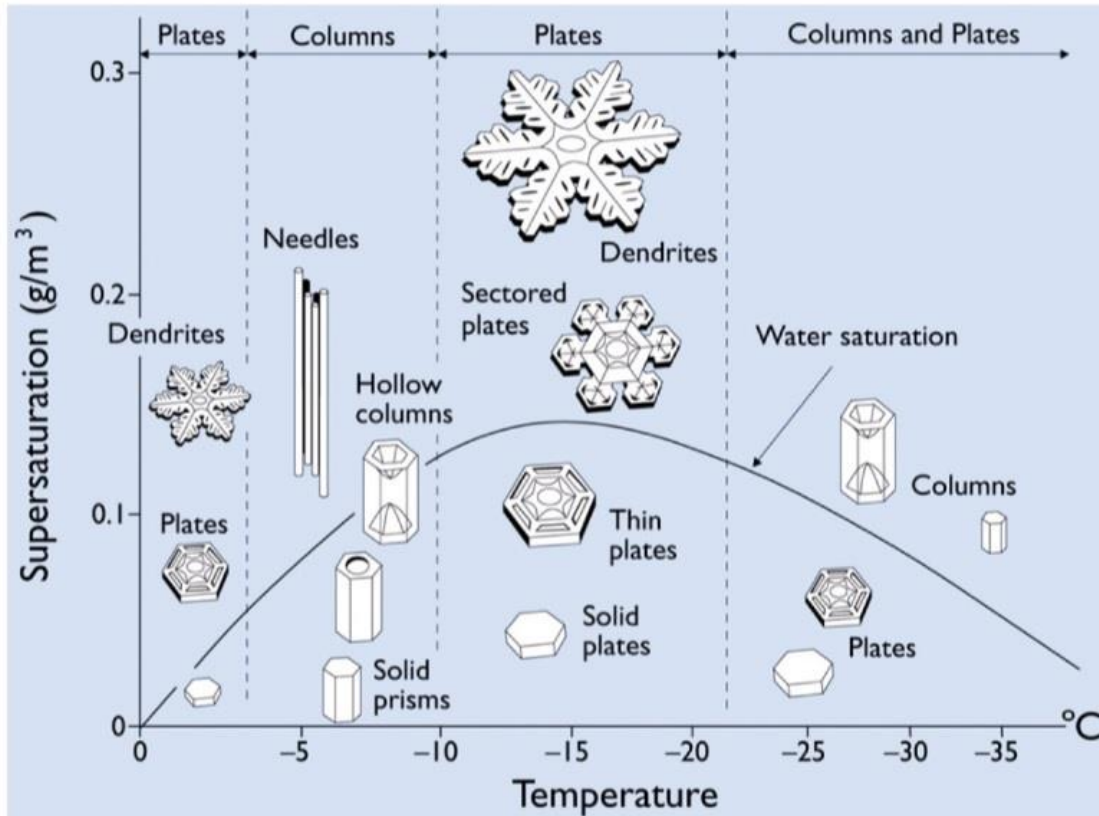
Mature contrail cirrus (on the order of 1–10 hours old in ice-supersaturated layers) transition into the same regime as natural cirrus, where habit classification based on temperature and supersaturation becomes appropriate.

To summarize:

**Fresh contrail (< 5 min):** *Tiny polycrystalline droxtals*; no habit classification.

**Early contrail cirrus (5 min–20 mins):** *Mixed phase*; spheres and rough aggregates.

**Mature contrail cirrus (20 mins–10 h):** *Crystals  $\geq 20\text{--}30\text{ }\mu\text{m}$* ; faceted habits consistent with natural cirrus and subject to the standard temperature-supersaturation-habit relationship.



Microphysics for ice-particle growth  
and shape evolution:

(Cheng and Lamb, 1994)

$$f_v(\mathbf{x}, a, \phi, t) = \frac{4\pi C s_i}{\rho_{dep} \left( \frac{R_v T}{e_i D_v} + \frac{L_s}{T k_a} \left( \frac{L_s}{R_v T} - 1 \right) \right)},$$

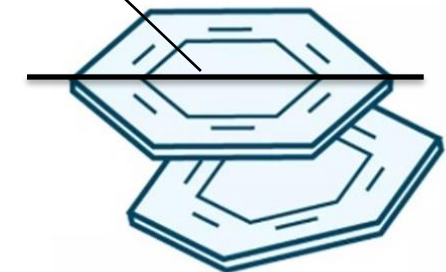
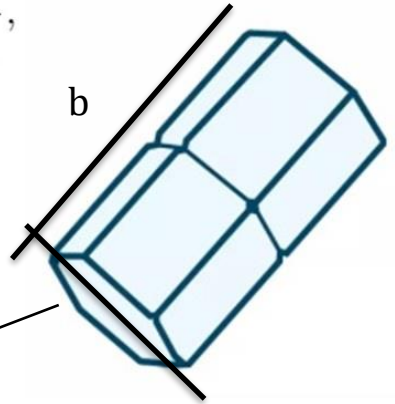
$$f_\phi(\mathbf{x}, a, \phi, t) = \frac{\Gamma - 1}{\Gamma + 2} \frac{\phi}{v} f_v(\mathbf{x}, a, \phi, t).$$

$$\frac{dm}{dt} = \rho_{dep} f_v,$$

$$\frac{d\phi}{dt} = f_\phi,$$

$$v = \frac{4}{3} a^3 \phi.$$

equatorial radius (a):  $\phi = \frac{b}{a}$



# Problem Statement: Multi-Phase Flow Settling

In Eulerian framework, settling velocity requires more careful implementation to account for self-diffusion effect:

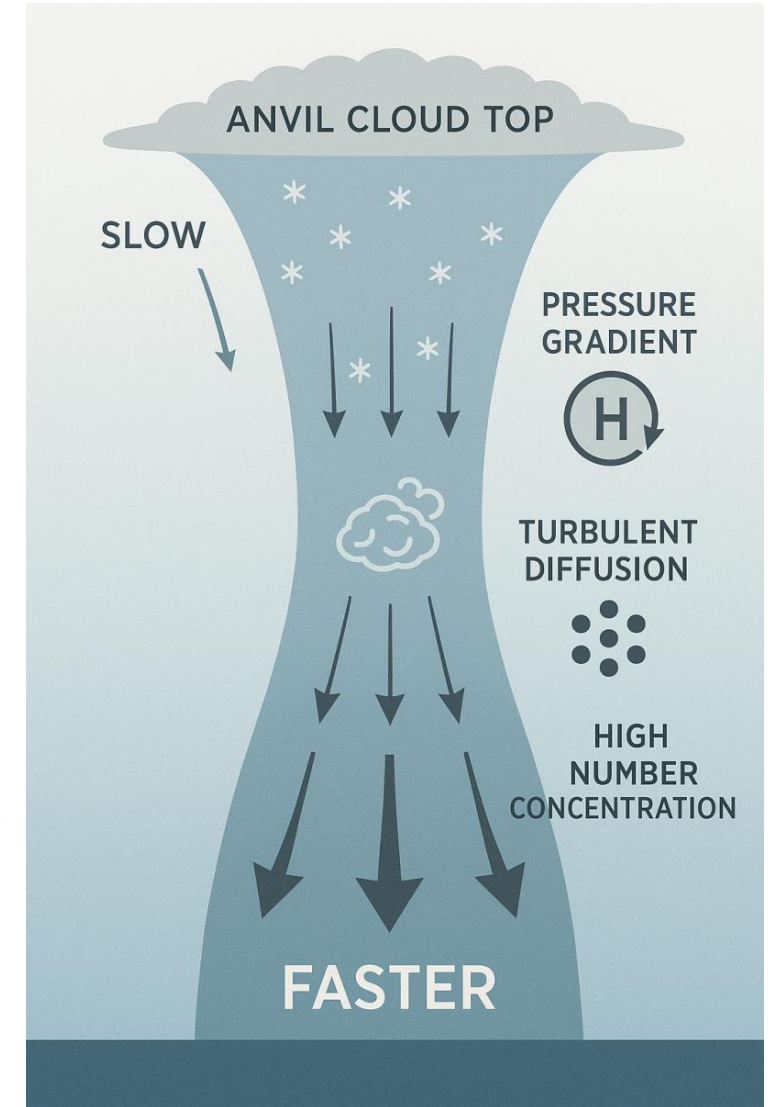
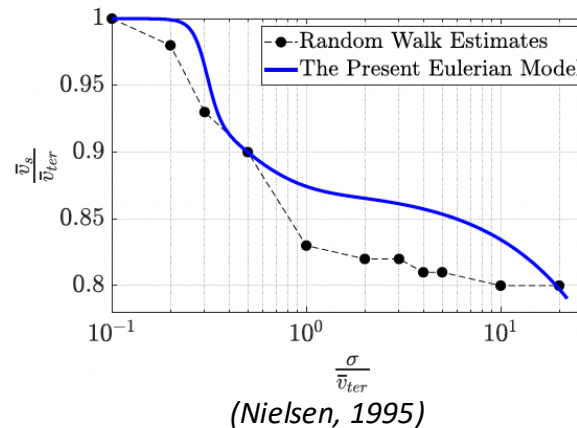
- Bulk of particles in a turbulent mixing
- Loitering and sweeping
- $V_s$  not equal to  $V_{ter}$  for all times (sol. to Stokes eq.)

