

Date Prepared: May 28, 2021  
Ref. No.: P21AT008

Initial Design	1
PCC Revision	

# STRUCTURAL CALCULATIONS

for

## **SAINT VINCENT DE PAUL HS (NOKIA MBO) (P21AT008)**

849 KEOKUK ST.  
PETALUMA, CA 94952

**Prepared for:**

**AT&T MOBILITY**

2255 6<sup>TH</sup> STREET  
OROVILLE, CA 95965



**Prepared by:**



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# SAINT VINCENT DE PAUL HS (NOKIA MBO)

849 Keokuk St, Petaluma, CA 94952, USA

Latitude, Longitude: 38.2435610000001, -122.6507041



<b>Date</b>	5/18/2021, 3:04:57 PM
<b>Design Code Reference Document</b>	ASCE7-16
<b>Risk Category</b>	III
<b>Site Class</b>	D - Default (See Section 11.4.3)

Type	Value	Description
S <sub>S</sub>	1.5	MCE <sub>R</sub> ground motion. (for 0.2 second period)
S <sub>1</sub>	0.6	MCE <sub>R</sub> ground motion. (for 1.0s period)
S <sub>MS</sub>	1.8	Site-modified spectral acceleration value
S <sub>M1</sub>	null -See Section 11.4.8	Site-modified spectral acceleration value
S <sub>DS</sub>	1.2	Numeric seismic design value at 0.2 second SA
S <sub>D1</sub>	null -See Section 11.4.8	Numeric seismic design value at 1.0 second SA

Type	Value	Description
SDC	null -See Section 11.4.8	Seismic design category
F <sub>a</sub>	1.2	Site amplification factor at 0.2 second
F <sub>v</sub>	null -See Section 11.4.8	Site amplification factor at 1.0 second
PGA	0.596	MCE <sub>G</sub> peak ground acceleration
F <sub>PGA</sub>	1.2	Site amplification factor at PGA
PGA <sub>M</sub>	0.715	Site modified peak ground acceleration
T <sub>L</sub>	12	Long-period transition period in seconds
SsRT	1.742	Probabilistic risk-targeted ground motion. (0.2 second)
SsUH	1.898	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration
SsD	1.5	Factored deterministic acceleration value. (0.2 second)
S1RT	0.671	Probabilistic risk-targeted ground motion. (1.0 second)
S1UH	0.739	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration.
S1D	0.6	Factored deterministic acceleration value. (1.0 second)
PGAd	0.596	Factored deterministic acceleration value. (Peak Ground Acceleration)
C <sub>RS</sub>	0.918	Mapped value of the risk coefficient at short periods



**LATERAL ANALYSIS**

**1) Seismic Load**

Code Compliance **California Building Code 2019** Editor **ASCE7-16**

Soil Site Class =	<b>D</b>	
Response Spectral Acc. (0.2 sec.), $S_s$ =	<b>1.500</b>	<a href="#">Figure 22-1 through 22-8</a>
Response Spectral Acc. (1.0 sec.), $S_1$ =	<b>0.6</b>	<a href="#">Figure 22-1 through 22-8</a>
Site Coefficient, $F_a$ =	<b>1.2</b>	<a href="#">Table 11.4-1</a>
Site Coefficient, $F_v$ =	<b>1.7</b>	<a href="#">Table 11.4-2</a>
Max. Considered Earthquake Acc, $S_{MS} = F_a * S_s$ =	<b>1.8</b>	<a href="#">Eq. 11.4-1</a>
Max. Considered Earthquake Acc, $S_{M1} = F_v * S_1$ =	<b>1.02</b>	<a href="#">Eq. 11.4-2</a>
$S_{DS} = 2/3 * (S_{MS})$ =	<b>1.200</b>	<a href="#">Eq. 11.4-3</a>
$S_{D1} = 2/3 * (S_{M1})$ =	<b>0.680</b>	<a href="#">Eq. 11.4-4</a>
Component Amplification Factor, $a_p$ =	<b>1.0</b>	<a href="#">Table 13.5-1 through 13.6-1</a>
Component Importance Factor, $I_p$ =	<b>1.25</b>	<a href="#">13.1.3, Page 121</a>
Component Operating Weight, $W_p$ (lbs) =	<b>100</b>	Max. per Antenna, MBO unit & Mounting Weight
Component Response Modification Factor, $R_p$ =	<b>2.5</b>	<a href="#">Table 13.5-1 through 13.6-1</a>
Height in structure of point of attachment component with respect to the base, $z$ (ft) =	<b>1</b>	
Average roof height of structure with respect to the base, $h$ (ft) =	<b>1</b>	

