

PRINCIPLE OF FERMAT (Principle of Least Time)

$$\int_{P_1}^{P_2} n ds = \text{OPTICAL LENGTH}$$

"PATH LENGTH"

RAY = Shortest path between two points
(not necessarily straight line)

COMPARE TO GRAVITATIONAL
FIELD

FOURIER OPTICS

We treated refraction/reflection

Goodman:
Introduction to
Fourier Optics

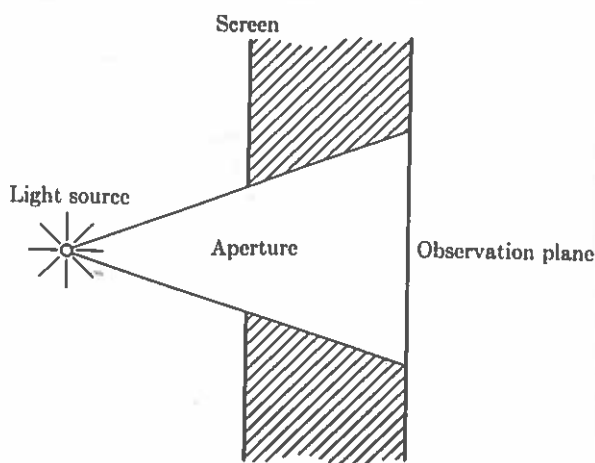
Now:

DIFFRACTION: Sommerfeld "Optics" (1954)

"any deviation of light rays from rectilinear paths which cannot be interpreted as reflection or refraction"

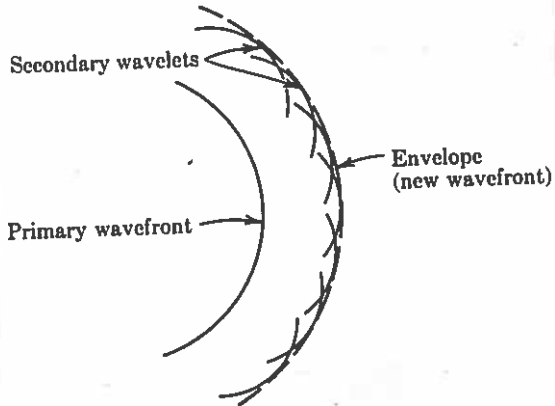
Wave nature \Leftrightarrow diffraction

Grimaldi 1665:



result not
explained by
corpuscular
theory of
light
propagation

Huygens : first proposed wave theory of light 1678



Time t_1 :
Each point on the wave front
new source of a
secondary wave

Time t_2 later :
Wavefront is envelope
of secondary
wavelets

Fresnel 1818 :

Huygens idea combined with Young's
idea of interference :
calculated diffraction patterns

↓
1882 - Kirchhoff mathematical foundation
Got it - by far - mostly right
- however did use two boundary
conditions proven inconsistent by
Poincaré' 1892 , Sommerfeld 1894

Follow Sommerfeld's corrective approach: ⁶³
1896

Scalar theory here (one component)

Sommerfeld \Leftrightarrow Feynman diagrams

spatial analysis, Green's functions
contributions to electric field amplitude in one
spatial point propagated thru Green's functions
from other space points

ALTERNATIVE (not widely used
in traditional physical
optics)

FOURIER OPTICS

Linear systems theory
used in

(Spatial) FREQUENCY ANALYSIS
of imaging system

electric circuit theory
communication theory:

e-m light field decomposed

typically in plane waves

= (SPATIAL) Fourier transformation

TRANSFER FUNCTION

basis functions

OUTPUT = \sum TRANSFORMED INPUT COMPONENTS

LINEARITY

Spatial FREQUENCY ANALYSIS of Imaging system
(TRANSFER FUNCTION)

Like

(temporal) FREQUENCY ANALYSIS for audio amplifier
characterization

Analysis

AND

Synthesis ← phase-contrast imaging

: frequency plane processing

filtering

LENS acts as FOURIER TRANSFORMER

FOURIER TRANSFORMATION SUMMARY :

Light field (e-m wave) = { spatial distribution of complex valued field amplitude =

for simple (lin. polarized) plane wave it would be $E_{0x} e^{ikz}$ $U(x, y, z)$

Pick z as propagation direction (like time in QM)

Input field = $U(x, y, z=0)$

Output field = $U(x, y, z=L)$

So generally : $g(x, y)$ (Complex valued field in 2 variables)

Fourier transform $FT \{g\} \equiv G :$

$G(l_x, l_y) = \iint_{-\infty}^{\infty} dx dy g(x, y) e^{-i2\pi(l_x x + l_y y)}$

spatial frequencies

$FT^{-1} \{G\} (x, y) = \iint_{-\infty}^{\infty} dl_x dl_y G(l_x, l_y) e^{i2\pi(l_x x + l_y y)} = g(x, y)$

So need to find response of system to

$$e^{i2\pi(l_x x + l_y y)} \text{ for each } (l_x, l_y)$$

* Fourier transform is linear

$$* \text{ FT } \{g(ax, by)\}(l_x, l_y) = \frac{1}{|ab|} \text{ FT } \{g\}\left(\frac{l_x}{a}, \frac{l_y}{b}\right)$$

contraction in space domain \leftrightarrow
stretching in frequency domain

$$* \text{ FT } \{g(x-a, y-b)\}(l_x, l_y) = \text{ FT } \{g\}(l_x, l_y) \cdot e^{-i2\pi(l_x a + l_y b)}$$

translation in space \leftrightarrow
phase shift in frequency domain

* Parseval's theorem: $G \equiv \text{ FT } \{g\}$:

$$\iint dx dy |g(x, y)|^2 = \iint dl_x dl_y |G(l_x, l_y)|^2$$

* Separable function : $g(x, y) = g_x(x) g_y(y)$:

$$\text{ FT } \{g\}(l_x, l_y) = \text{ FT}_x \{g_x\}(l_x) \cdot \text{ FT}_y \{g_y\}(l_y)$$

* CONVOLUTION THEOREM :

$$FT\{g\} = G \quad ; \quad FT\{h\} = H :$$

$$FT\left\{\iint_{-\infty}^{\infty} dx' dy' g(x', y') h(x-x', y-y')\right\}(fx, fy)$$

$$= G(fx, fy) \cdot H(fx, fy)$$

! !