Starting with the classical multi-phase flow equation in an Euler-Euler framework for the particle phase:

$$\frac{\partial(\epsilon_p \rho_p \mathbf{v}_{slp})}{\partial t} + \nabla \cdot (\epsilon_p \rho_p \mathbf{v}_{slp} \mathbf{v}_{slp}) = -\epsilon_p \nabla p + \nabla \cdot \tau_p + \epsilon_p \rho_p \mathbf{g} + F_d,$$

We can show that the equation can be reduce to the following reduced-order model  
(A Burgues-type PDE):

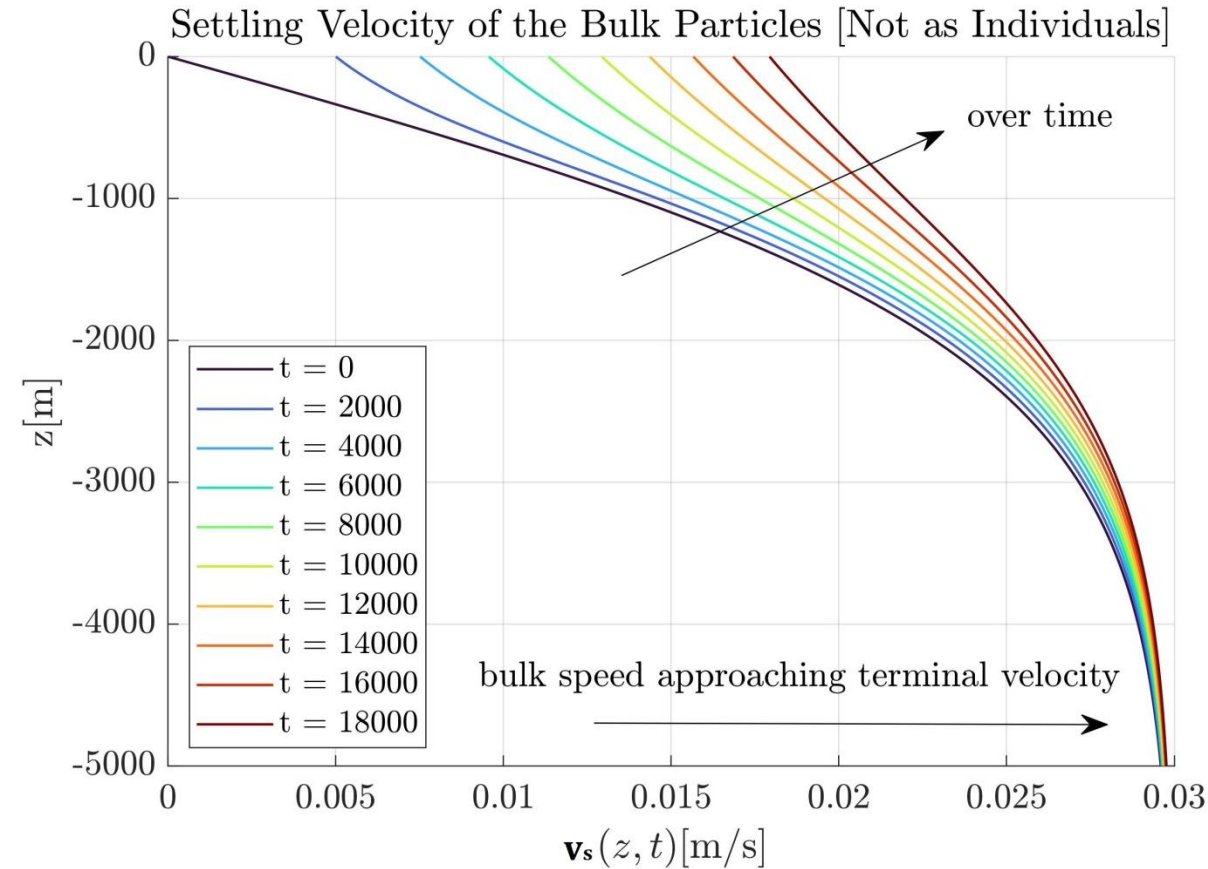
$$\begin{aligned} \frac{\partial v_s}{\partial t} + v_s(z, t) \frac{\partial v_s}{\partial z} &= \nu_{t,ef} \frac{\partial^2 v_s}{\partial z^2}, \\ v_s(z_{ref}, 0) &= 0, \quad \lim_{z \rightarrow -\infty} v_s = v_{ter}, \quad \lim_{t \rightarrow \infty} v_s = v_{ter}, \\ Re^2 C_D(Re^*) &= B. \quad v_{ter} = \frac{Re \mu_{ef}}{\rho_f d_v}. \end{aligned}$$



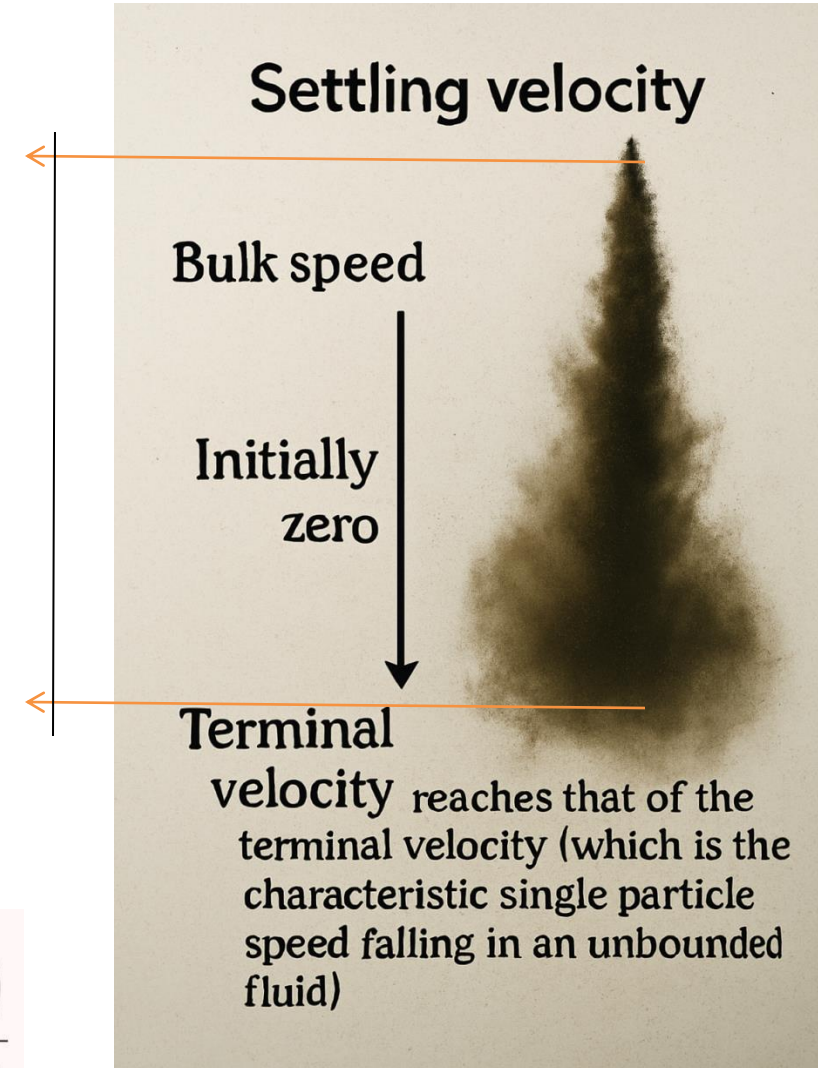


# Problem Statement: Multi-Phase Flow Settling

In Eulerian framework, settling velocity requires more careful implementation to account for self-diffusion effect:



$$v_s(z, t) = v_{\text{ter}} \cdot \frac{\operatorname{erfc}\left(\frac{z - v_{\text{ter}}t}{2\sqrt{\nu t}}\right) - \exp\left(\frac{v_{\text{ter}}(z - v_{\text{ter}}t)}{\nu}\right) \cdot \operatorname{erfc}\left(\frac{z + v_{\text{ter}}t}{2\sqrt{\nu t}}\right)}{\operatorname{erfc}\left(\frac{z - v_{\text{ter}}t}{2\sqrt{\nu t}}\right) + \exp\left(\frac{v_{\text{ter}}(z - v_{\text{ter}}t)}{\nu}\right) \cdot \operatorname{erfc}\left(\frac{z + v_{\text{ter}}t}{2\sqrt{\nu t}}\right)}$$



