

# Improving Throughput for Oils Analysis by ICP-OES

## **Application Note**

Inductively Coupled Plasma-Optical Emission Spectrometers

## Introduction

Trend analysis of wear metals in lubricating oils is a proven, cost-effective predictive maintenance technique. The presence and levels of various metal elements in lubricating oils gives an indication of the type of wear occurring in an engine. For example, an increase in the level of copper may indicate increased wear of bushings. Non-metals such as silicon, boron and phosphorus elements can also be determined. Monitoring the levels of wear metals and other elements in lubricating oils provides many benefits apart from predicting engine failure. For example, machinery can be kept up and running until maintenance becomes necessary, avoiding premature maintenance. Potential problems can be associated with specific components, eliminating complete teardowns.

The inductively coupled plasma optical emission spectroscopy (ICP-OES) technique for monitoring wear metals is the method of choice for trend analysis because it is fast and accurate. For the busy laboratory, not only is accuracy and long-term stability important; sample throughput is often a vital factor. The most significant contributor to the time taken for an analysis is the sample introduction system; the actual measurement time is most often less than one tenth of the total analysis time. This work shows that the use of a novel pump tubing arrangement can improve the speed of analysis. Using an improved sample introduction system, it was possible to accurately determine key wear metals and other elements in less than 50 seconds per sample using one simple method.



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## **Experimental**

#### Instrumental

A Vista-PRO simultaneous ICP-OES with a radially viewed plasma was used. The radial plasma configuration is the accepted standard for the oils industry. The radial plasma orientation allows direct venting of combustion products, thereby reducing carbon build-up on the torch. The highly efficient 40 MHz free-running RF generator is easily able to cope with solvents to produce a stable, robust plasma with excellent long term stability. The instrument was fitted with a 3 channel peristaltic pump to allow a modified pump tubing configuration for faster sample uptake and washout. A glass concentric nebulizer with wide internal bore size was used to better handle particulates, and a glass double-pass spraychamber was used to prevent overloading the plasma with sample. Optimized instrument operating conditions are set out in Table 1.

Table 1. Instrument Operating Conditions

|                            |                             | Part number        |
|----------------------------|-----------------------------|--------------------|
| Parameter                  | Setting                     | (where applicable) |
| Power                      | 1.35 kW                     |                    |
| Plasma gas flow            | 15.0 L/min                  |                    |
| Auxilliary gas flow        | 2.25 L/min                  |                    |
| Nebulizer pressure or flow | 110 kPa or 0.60 L/min       |                    |
| Viewing height             | 10 mm                       |                    |
| Pump speed                 | 12 rpm                      |                    |
| Sample uptake delay        | 15 s                        |                    |
| Stabilization time         | 5 s                         |                    |
| Rinse time                 | 10 s                        |                    |
| Replicate read time        | 1 s                         |                    |
| Replicates                 | 2                           |                    |
| Nebulizer type             | Slurry glass concentric     | 20-100976-00       |
| Torch type                 | Radial fully demountable    |                    |
|                            | torch kit (includes bracket |                    |
|                            | and clamp)                  | 99-101064-00       |
| Spraychamber               | Twister double pass         | 79-100437-00       |
| Sample tubing to nebulizer | Grey/grey solvent flex      | 37-100352-00       |
| Sample tubing to waste     | Black/black solvent flex    | 37-100348-00       |
| Tubing to waste from       |                             |                    |
| spraychamber               | Solvent flex waste tubing   | 37-100354-00       |
| Transfer tubing            | Solvent flex transfer tubin | g                  |
|                            | ¼"internal diameter         | 37-100378-00       |
| Drain tubing               | Purple/black solvent flex   | 37-100470-00       |
| Autosampler                | AIM 1250*                   |                    |

Manufactured by A.I. Scientific, Scarborough, Old, Australia

#### **Standards and Reagents**

Calibration solutions of 5, 10, 25, 50, 100, and 250 mg/L were prepared from Conostan S-21 certified standard, which contains 21 elements (Ag, Al, B, Ba, Ca, Cd, Cr, Cu, Fe, Mg, Mn, Mo, Na, Ni, P, Pb, Si, Sn, Ti, V, Zn) at 500 mg/kg in oil. These calibration solutions were viscosity matched using Conostan base oil 75. Single element standards of Ca, Fe, Pb, P, and Zn were prepared from certified 5000 mg/kg Conostan standards (Conostan Division, Conoco Specialty Products Inc., Ponca City, OK, USA). The single element standard concentrations prepared were 10, 25, 50, 100, 250, 500, 1000 and 2500 mg/L. Jet-A1 kerosene (Mobil, Melbourne, Australia) was used as diluent.