SEPARABLE IN POLAR COORDINATES :

More Complicated ; simplest case :

IMPORTANT \longrightarrow circular symmetry case

$$g(r, \theta) = g(r)$$

$$r = \sqrt{x^2 + y^2} ; \theta = \tan^{-1}\left(\frac{y}{x}\right)$$

FT $\{g\} = G \leftarrow$ function of f_x, f_y or $\rho, \phi :$

$$\rho = \sqrt{f_x^2 + f_y^2} ; \phi = \tan^{-1}\left(\frac{f_y}{f_x}\right)$$

$$G(\rho, \phi) = \int_0^\infty dr \cdot r g(r) \int_0^{2\pi} d\theta e^{-i2\pi r \rho \cos(\theta - \phi)}$$

Use: $= \underline{G(\rho)}$ \leftarrow Circular symmetry also
 J_0 : Bessel function of the first kind, zero order :

$$J_0(a) = \frac{1}{2\pi} \int_0^{2\pi} e^{-ia \cos \theta} \cdot d\theta$$

$$G(\rho) = 2\pi \int_0^\infty dr \cdot r g(r) J_0(2\pi r \rho)$$

\nearrow one-dim. transform : Fourier - Bessel transform

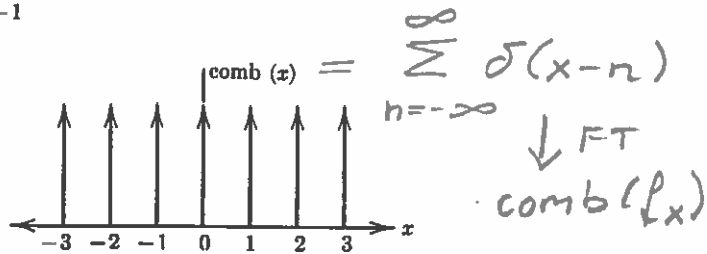
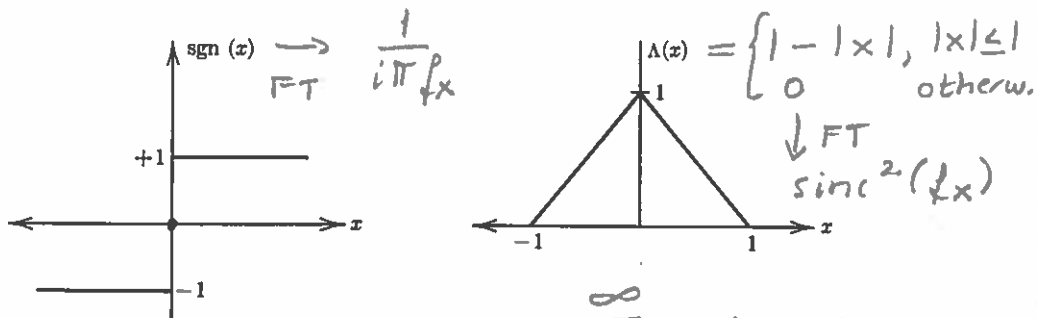
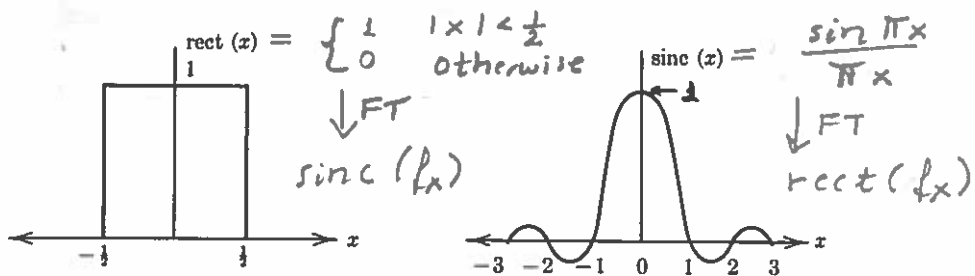
Idealized point source of light :

Dirac δ function

$$\delta(x, y) = \lim_{N \rightarrow \infty} N^2 e^{-N^2 \pi (x^2 + y^2)}$$

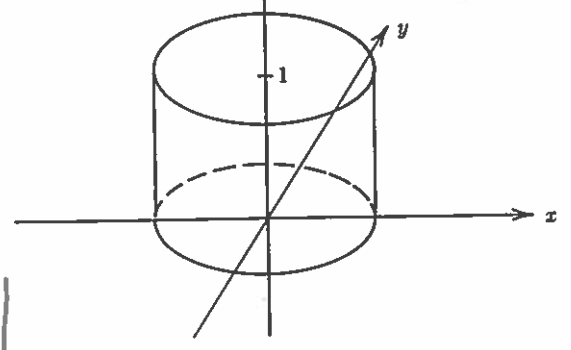
$$FT\{\delta\} = \lim_{N \rightarrow \infty} FT\left\{ \underbrace{N^2 e^{-N^2 \pi (x^2 + y^2)}}_{\downarrow} \right\} = \lim_{N \rightarrow \infty} e^{-\pi (f_x^2 + f_y^2) / N^2}$$

$$= e^{-0} = \underline{\underline{1}}$$



2 DIM. FT :

$$\text{circ}(r) = \begin{cases} 1 & r = \sqrt{x^2 + y^2} \leq 1 \\ 0 & \text{otherwise} \end{cases}$$