The schematic shows *Free-Fall* of particles as a bulk



# Problem Statement: System of Equations

It turns out the homogeneous boundary and initial conditions allow separation of variables through:

$$c_N(x, y, z, t) = F(x, y, t) g(z, t),$$

$$\mathcal{D}(c) \propto \frac{1}{1 + \beta c}.$$

$$\tilde{\mathcal{D}}_{ij}(c_N) \longrightarrow \begin{cases} \tilde{\mathcal{D}}_{xx}(F(x, y, t)), \\ \tilde{\mathcal{D}}_{yy}(F(x, y, t)), \\ \tilde{\mathcal{D}}_{zz}(g(z, t)). \end{cases}$$

$$\begin{aligned} w'_x(x, y, t) &= \sigma_{w_x} \Re \left\{ \mathcal{F}^{-1} \left[ \sqrt{E(k_x, k_y)} \xi_{w_x}(k_x, k_y, t) \right] \right\}, \\ w'_y(x, y, t) &= \sigma_{w_y} \Re \left\{ \mathcal{F}^{-1} \left[ \sqrt{E(k_x, k_y)} \xi_{w_y}(k_x, k_y, t) \right] \right\}. \end{aligned}$$

wind turbulence

Therefore, following the assumption of local (piece-wise) constant temperature, we can show that the system breaks down into:

$$\begin{aligned} \frac{\partial F}{\partial t} + w_x(x, y, t) \frac{\partial F}{\partial x} + w_y(x, y, t) \frac{\partial F}{\partial y} &= \frac{\partial}{\partial x} \left( \tilde{\mathcal{D}}_{xx}(F) \frac{\partial F}{\partial x} \right) + \frac{\partial}{\partial y} \left( \tilde{\mathcal{D}}_{yy}(F) \frac{\partial F}{\partial y} \right), \\ \frac{\partial g}{\partial t} + v_s(z, t) \frac{\partial g}{\partial z} &= \frac{\partial}{\partial z} \left( \tilde{\mathcal{D}}_{zz}(g) \frac{\partial g}{\partial z} \right), \\ \frac{\partial m}{\partial t} + v_s(z, t) \frac{\partial m}{\partial z} &= \frac{\partial}{\partial z} \left( \tilde{\mathcal{D}}_{zz}(g) \frac{\partial m}{\partial z} \right) + \frac{2 \tilde{\mathcal{D}}_{zz}(g)}{g} \frac{\partial m}{\partial z} \frac{\partial g}{\partial z} + \rho_{\text{dep}} f_v(z, t), \\ \frac{\partial \phi}{\partial t} + v_s(z, t) \frac{\partial \phi}{\partial z} &= \frac{\Gamma(T(z, t)) - 1}{\Gamma(T(z, t)) + 2} \frac{\phi}{v} f_v(z, t), \\ \frac{\partial v_s}{\partial t} + v_s(z, t) \frac{\partial v_s}{\partial z} &= \nu_{t,ef} \frac{\partial^2 v_s}{\partial z^2}, \\ v_s(z_{ref}, 0) &= 0, \quad \lim_{z \rightarrow -\infty} v_s = v_{ter}, \quad \lim_{t \rightarrow \infty} v_s = v_{ter}, \\ dX &= -\frac{X - \mu}{\tau} dt + \sigma_X dW_t, \quad X \in \{\tilde{v}_s, \tilde{\mathcal{D}}_{xx}, \tilde{\mathcal{D}}_{yy}, \tilde{\mathcal{D}}_{zz}\}, \\ v(z, t) &= \frac{m(z, t)}{\rho_{\text{dep}}}. \end{aligned}$$

number concentration

microphysics evolution

settling velocity

stochasticity

**Terminal Velocity**

$$Re^2 C_D(Re^*) = B.$$

$$v_{ter} = \frac{Re \mu_{ef}}{\rho_f d_v}.$$

# Sol. Approach: Directional-ODE Discretization\*

$$\frac{\partial u}{\partial t} = D \frac{\partial^2 u}{\partial x^2} + f(x, t). \quad \text{traditional way}$$

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} = D \cdot \frac{u_{i-1}^n - 2u_i^n + u_{i+1}^n}{(\Delta x)^2} + f(x_i, t_n, u_i^n)$$

$$\frac{du_i}{dt} = D \frac{u_{i-1}(t) - 2u_i(t) + u_{i+1}(t)}{(\Delta x)^2} + f(x_i, t_n, u_i^n), \quad t \in [t_n, t_{n+1}].$$

Constant Neighboring Nodes:

$$\frac{du_i}{d\tau} = -Au_i(\tau) + B, \quad u_i(0) = u_i^n, \quad \tau := t - t_n, \quad \tau \in [0, \Delta t], \quad \Delta t := t_{n+1} - t_n.$$

Solution with Constant Neighboring Nodes:

$$u(t) = -\frac{B'}{A'} + \left(\frac{B'}{A'} + u_i^n\right)e^{A'(t-t^n)}.$$

Global Update Formula with Non-Constant Neighboring Nodes:

$$u_i(\tau) = \left(u_i^n - \frac{s}{2\bar{a}} - \sum_{p=0}^P \frac{a_p}{2} \frac{(-1)^p p!}{(2\bar{a})^p}\right) e^{-2\bar{a}\tau} + \sum_{p=0}^P \frac{a_p}{2} \sum_{q=0}^p \frac{\tau^{p-q} (-1)^q p!}{(2\bar{a})^q (p-q)!} + \frac{s}{2\bar{a}}.$$

Amin Jafarimoghaddam, Manuel Soler, and Irene Ortiz. A directional-ode framework for discretization of advection-diffusion equations. arXiv preprint arXiv:2506.06543, Jun 2025. arXiv:2506.06543 [math.AP].

modern way

a. Advection-Diffusion Process



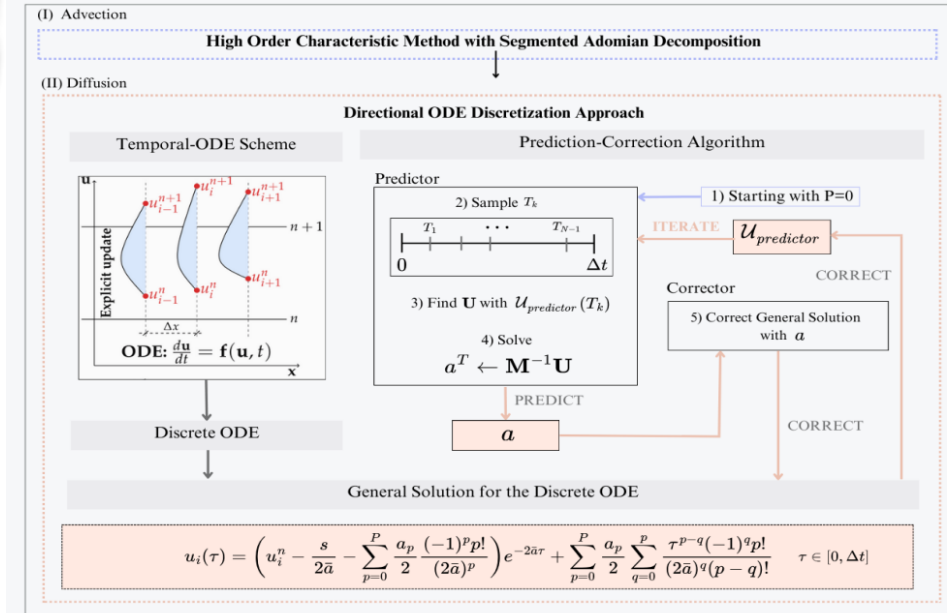
b. Advection-Diffusion Equation

Operator Splitting.

$$\frac{\partial u}{\partial t} + \mathbf{V} \cdot \nabla u = \bar{d} \Delta u + f(\mathbf{x}, t, u)$$