## **Results**

#### **Detection Limits**

In general, sensitive emission line wavelengths have lower detection limits than less sensitive emission line wavelengths for any given element. This is because sensitive emission lines produce a larger signal for a given concentration than less sensitive emission lines. Thus, low concentrations can be better detected using a sensitive emission line wavelength than an insensitive one. Frequently, detection limits improve with increasing read time because readout noise is reduced. The detection limits of various elements in kerosene are shown in Table 2. All detection limits in the table are below 1 mg/L, which easily allows trace levels of wear metals to be detected and a trend to be observed, even at low levels.

| Table 2. | Detection Limits of Elements in Kerosene at 2, 5 and 10 Seconds |
|----------|-----------------------------------------------------------------|
|          | Integration Time                                                |

| Element and   |               |                                    |        |  |
|---------------|---------------|------------------------------------|--------|--|
| emission line | 3 σ Detection | $3 \sigma$ Detection limits (mg/L) |        |  |
| wavelength    | 1 s           | 2 s                                | 3 s    |  |
| Ag 328.068    | 0.006         | 0.003                              | 0.002  |  |
| AI 308.215    | 0.05          | 0.02                               | 0.02   |  |
| AI 396.152    | 0.05          | 0.02                               | 0.01   |  |
| B 249.772     | 0.021         | 0.007                              | 0.005  |  |
| Ba 455.403    | 0.003         | 0.002                              | 0.001  |  |
| Ba 493.408    | 0.0010        | 0.0007                             | 0.0005 |  |
| Ca 317.933    | 0.02          | 0.01                               | 0.01   |  |
| Ca 396.847    | 0.002         | 0.002                              | 0.002  |  |
| Cd 226.502    | 0.023         | 0.003                              | 0.002  |  |
| Cr 284.325    | 0.012         | 0.005                              | 0.003  |  |
| Cu 327.395    | 0.011         | 0.004                              | 0.003  |  |
| Fe 259.940    | 0.014         | 0.006                              | 0.005  |  |
| Fe 274.932    | 0.06          | 0.02                               | 0.02   |  |
| Mg 280.270    | 0.001         | 0.001                              | 0.001  |  |
| Mn 257.610    | 0.002         | 0.001                              | 0.000  |  |
| Mo 202.032    | 0.072         | 0.009                              | 0.005  |  |
| Na 589.592    | 0.004         | 0.002                              | 0.002  |  |
| Ni 230.299    | 0.08          | 0.02                               | 0.01   |  |
| P 213.618     | 0.26          | 0.03                               | 0.02   |  |
| Pb 220.353    | 0.39          | 0.05                               | 0.03   |  |
| Si 251.608    | 0.05          | 0.02                               | 0.02   |  |
| Sn 283.998    | 0.11          | 0.04                               | 0.02   |  |
| Ti 336.122    | 0.003         | 0.002                              | 0.001  |  |
| V 311.837     | 0.012         | 0.004                              | 0.003  |  |
| Z n 206.200   | 0.063         | 0.007                              | 0.005  |  |
| Zn 213.857    | 0.017         | 0.002                              | 0.002  |  |

#### Linear Range

In general, the maximum accurately measurable concentration of an element is obtained by using a less sensitive emission line wavelength for that element. Although sensitive emission line wavelengths have lower detection limits than insensitive ones, insensitive emission line wavelengths can measure higher maximum concentrations. Some elements, such as calcium and phosphorus, may be present at high concentrations in oils, so a high maximum measurable concentration is desirable. The wavelengths chosen for analysis reflect a compromize between best detection limits and desired concentration range.

| Table 3. | Maximum Measurable Concentration of Selected Elements at |
|----------|----------------------------------------------------------|
|          | Specified Emission Line Wavelengths                      |

| Element and emission | Maximum              |  |
|----------------------|----------------------|--|
| line wavelength      | concentration (mg/L) |  |
| Ag 328.068           | 250+                 |  |
| AI 308.215           | 250+                 |  |
| AI 396.192           | 100                  |  |
| B 249.772            | 250+                 |  |
| Ba 455.403           | 100                  |  |
| Ba 493.408           | 250+                 |  |
| Ca 317.933           | 2500                 |  |
| Ca 396.847           | 100                  |  |
| Cd 226.502           | 250+                 |  |
| Cr 284.325           | 250+                 |  |
| Cu 327.395           | 250+                 |  |
| Fe 259.940           | 250+                 |  |
| Fe 274.932           | 1000                 |  |
| Mg 280.270           | 100                  |  |
| Mn 257.610           | 250+                 |  |
| Mo 202.032           | 250+                 |  |
| Na 589.592           | 250+                 |  |
| Ni 230.299           | 250+                 |  |
| P 213.618            | 2500                 |  |
| Pb 220.353           | 1500                 |  |
| Si 251.608           | 250+                 |  |
| Sn 283.998           | 250+                 |  |
| Ti 336.122           | 250+                 |  |
| V 311.837            | 250+                 |  |
| Zn 206.200           | 2500                 |  |
| Zn 213.857           | 250                  |  |

 Note that 250+ designates an accurately measurable concentration that may surpass 250 mg/L.