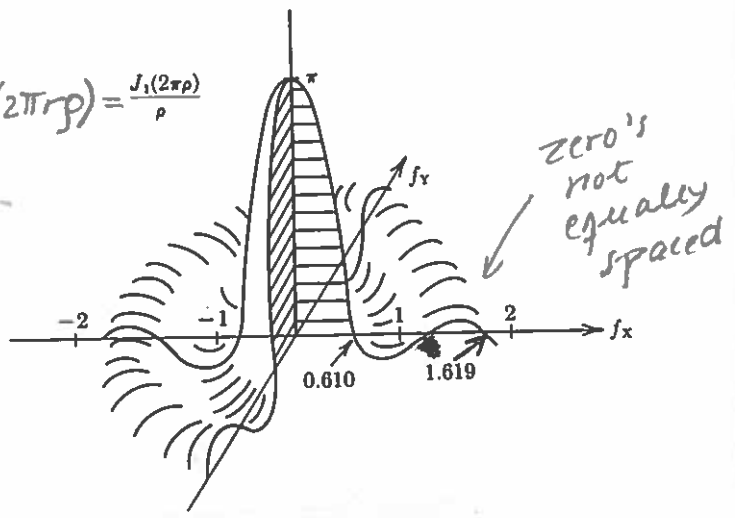


← aperture!

FT ↓

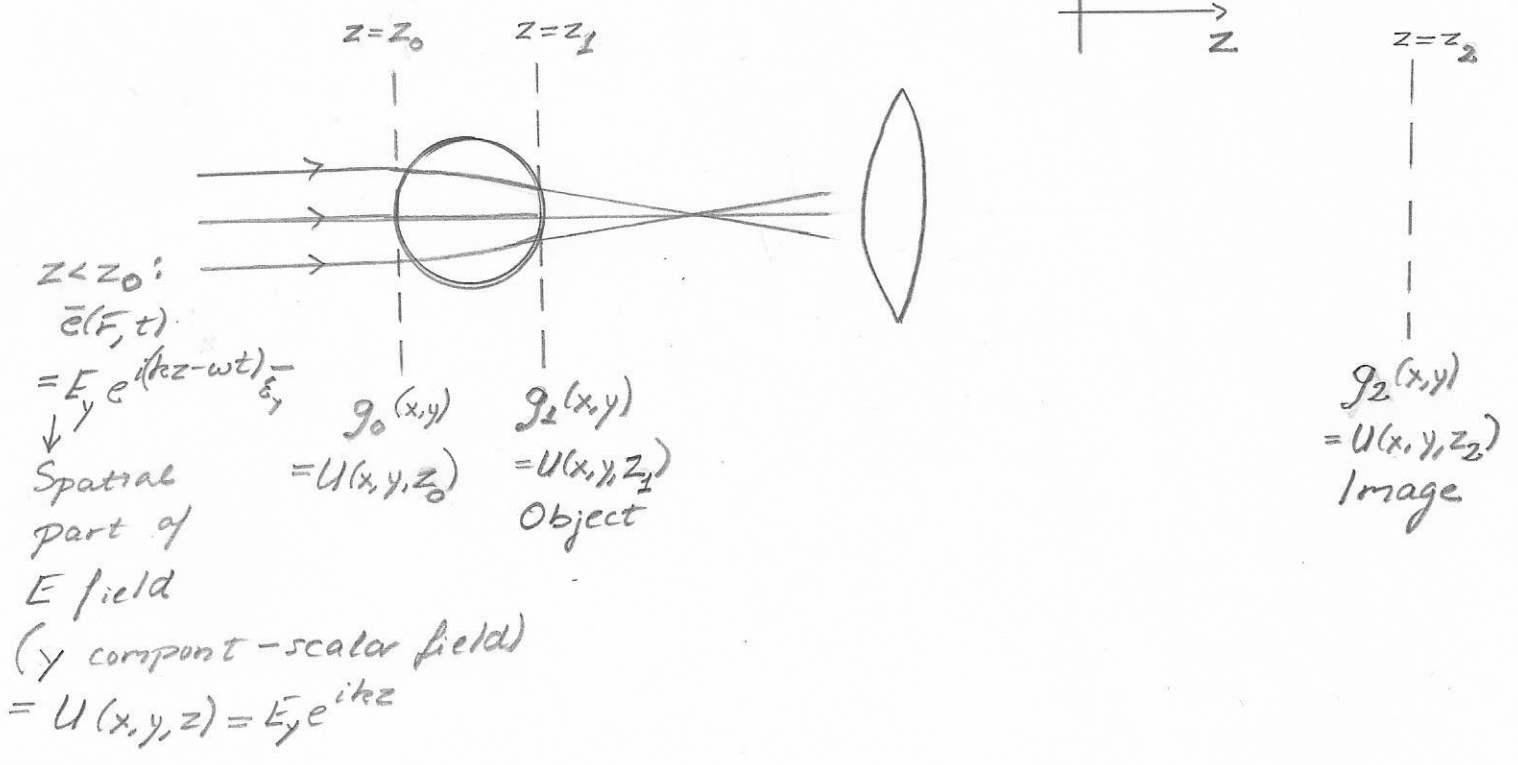
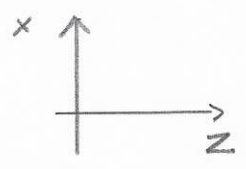
$$2\pi \int_0^{\infty} dr \cdot r \cdot g(r) J_0(2\pi r \rho) = \frac{J_1(2\pi \rho)}{\rho}$$

$\begin{matrix} \infty \rightarrow 1 \\ \downarrow \\ 1 \end{matrix}$



$$\int_0^x dy y \cdot J_0(y) = x J_1(x)$$

Bessel func.
1st kind
order 1



MORE GENERALLY :

$U(x, y, z) =$ complex field (representing

$E(x, y, z)$ or $B(x, y, z)$: both single components in scalar theory).