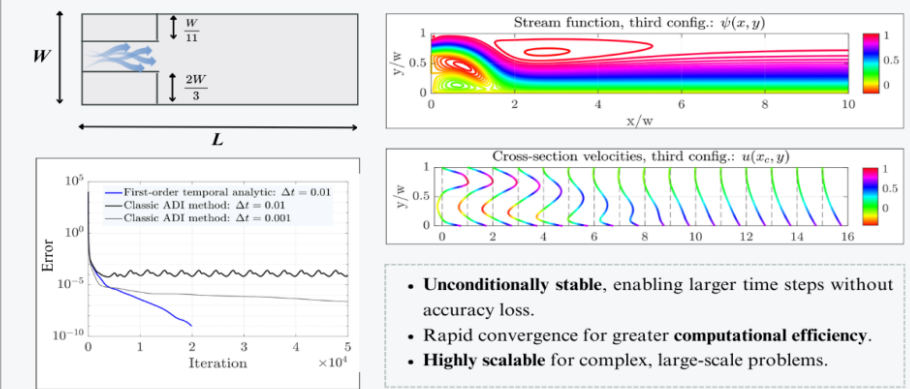
$u^n \xrightarrow{\text{advection operator}} u_{\text{adv}}^n \xrightarrow{\text{diffusion operator}} u^{n+1}$

d. Discretization Method



e. Application Example

The Navier-Stokes equations in the streamfunction-vorticity for 2D incompressible flow



# Simulation Results

## Plume Initialization:

Reference altitude: 10 km,

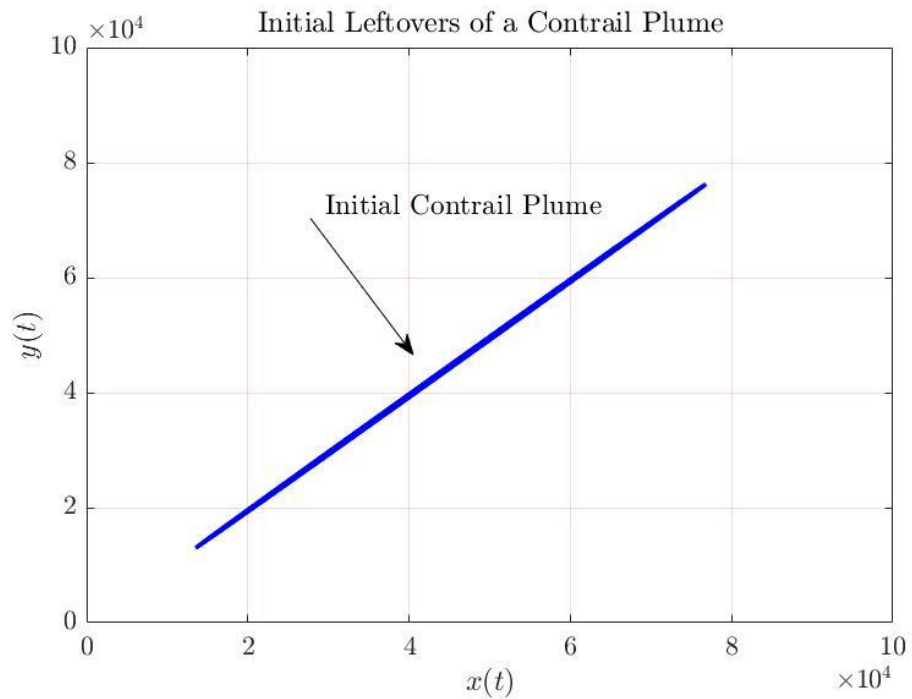
Reference Temperature: -61 C (*Yang et al., 2010*)

Background ISSR: Varied Magnitude,  $\sim 1.3$  km thick,

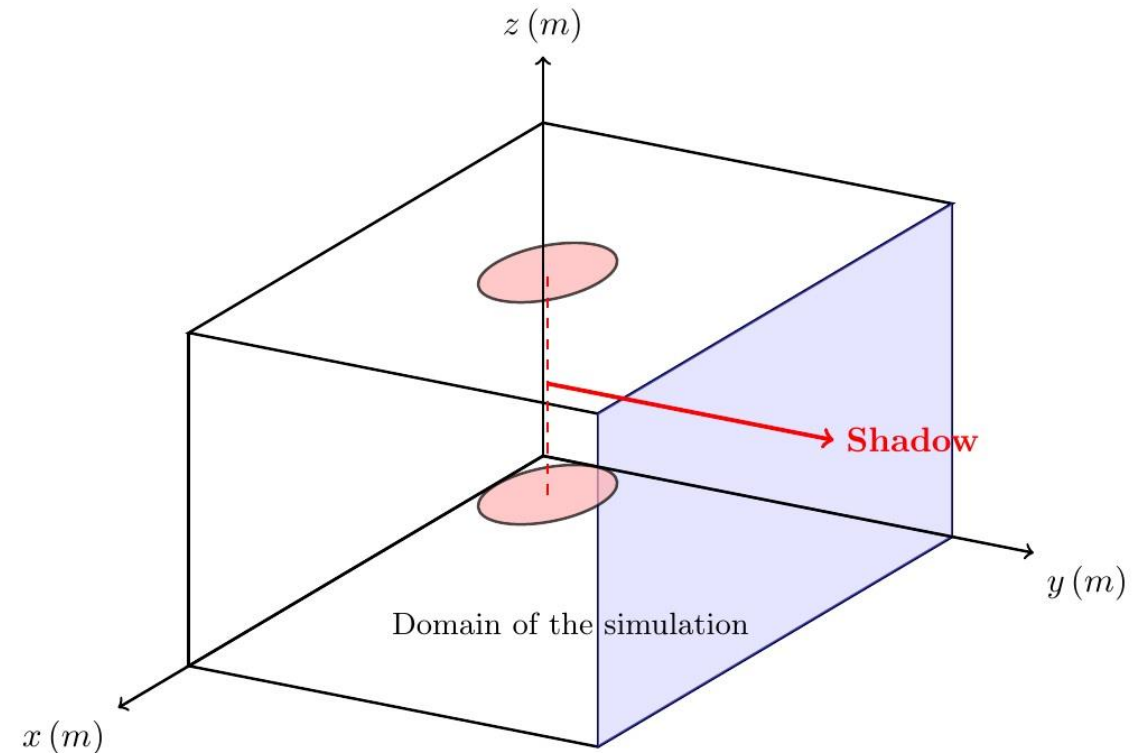
Background ISSR Profile: Gaussian-Like, Peaking up to 27% + Linear Negative Decay up to 8%