**Seismic Design Force,  $F_p$**

$$F_p = \frac{0.4a_p S_{DS} W_p (1 + 2\frac{z}{h})}{\left(\frac{R_p}{I_p}\right)} = \mathbf{72.00} \text{ lbs} \quad \text{Eq. 13.3-1}$$

$$F_{p(max)} = 1.6 S_{DS} I_p W_p = \mathbf{240.00} \text{ lbs} \quad \text{Eq. 13.3-2}$$

$$F_{p(min)} = 0.3 S_{DS} I_p W_p = \mathbf{45.00} \text{ lbs} \quad \text{Eq. 13.3-3}$$

**2) Wind Load**

Design Wind Speed,  $V = 100$  mph (ASCE 7-16 Figure 26.5-1A, page 254)  
Exposure : **C**

Design Wind Pressure:

$$q_z = 0.00256 K_z K_{zt} K_d K_e V^2 = \mathbf{19.6} \text{ psf} \quad (\text{ASCE7-16 Eq. 26.10-1, Page 268})$$

Velocity Pressure Exposure Coefficients,  $K_z = 0.90$  (ASCE7-16 Table 26.10-1, Page 268)  
Topographic Factor,  $K_{zt} = 1.00$  (ASCE7-16 Section 26.8.2, Page 268)  
Wind Directionality Factor,  $K_d = 0.85$  (ASCE7-16 Table 26.6-1, Page 266)  
Ground Elevation Factor,  $K_e = 1.00$  (ASCE7-16 Table 26.9-1, Page 268)

$$F = q_z G C_f A_s = \mathbf{92} \text{ lbs} \quad (\text{ASCE7-16 Eq. 29.3-1, Page 322})$$

Gust Effect Factor,  $G = 0.85$  (ASCE7-16 Section 26.11.1, Page 269)  
Force Coefficient,  $C_f = 1.20$  (ASCE7-16 Figure 29.3-1, Page 323)  
Gross Area,  $A_s = 5 \text{ ft}^2 = \mathbf{1.00} \text{ ft} \times \mathbf{5} \text{ ft}$  Max. per post

**3) Design Lateral Load**

Seismic Design Force,  $F_p = 72.00$  lbs = **0.7**  $W_p$   
Design Wind Force,  $F_w = 91.89$  lbs = **19.98** psf <--Design Wind Load