Spatial part of solutions to Maxwell eqs. Temporal part : $e^{-i\omega t}$.

PROPAGATION IN SPACE:

$$\begin{array}{ccc}
 U(x, y, z=0) & \longrightarrow & U(x, y, z=L) \\
 \parallel & & \parallel \\
 g_1(x, y) & & g_2(x, y)
 \end{array}$$

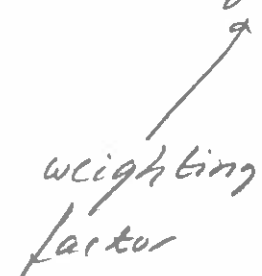
Mapping S : $g_2 = S\{g_1\}$

Linear systems: S linear

One possible way of decomposing input into elementary input functions:

Use δ functions:

$$g_1(x, y) = \iint_{-\infty}^{\infty} dx' dy' g_1(x', y') \delta(x-x', y-y')$$



weighting factor

Linearity - we just need to find

$$S\{\delta(x-x', y-y')\} \equiv h(x_2, y_2; x', y')$$

IMPULSE
 \equiv response of system at x_2, y_2 in $z=L$ plane to δ -function input at x', y' in $z=0$ plane

$$g_2(x_2, y_2) = \iint dx' dy' g_1(x', y') h(x_2, y_2; x', y')$$

$$h(x_2, y_2; x', y')$$

exactly equivalent to Feynman path integral propagator in 2D quantum mechanics with z acting as time coordinate

so just need to know response of all point sources in object plane

(Ref.: Feynman & Hibbs Quantum Mechanics and Integrals)

Space invariance:

$$h(x_2, y_2; x', y') = h(x_2 - x'; y_2 - y')$$

$$\therefore g_2(x_2, y_2) = \iint dx' dy' g_1(x', y') h(x_2 - x', y_2 - y')$$

convolution integral

$$FT\{g_2\}(f_x, f_y) = \underbrace{FT\{g_1\}(f_x, f_y)}_{\text{Fourier transform of input field in object plane}} \cdot \underbrace{FT\{h\}(f_x, f_y)}_{\text{Fourier transform of impulse response}}$$

Fourier transform of input field in object plane

Fourier transform of impulse response

$$H(f_x, f_y)$$

TRANSFER FUNCTION for imaging sys

effects in freq. domain

So: CONVOLUTION INTEGRAL complicated



PRODUCT

Simple

BEST BASIS for linear, space invariant syst.

PLANE WAVES

$$g_1(x, y) = \iint d p_x d p_y G_1(p_x, p_y) e^{i 2 \pi (p_x x + p_y y)}$$

↑
FT{g₁}

$$g_2(x, y) = \iint d p_x d p_y G_2(p_x, p_y) \cdot \underbrace{H(p_x, p_y)} e^{i 2 \pi (p_x x + p_y y)}$$

simple multiplication w/ complex number

gives response to basis function input

FOURIER OPTICS view of DIFFRACTION 75

1) Free space propagation: find transfer function $H(f_x, f_y)$

(see notes p. 73)

$$U(x, y, z=0) \xrightarrow{\hspace{10em}} U(x, y, z=L)$$

$$U(x, y, 0) = \iint A_0(f_x, f_y) e^{i2\pi(f_x x + f_y y)} df_x df_y$$

$$A_0 = \iint U(x, y, z=0) e^{-i2\pi(f_x x + f_y y)} dx dy$$

AND (generally)

$$U(x, y, z) = \iint A(f_x, f_y; z) e^{i2\pi(f_x x + f_y y)} df_x df_y$$

U satisfies Helmholtz' wave equation IN FREE SPACE:

$$\nabla^2 U + \underbrace{\epsilon \mu \omega^2}_{k^2} U = 0 \quad \text{so}$$

$$0 = \frac{d^2}{dz^2} A(f_x, f_y; z) + (k^2 - (2\pi f_x)^2 - (2\pi f_y)^2) A(f_x, f_y; z)$$

$$\Rightarrow A(f_x, f_y; z) = A_0(f_x, f_y) e^{i \underbrace{\sqrt{k^2 - (2\pi f_x)^2 - (2\pi f_y)^2}}_{k_z} z}$$

Note:

Remember : wave equation predicted by
Maxwell's eqs :

$$\nabla^2 \bar{e} = \epsilon \mu \frac{\partial^2 \bar{e}}{\partial t^2} \quad \bar{e}(\vec{r}, t)$$

$$\nabla^2 \bar{E} = -\epsilon \mu \omega^2 \bar{E} \quad \parallel \quad e^{-i\omega t} \bar{E}(\vec{r})$$

$1/c^2$ in free space
Helmholtz eq.