Initial Particles' Shape: Spherical

Initial Particles' Size: 1 micro-meter

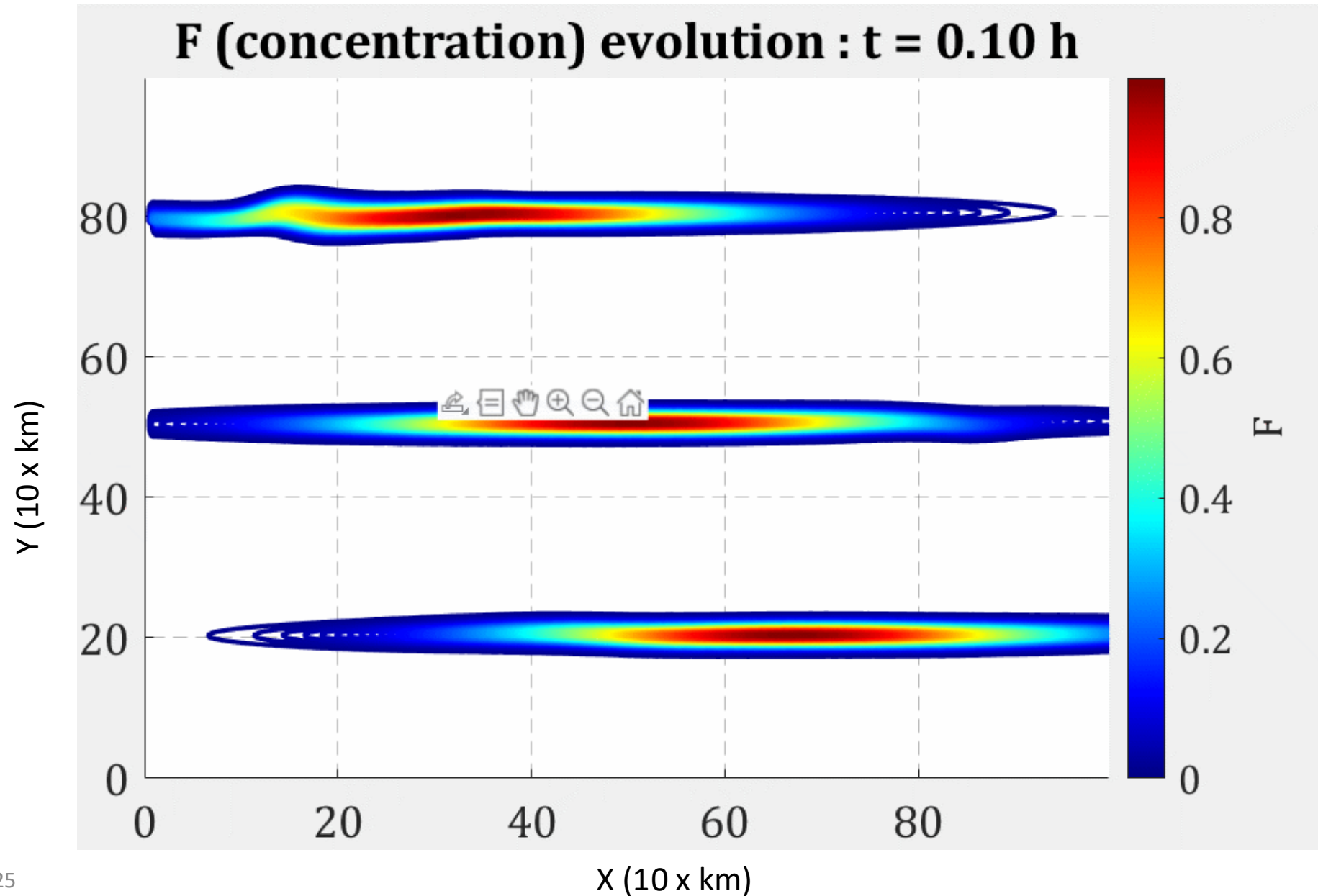


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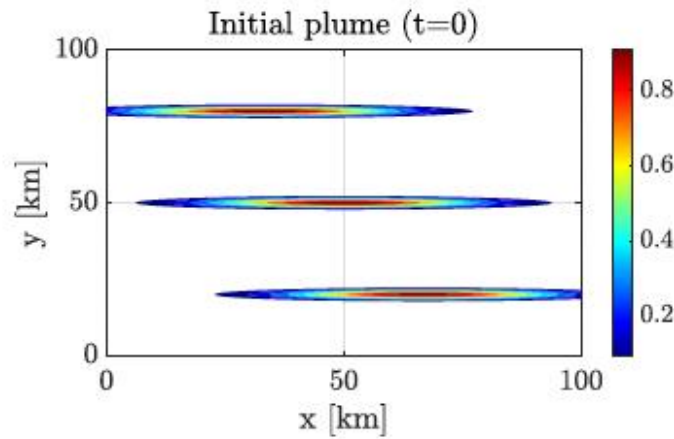




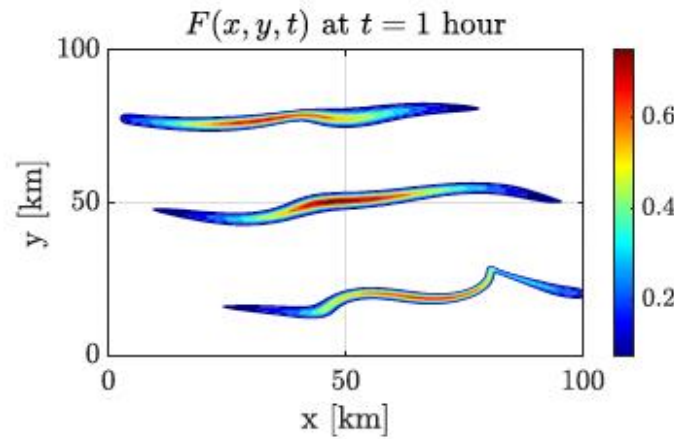
# Horizontal Evolution of the plume



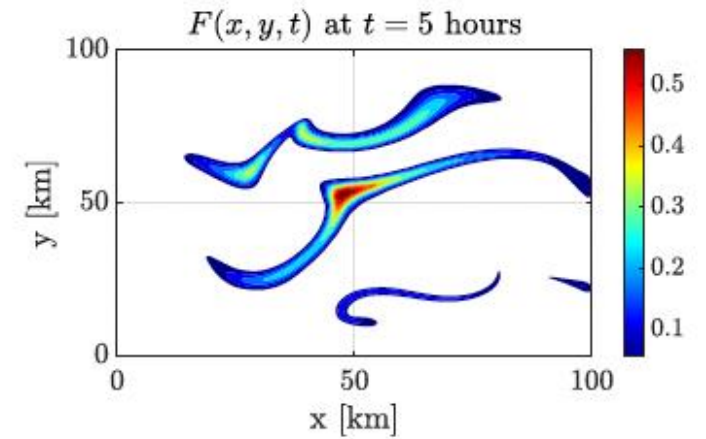
# Horizontal Evolution of the plume (diffusion-blocking coefficient)