## **Modified Pump Tubing Setup**

To speed up sample delivery to the plasma, the flow rate of sample through the autosampler probe was increased based on the "rapid flow" concept conceived by Shane Elliott and investigated as applied to organic solutions by Ross Ashdown (both from Agilent). The idea is to increase the flow rate of sample from the autosampler to the peristaltic pump. To increase the sample flow rate, a wider internal diameter peristaltic pump tubing could have been used, but this would overload the nebulizer, adversely affecting nebulization. Instead, an additional sample peristaltic pump tube was introduced to the system via a T-piece inserted between the end of the autosampler line and the start of the sample peristaltic pump tubing so that sample would flow through two sample perstaltic pump tubings instead of one. One of the peristaltic pump tubes was directed to the nebulizer, and the other to waste, which avoided overloading the nebulizer with sample. By having sample flow through two pump tubings, the sample flow rate through the autosampler probe up to the point where the T-piece was inserted was increased, thus reducing sample uptake time.

To measure sample uptake time, kerosene was introduced to the autosampler probe manually after aspirating air, and the time taken for the plasma to turn bright green (which indicates that organic solution is being aspirated into the plasma) was measured by stopwatch. Table 4 shows that using the modified pump tubing setup, the sample uptake time was decreased by approximately 10 seconds. An added benefit of decreasing sample uptake time is that the time taken to achieve a fixed degree of washout is also reduced.

Table 4. Time Saved Using Modified Pump Tubing Setup

| Pump tubing configuration | Acutal sample<br>uptake time (s) | Sample uptake time<br>in method (s) |
|---------------------------|----------------------------------|-------------------------------------|
| Standard                  | 24                               | 25                                  |
| Modified                  | 15                               | 15                                  |

## Washout

To determine the washout achieved in an autosampler run, an analysis was performed where a blank kerosene solution was measured immediately following a solution containing 1000 mg/L of Fe. These two solutions were then measured in pairs six times each. Table 5 shows that three orders of reduction in sample concentration was achieved in an autosampler run with a rinse time of 10 seconds. If a more thorough rinse was required, then SmartRinse could have been used. The SmartRinse feature of the ICP Expert software optimizes the rinse time for each sample, ensuring that the rinse time is only as long as required to return the signal to that of a blank for each wavelength in the analysis [1]. This means that high concentration samples. For this work, a washout of three orders was acceptable, so a short, fixed rinse time was used. 
 Table 5.
 Blank Results After Measuring 1000 mg/L Iron. This

 Demonstrates that Three Orders of Washout is Achieved with a Rinse Time of 10 Seconds.

| Kerosene blank<br>measurement number | Measured Fe conc.<br>(mg/L) |  |
|--------------------------------------|-----------------------------|--|
| 2                                    | 0.66                        |  |
| 4                                    | 0.77                        |  |
| 6                                    | 0.79                        |  |
| 8                                    | 0.79                        |  |
| 10                                   | 0.80                        |  |
| 12                                   | 0.64                        |  |



Figure 1. Stability of the Vista-PRO radial instrument over 8 hours. Results remained within ±10% for all elements in the 5 mg/L S21 kerosene solution without internal standardization or recalibration.

## **Long-Term Stability**

A 5 mg/L solution of S21 elements in Jet-A1 kerosene was analysed continuously over an eight hour period. No recalibrations were performed, and no internal standard was used. Figure 1 shows that results remained within 10% of the true value over the entire 8 hours. Precision was typically better than 2 %RSD.

## Conclusion

The Vista-PRO radial ICP-OES provides excellent throughput at 47 seconds per sample using a simple optimized sample introduction system. The detection limits and maximum measurable concentration of selected wavelengths allows typical oil samples to be analysed, while the excellent stability allows continuous running without recalibration, providing a saving on costs by reducing analysis time and the amount of standard solution used.

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#### Reference

1. I. Szikla, SmartRinse - the latest advance in maximizing

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