Here scalar theory of diffraction:
consider i.e. $E_x(\vec{r}) \equiv U(\vec{r})$



TRANSFER FUNCTION

for propagation in free space thru distance z :

$$H(f_x, f_y) = \frac{A(f_x, f_y; z)}{A_0(f_x, f_y)} = e^{i \sqrt{k^2 - (2\pi f_x)^2 - (2\pi f_y)^2} \cdot z}$$

$\equiv e^{ik_z z}$

↑
phase change
dependent on f_x, f_y

AND

 z

So: Like 2D QUANTUM MECHANICS

$$\begin{aligned} \text{time} &= (-) \hbar / c \\ \text{energy} &= \hbar \omega \sqrt{1 - k_{\perp}^2 / k^2} \end{aligned}$$

$$U(x, y; z) =$$

$$= \iint dx dy A_0(f_x, f_y) \cdot e^{i 2\pi (f_x x + f_y y)} \cdot e^{ik_z z}$$

$$k_z z \equiv \sqrt{k^2 - (2\pi f_x)^2 - (2\pi f_y)^2} z = z \cdot \overbrace{\omega \sqrt{\epsilon \mu}}^k \cdot \sqrt{1 - \frac{k_{\perp}^2}{k^2}}$$

$$\omega \sqrt{\epsilon_0 \mu_0} = \omega / c \quad \uparrow$$

$$e^{ik_z z} = e^{i \frac{z}{c} \cdot \omega \sqrt{1 - k_{\perp}^2 / k^2}}$$

$$\leftarrow \boxed{k_{\perp} = (2\pi f_x, 2\pi f_y)}$$

2) Diffraction: { just need to
find transfer function $H(f_x, f_y)$
thru aperture and multiply
with free-space transfer function

(78)

Sommerfeld boundary condition:

Screen placed
at $z=0$:

$$U(x, y; z=0^+)$$

$$= U(x, y, z=0^-) \cdot t(x, y)$$

t = transmittance function

of aperture Σ (with arbitrary shape):

$$t(x, y) = \begin{cases} 1 & (x, y) \text{ in } \Sigma \\ 0 & \text{otherwise} \end{cases}$$

Use convolution theorem:

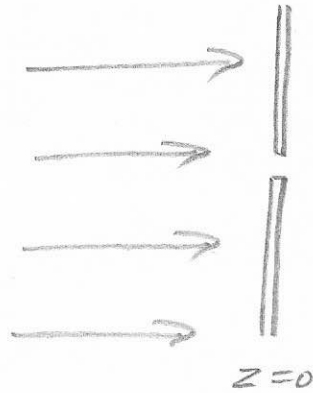
$$T = FT\{t\} :$$

$$FT\{U(x, y; z=0^+)\} = \text{CONVOLUTION OF} \\ FT\{U(x, y; z=0^-\} \text{ and } T$$

FOR EXAMPLE:

(79)

PLANE WAVE hitting aperture
at normal incidence:



$U(x, y; z=0^-)$ is
uniform, say 1.

Then:

$$\text{FT}(U(x, y; z=0^-)) \\ = \delta(l_x, l_y), \text{ and}$$

$$\text{FT}\{U(x, y; z=0^+)\}(l_x, l_y) = \delta(l_x', l_y')$$
$$= \iint dx' dy' \text{FT}\{U(x, y; z=0^-)\}(l_x', l_y')$$

$$\cdot T(l_x - l_x', l_y - l_y')$$

$$= T(l_x, l_y) = \text{Fourier transform of aperture transmission function}$$

If circle aperture } : $t(r) = \text{circ}(r/a)$
radius a $T(\rho) = \frac{J_1(2\pi\rho a) \cdot a^2}{\rho a}$

see notes p. (70)

DIFFRACTION RESULT :

(80)

So : APERTURE

BROADENS MOMENTUM SPREAD $\hbar(2\pi/x, 2\pi/y)$

OF LIGHT FIELD AS

$\Delta p \propto \frac{\hbar}{a}$: The smaller the

aperture the bigger the
momentum spread.

First node in 1st order Bessel function J_1 :

at $pa = 0.610 \Rightarrow \Delta p = \frac{0.610}{a} \cdot 2\pi \cdot \hbar = 0.610 \frac{\hbar}{a}$

Uncertainty principle

FRESNEL & FRAUNHOFER DIFFRACTION

(81)

We found transfer function for propagation of distance z in free space:

$$H(f_x, f_y) = e^{i \sqrt{k^2 - (2\pi f_x)^2 - (2\pi f_y)^2} \cdot z} \quad \text{Exact (p. 77)}$$

$$k = \frac{\omega}{c}$$

Fresnel approximation: $2\pi \sqrt{f_x^2 + f_y^2} \ll k$:

$$H(f_x, f_y) \approx e^{ikz} e^{-i\pi\lambda z (f_x^2 + f_y^2)} \quad ; \lambda = \frac{2\pi}{k}$$

$$FT\{U(x, y, z)\} = FT\{U(x, y, z=0)\} \cdot H(f_x, f_y) :$$

$$(*) U(x_1, y_1, z) \approx \frac{e^{ikz}}{i\lambda z} \int dx_0 \int dy_0 e^{i \frac{k}{2z} ((x_1 - x_0)^2 + (y_1 - y_0)^2)} U(x_0, y_0, z=0)$$