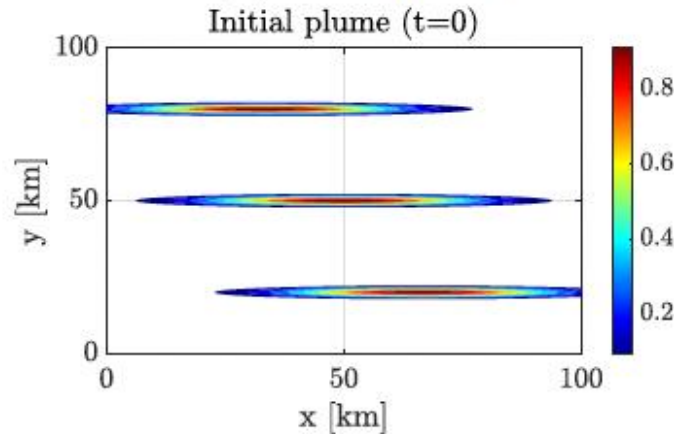
(a)  $\beta = 0, t = 0$



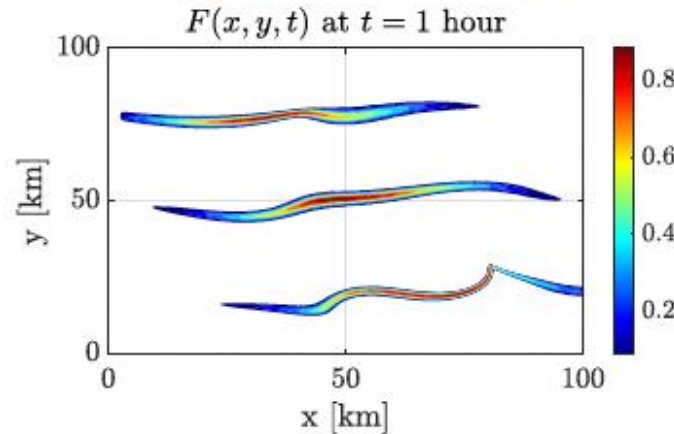
(b)  $\beta = 0, t = 1$  hour



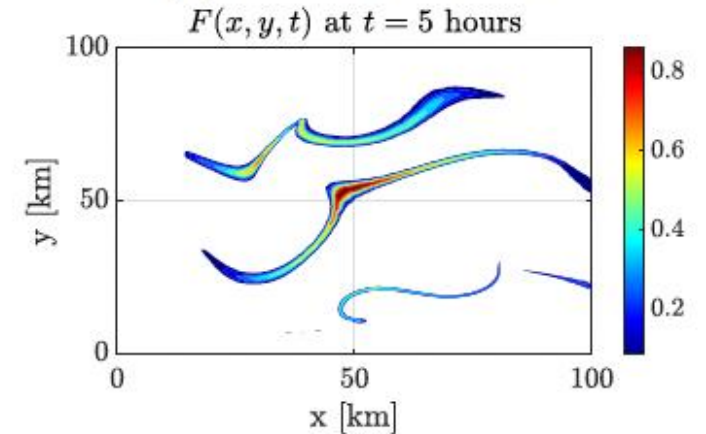
(c)  $\beta = 0, t = 5$  hours



(d)  $\beta = 1000, t = 0$



(e)  $\beta = 1000, t = 1$  hour

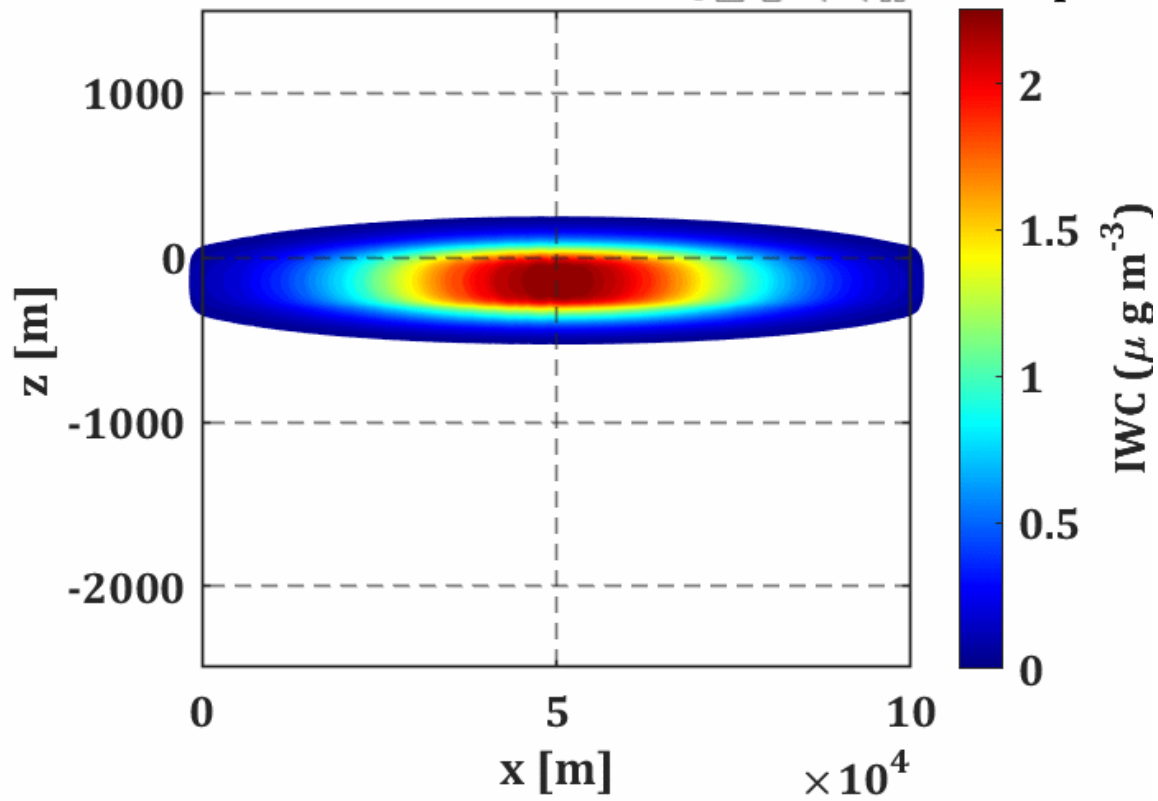


(f)  $\beta = 1000, t = 5$  hours

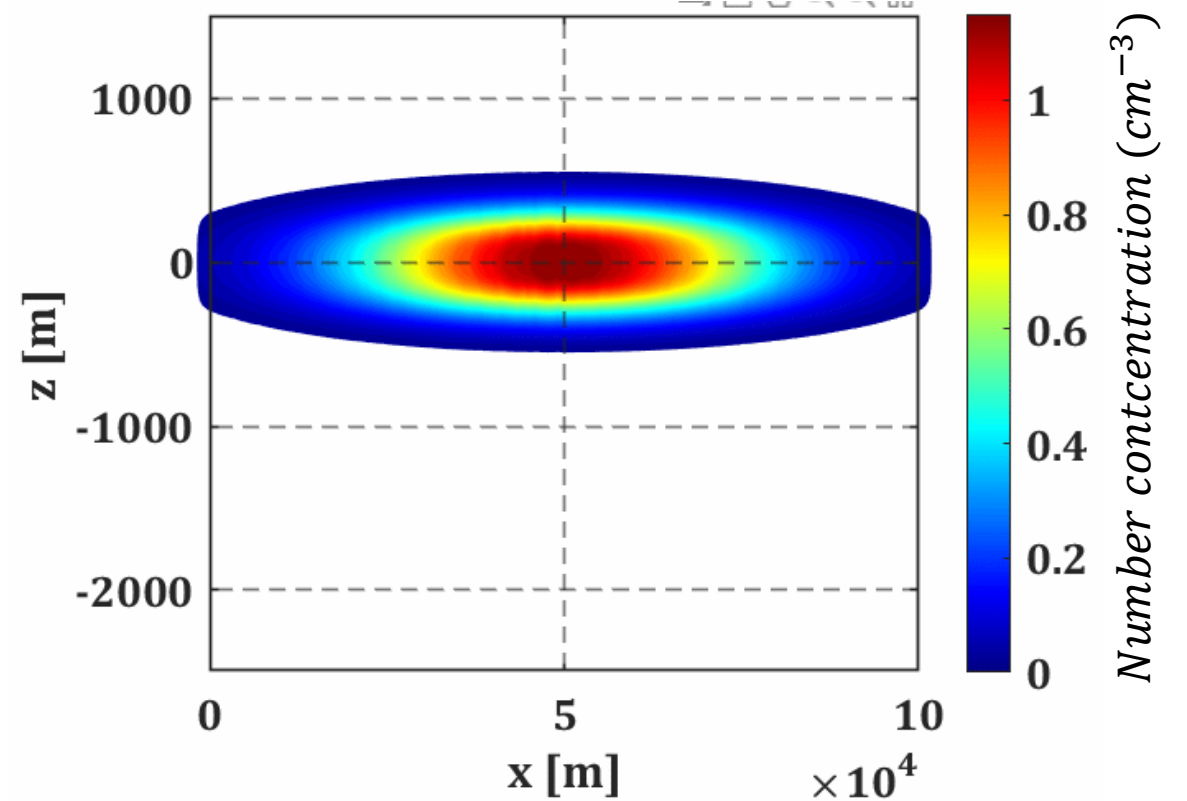
Horizontal evolution of  $F(x, y, t)$  –number concentration– for two diffusion-blocking coefficients  $\beta$

# Vertical Evolution of the plume

T=-61 C, ISSR Peak=17%  
Habit Dynamics Model



IWC: from about 3 mins to 6 hours with about 3 mins step



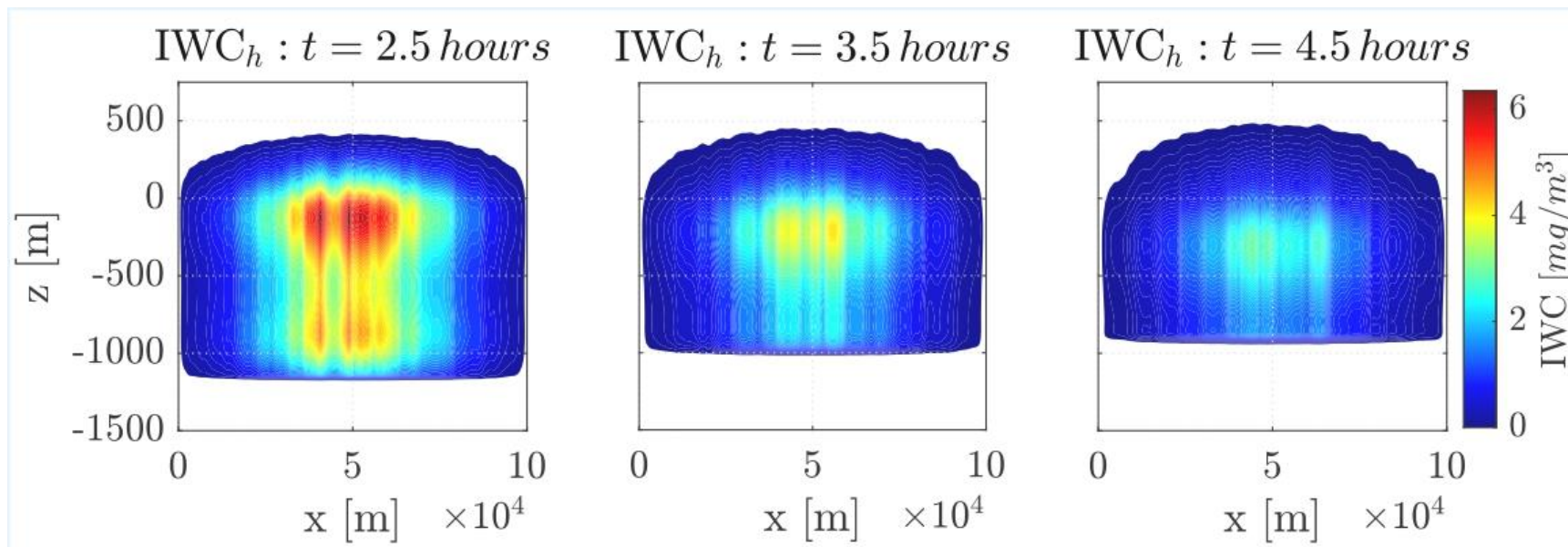
Number Cons.: from about 3 mins to 6 hours with about 3 mins step



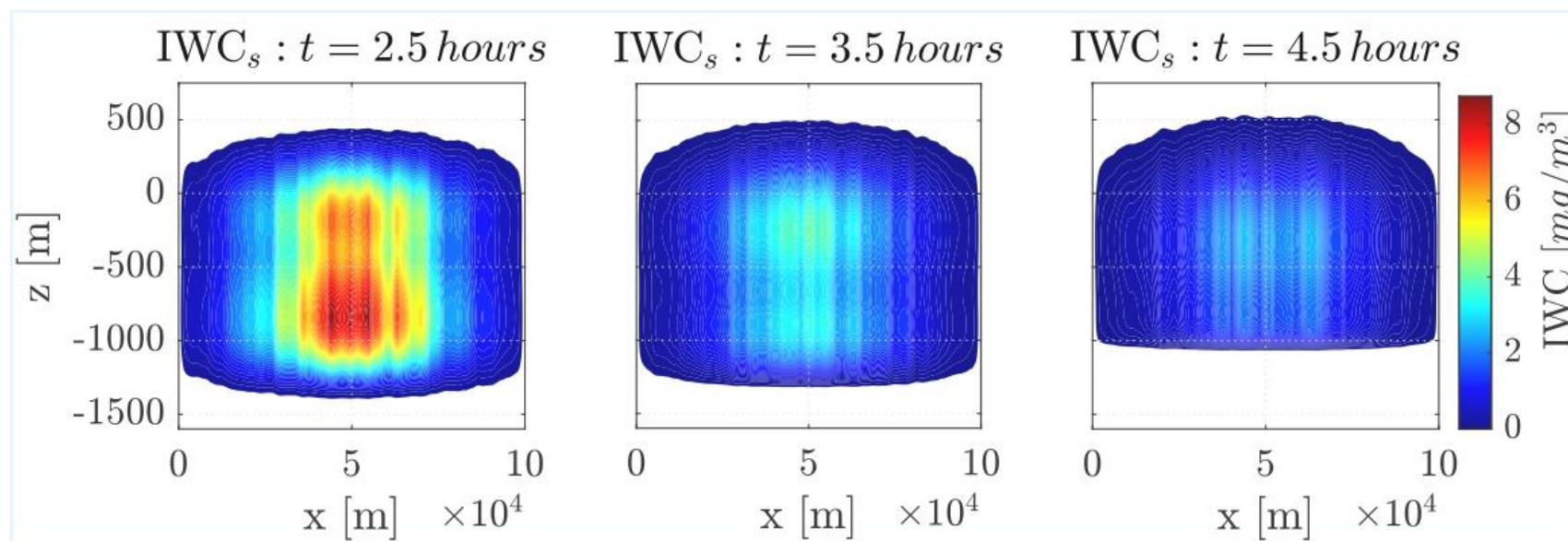
# Vertical Evolution of the plume: Habit vs. spherical model

$T = -61\text{ C}$ ,  
ISSR Peak = 17%

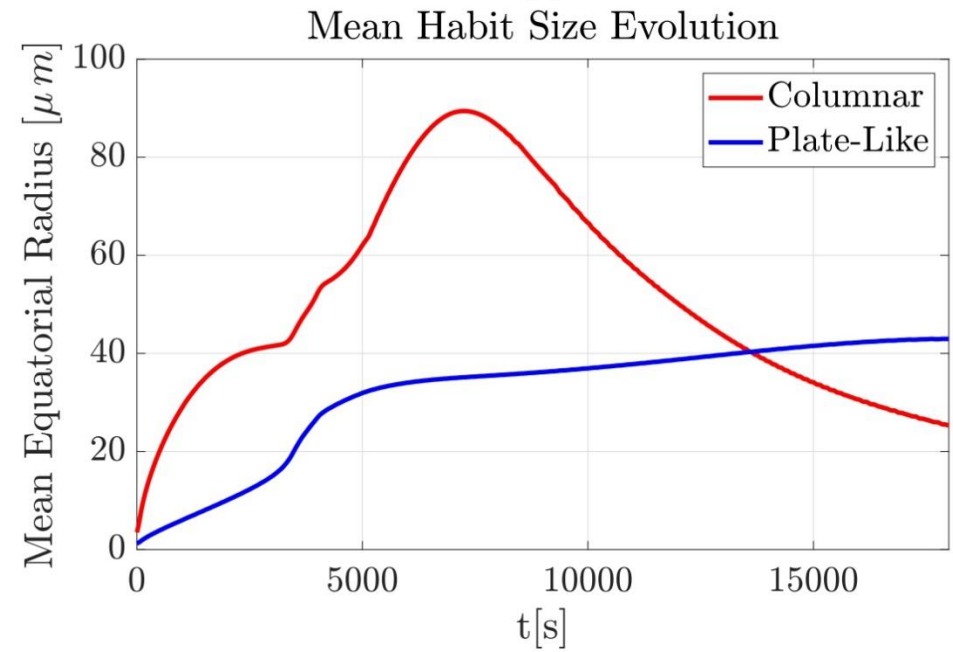
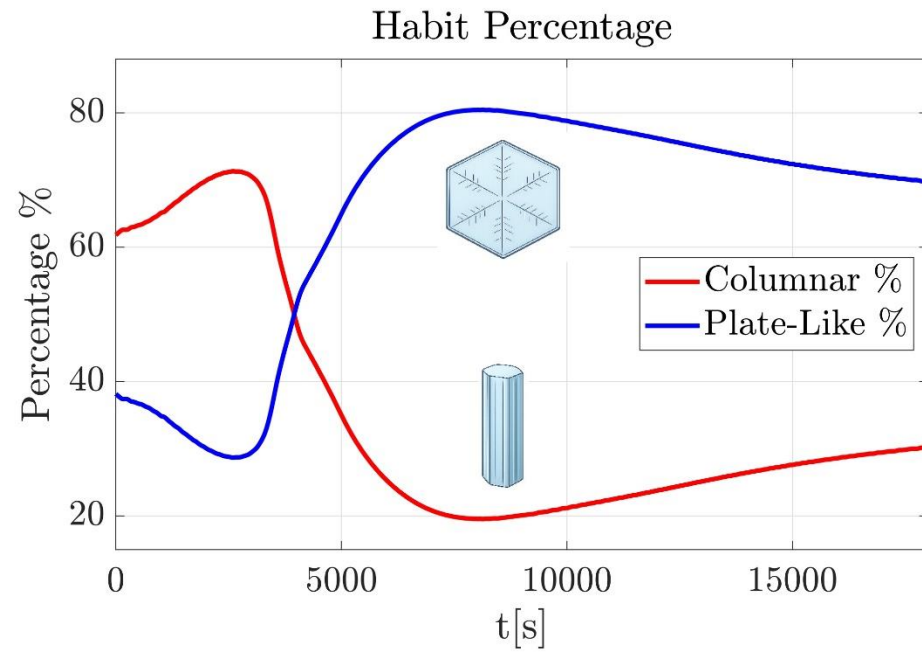
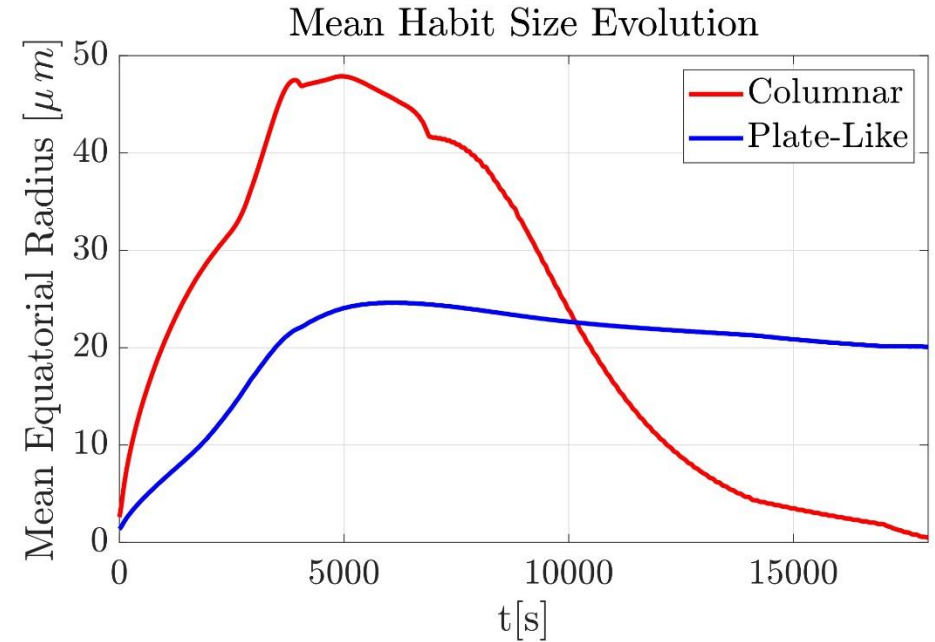
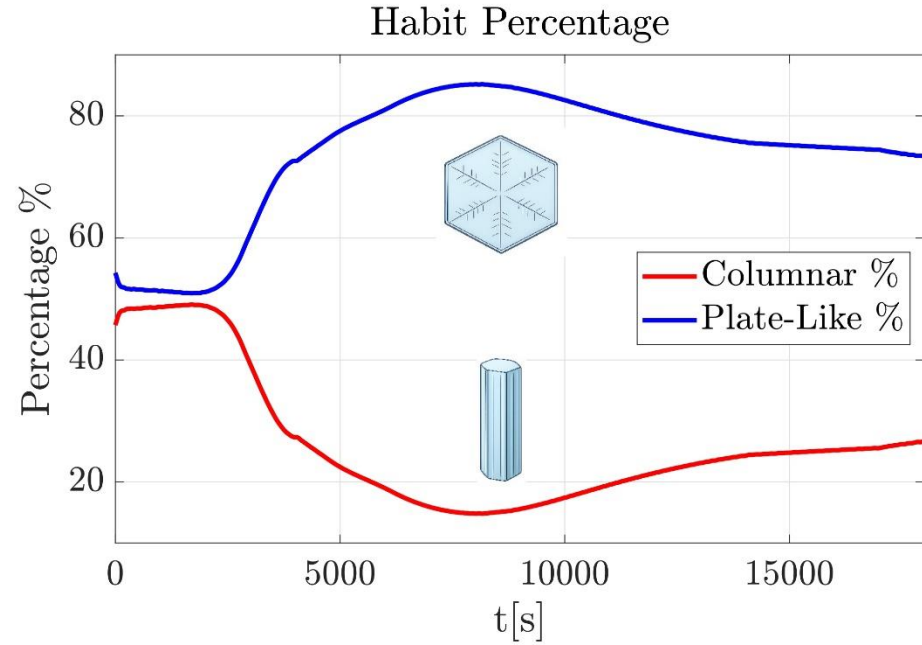
Habit Dynamics Model