↑ spatial version of Fresnel approximation

Rewrite eq. (*):

$$U(x_1, y_1, z) = \frac{e^{ikz}}{i\lambda z} e^{i \frac{k}{2z} (x_1^2 + y_1^2)} \iint dx_0 dy_0 e^{i \frac{k}{2z} (x_0^2 + y_0^2)} U(x_0, y_0, z=0) \cdot e^{-i \frac{k}{z} (x_0 x_1 + y_0 y_1)}$$

$$= \frac{e^{ikz}}{i\lambda z} e^{i \frac{k}{2z} (x_1^2 + y_1^2)} FT\{e^{i \frac{k}{2z} (x^2 + y^2)} U(x, y, z=0)\} (f_x, f_y)$$

$$f_x = \frac{x_1}{z\lambda} \quad ; \quad f_y = \frac{y_1}{z\lambda}$$

Fraunhofer Approx. is :

$$FT \left\{ U(x, y, z=0) e^{i \frac{k}{2z} (x^2 + y^2)} \right\}$$

neglect

$$\frac{k}{2z} (x^2 + y^2) \ll 1$$

1mm aperture
6000 Å red light
z → 2.5m

So :

$$U(x_1, y_1, z) = \frac{e^{ikz}}{i\lambda z} e^{i \frac{k}{2z} (x_1^2 + y_1^2)} FT \{ U(x, y, z=0) \} (f_x, f_y)$$

$$U(x, y, z) \quad (f_x, f_y) = \frac{k}{2\pi z} (x_1, y_1)$$

So diffraction pattern at distance z is obtained from Fourier transform of field distribution right after aperture.

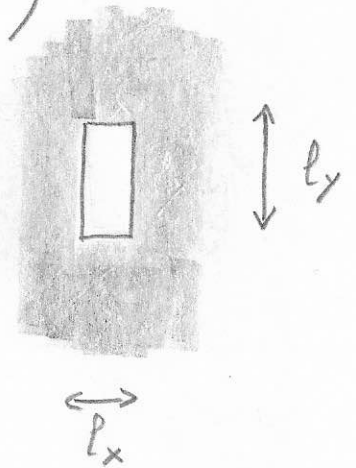
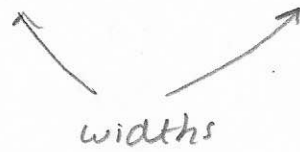
$$U(x, y, z=0^+)$$

So apart from phase factor $\frac{e^{ikz}}{i}$ and amplitude factor $\frac{1}{\lambda z}$

free space propagation in Fraunhofer regime acts as Fourier transformer.

Rectangular aperture:

$$t(x, y) = \text{rect}\left(\frac{x}{l_x}\right) \cdot \text{rect}\left(\frac{y}{l_y}\right)$$



Irradiate with orthogonal plane wave:

$$U(x_1, y_1; z) = \frac{e^{ikz}}{i\lambda z} e^{i\frac{k}{2z}(x_1^2 + y_1^2)} \cdot \text{FT}\{t(x, y)\}(f_x, f_y)$$

Fraunhofer

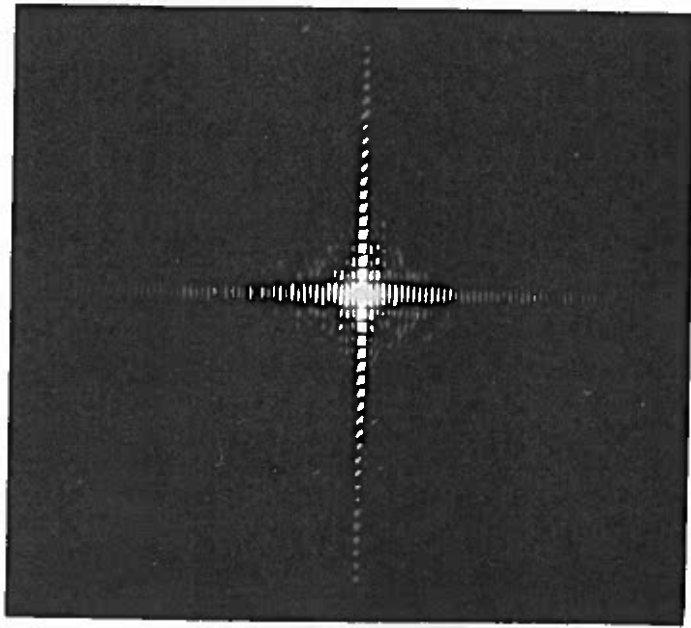
$$(f_x, f_y) = \frac{k}{2\pi z} (x_1, y_1)$$

$$\text{FT}\{t(x, y)\} = l_x l_y \text{sinc}(l_x f_x) \text{sinc}(l_y f_y)$$

$$\text{sinc } x = \frac{\sin \pi x}{\pi x}$$

$$\text{Eye: Intensity} \propto |U(x_1, y_1; z)|^2$$

$$= \frac{l_x^2 l_y^2}{\lambda^2 z^2} \text{sinc}^2 \frac{l_x x_1}{\lambda z} \text{sinc}^2 \frac{l_y y_1}{\lambda z}$$



Fraunhofer of
square slit

$$\begin{array}{c} l_x \\ \boxed{} \end{array} l_y$$

$$l_x = 2l_y$$

$$\text{Width of central spot} = \begin{cases} \frac{\lambda z}{l_x} \cdot 2 & \text{along } x \\ \frac{\lambda z}{l_y} \cdot 2 & \text{along } y \end{cases}$$

Circular aperture

Radius a : $t(x, y) = t(r) = \text{circ}\left(\frac{r}{a}\right)$

Irradiate with orthogonal plane wave :

$$U(x_1, y_1; z) = U(r_1; z) = \frac{e^{ikz}}{i\lambda z} e^{i\frac{k}{2z} r_1^2} \text{FT}\left\{U(r; z=0)\right\}(p_x, p_y)$$

$$(p_x, p_y) = \frac{1}{\lambda z} (x_1, y_1)$$

Bessel transform (circle symmetry)

$$\text{FT}\left\{\text{circ}\left(\frac{r}{a}\right)\right\}_{\rho = \sqrt{p_x^2 + p_y^2}} = a^2 \frac{J_1(2\pi a \rho)}{a \rho}$$

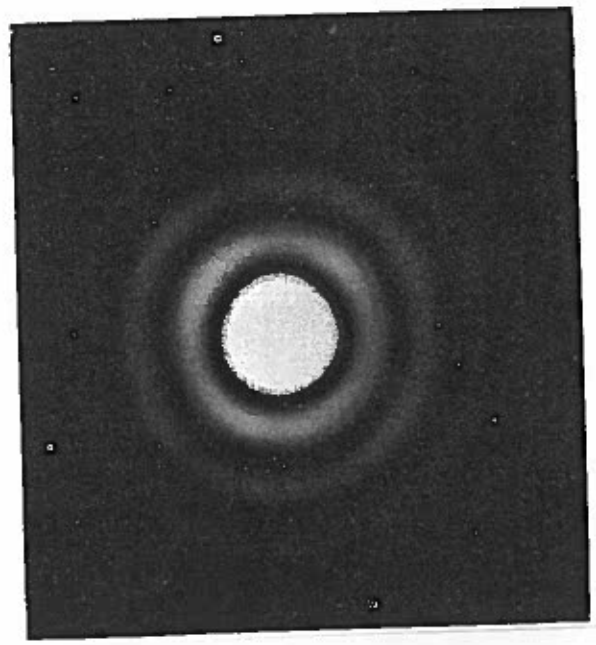
$$\rho = \frac{1}{\lambda z} \cdot r_1$$

$$\text{Fraunhofer} = \frac{e^{ikz}}{i\lambda z} \cdot e^{i\frac{k}{2z} r_1^2} \cdot a^2 \frac{J_1(2\pi a r_1 / (\lambda z))}{a \cdot r_1 / (\lambda z)}$$

$$\text{Intensity} = |U(x_1, y_1; z)|^2 = \left(\frac{k a^2}{\lambda z}\right)^2 \left(\frac{J_1\left(\frac{k a r_1}{z}\right)}{k a r_1 / z}\right)^2$$

$$= \text{AIRY PATTERN}$$

FRAUNHOFER
OF
ROUND
APERTURE
radius = a



AIRY
PATTERN

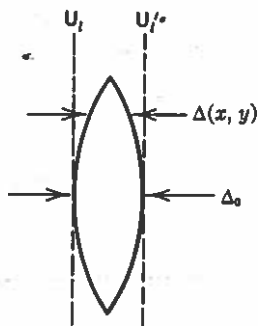
Diameter of central spot =
$$= 1.22 \cdot \frac{\lambda z}{a}$$

LENSES

1) FOURIER TRANSFORMER

2) IMAGING

What are they



GLASS
with index
 $n \sim 1.5$

Thin lens if position does not change:

$(x, y)_i = (x, y)_o$ in ray sense:

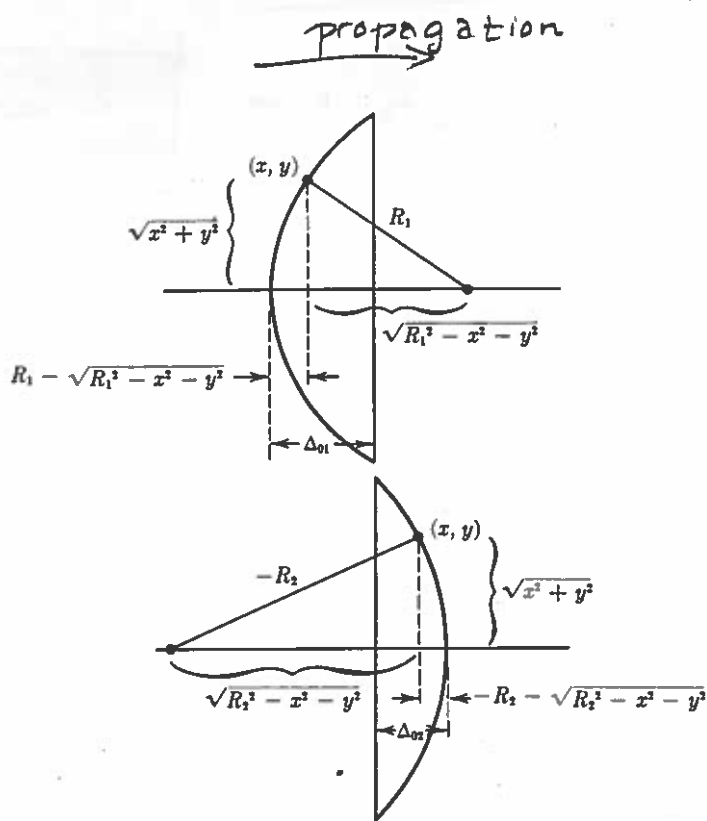
Phase shifter $t_e(x, y)$:

$$U_o(x, y) = t_e(x, y) U_e(x, y)$$

$t_e(x, y) =$:

thickness function $\Delta(x, y)$ in lens in free space
 phase delay = $\phi(x, y) = kn\Delta(x, y) + k(\Delta_0 - \Delta(x, y))$

FIND $\Delta(x, y) = \text{thickness function of lens}$ (88)