Spherical Model

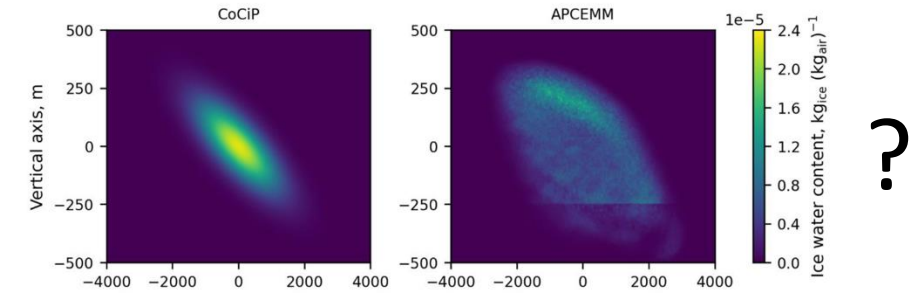


# Habit Shape

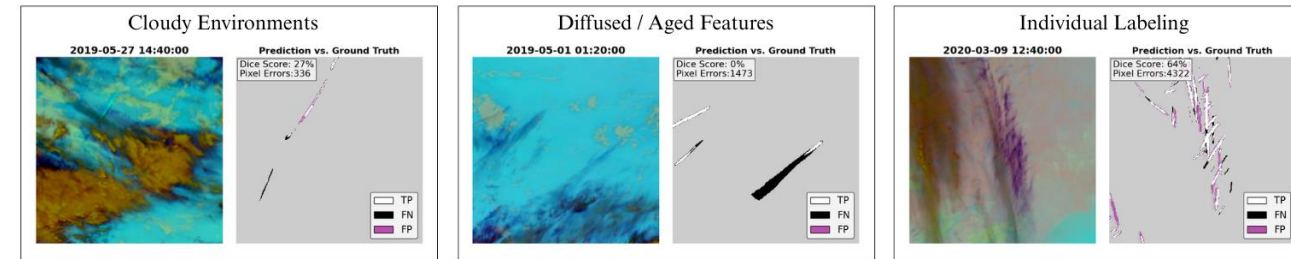


# (Some) Future Work

- Benchmarking w.r.t. state of the art contrail models (e.g., CoCiP and APCEMM)
- Validation using Remote sensing devices (e.g., EarthCARE LIDAR) & Ground Visible and IR Cameras.
- PINNs for contrail detection.
- Integrating/parametrizing short-range phases.
- Application to Monitoring Reporting and Verification.



Akhtar Martínez et al. (2025).



(Ortiz et al., 2025)

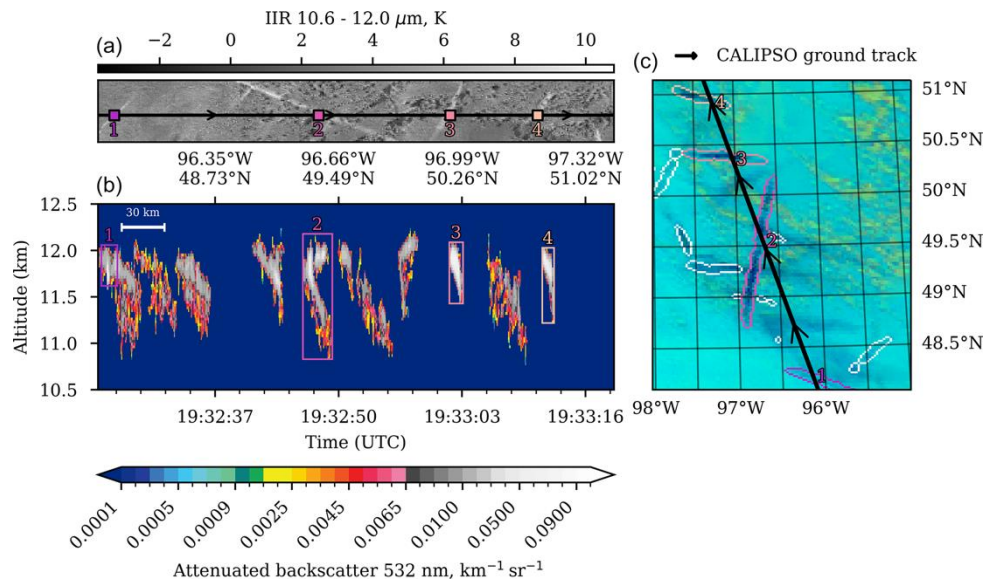
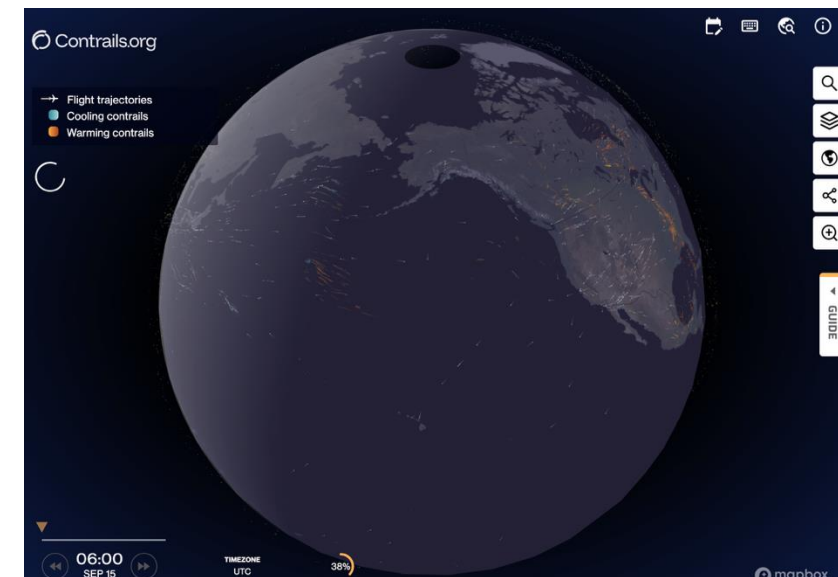


Figure 17: Example from Meijer et al. (2024) showing contrails detected in GOES-16 ABI imagery (c) located in CALIPSO LIDAR data (b). Contrails are numbered to enable comparison between the LIDAR cross-sections and the “top view” from the GOES-16 satellite.



Contrails.org visualization

# A Multi-Physics Eulerian Framework for Long-Term Contrail Evolution\*

*Contrails Analysis Workshop  
Imperial College, London, Sept 16–18, 2025*

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# Thanks!



# References

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- Jafarimoghaddam, A., & Soler, M. (2025). A Multi-Physics Eulerian Framework for Long-Term Contrail Evolution. *arXiv preprint arXiv:2509.00965*.