PART 1

POS RAD. OF CURVATURE
 R_1

PART 2

NEG RAD. OF CURVATURE
 R_2

$$\Delta(x, y) = \Delta_1(x, y) + \Delta_2(x, y)$$

$$\Delta_1(x, y) = \Delta_{01} - (R_1 - \sqrt{R_1^2 - x^2 - y^2})$$

$$\Delta_2(x, y) = \Delta_{02} - \underbrace{(-R_2 - \sqrt{R_2^2 - x^2 - y^2})}_{\text{POS}}$$

$$\Delta(x, y) = \underbrace{\Delta_{01} + \Delta_{02}}_{\Delta_0} - R_1 \left(1 - \sqrt{1 - \frac{x^2 + y^2}{R_1^2}}\right) + R_2 \left(1 - \sqrt{1 - \frac{x^2 + y^2}{R_2^2}}\right)$$

PARAXIAL APPROX:

$$\sqrt{1 - \frac{x^2 + y^2}{R_i^2}} \approx 1 - \frac{x^2 + y^2}{2R_i^2} \quad ; \quad i = 1, 2$$

So: $\Delta(x,y) = \Delta_0 - \frac{x^2+y^2}{2} \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$

Lens action

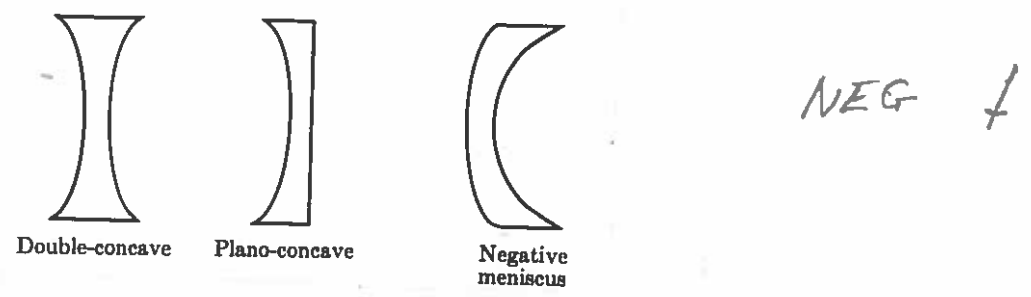
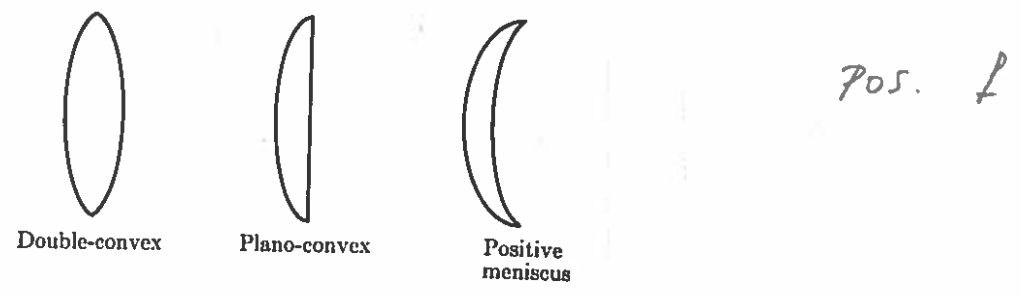
$$t_l(x,y) = e^{i\phi(x,y)}$$

$$= e^{ikn\Delta_0} e^{-ik(n-1) \frac{x^2+y^2}{2} \left(\frac{1}{R_1} - \frac{1}{R_2} \right)}$$

Lens shape defined by R_1, R_2, n :
 combined in focal length f

$$\frac{1}{f} \equiv (n-1) \left(\frac{1}{R_1} - \frac{1}{R_2} \right) :$$

$$t_l(x,y) = e^{ikn\Delta_0} e^{-i \frac{k}{2f} (x^2+y^2)}$$



What is lens actually doing:

Plane wave, normal incidence: $U_L(x,y) = A$:

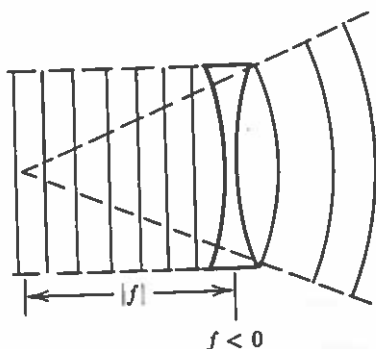
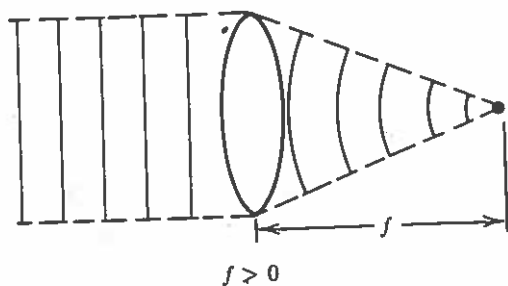
$$U_L'(x,y) = e^{i k n \Delta_0} e^{-i \frac{k}{2f} (x^2 + y^2)} A$$

$\underbrace{\hspace{10em}}_{\text{phase delay}} \quad \quad \quad \underbrace{\hspace{10em}}_{\text{spherical wave}}$

Taylor expanded to 1st ord.
 $(e^{-i k \sqrt{f^2 + x^2 + y^2}} \approx e^{-i k f} e^{-i \frac{k}{2f} (x^2 + y^2)})$
 \uparrow
 $x^2 + y^2 \ll f^2$

f pos : converging

f neg : diverging



Spherical surfaces \rightarrow Spherical waves

\rightarrow focus = δ function

Non paraxial conditions:

Spherical surface \rightarrow Non spherical waves

//

aberration

\rightarrow corrected for aberrations by grinding
surface aspherical