Since,  $F_p < F_w$  **Wind Govern Design**



**LAG SCREW FOR ANTENNA MOUNTING ANALYSIS** Ref. detail: 1/A5

**Design Of Antenna Mounting:**

**Antenna and Mounting Weight:** = 100 lbs Max.

**Lateral Anlysis:**

1 **Seismic load:**  $F_p = 72.0$  lbs

2 **Wind load:**  $F_w = 91.9$  lbs

**Wind Govern Design**

$$V = W_p = 100 \text{ lbs} \quad H = 1.08 \text{ ft. Min.}$$

$$T \times H = F_w \times L$$

$$1.1 \times T = 92 \times 5.66$$

$$T = 481.6 \text{ lbs}$$

**Total Applied Shear Load:**  $V = 100.0$  lbs

**Total Applied Tension Load**  $T = 481.6$  lbs

**Total Number Of Bolt Resisting Shear**  $N_s = 4$

**Total Number Of Bolt Resisting Tension**  $N_T = 2$

**Applied Tension Load:**  $P_s = T / N_T = 240.8$  lbs

**Applied Shear Load:**  $V_s = V / N_s = 25$  lbs

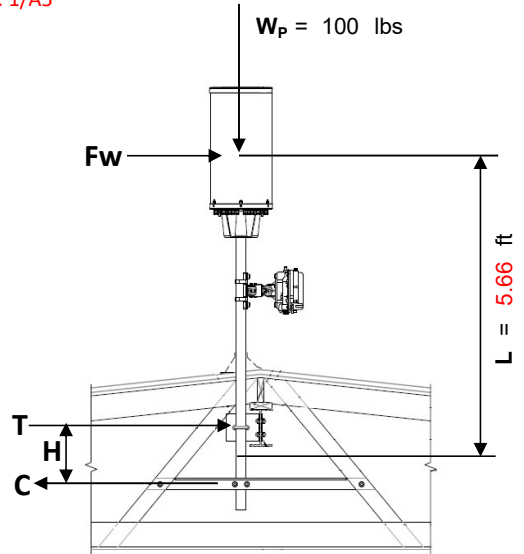
Check 5/8"Ø Bolts Capacity

**Allowable Tension :**  $Ta' = 6900$  lbs (AISC Steel Construction Manual 15th ed. Table 7-1,7-2)

**Allowable Shear :**  $Va' = 4140$  lbs (AISC Steel Construction Manual 15th ed. Table 7-1,7-2)

**Interaction Check :**  $P_s / Ta' + V_s / Va' = 0.04 < 1.0$  [O.K.]

**Use 5/8 in. Diameter Bolt**





Project Title:  
 Engineer:  
 Project ID:  
 Project Descr:

## Steel Beam

Lic. #: KW-06001779

File: WF beam check.ec6  
 Software copyright ENERCALC, INC. 1983-2020, Build:12.20.8.24  
 DELTA GROUPS ENGINEERING

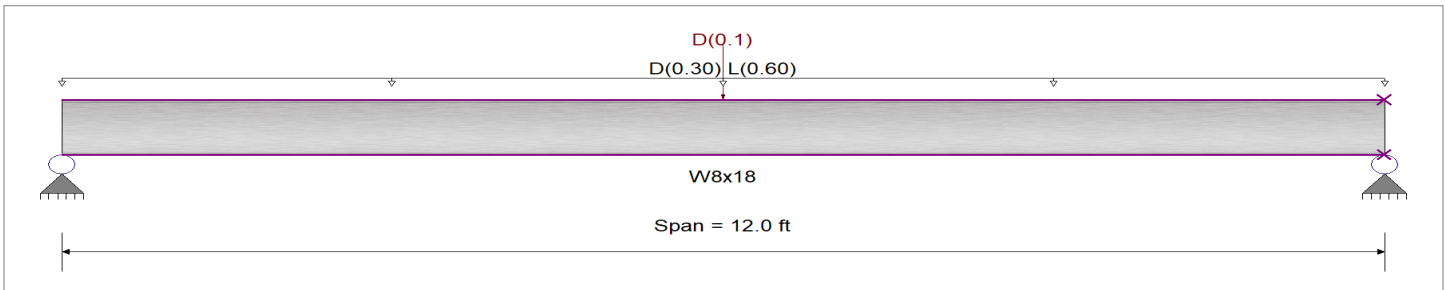
DESCRIPTION: (E) WF beam

### CODE REFERENCES

Calculations per AISC 360-16, IBC 2018, CBC 2019, ASCE 7-16  
 Load Combination Set : ASCE 7-16

### Material Properties

Analysis Method : **Allowable Strength Design**  
 Beam Bracing : **Beam is Fully Braced against lateral-torsional buckling**  
 Bending Axis : **Major Axis Bending**  
 Fy : Steel Yield : **36.0 ksi**  
 E: Modulus : **29,000.0 ksi**



### Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added  
 Loads on all spans...  
 Uniform Load on ALL spans : D = 0.020, L = 0.040 ksf, Tributary Width = 15.0 ft

Load(s) for Span Number 1  
 Point Load : D = 0.10 k @ 6.0 ft

### DESIGN SUMMARY

**Design OK**

Maximum Bending Stress Ratio =	<b>0.540</b> : 1	Maximum Shear Stress Ratio =	<b>0.202</b> : 1
Section used for this span	<b>W8x18</b>	Section used for this span	<b>W8x18</b>
Ma : Applied	<b>16.500 k-ft</b>	Va : Applied	<b>5.450 k</b>
Mn / Omega : Allowable	<b>30.539 k-ft</b>	Vn/Omega : Allowable	<b>26.960 k</b>
Load Combination	<b>+D+L</b>	Load Combination	<b>+D+L</b>
Location of maximum on span	<b>6.000ft</b>	Location of maximum on span	<b>0.000 ft</b>
Span # where maximum occurs	<b>Span # 1</b>	Span # where maximum occurs	<b>Span # 1</b>
Maximum Deflection			
Max Downward Transient Deflection	<b>0.157 in</b>	Ratio =	<b>919</b> >=360
Max Upward Transient Deflection	<b>0.000 in</b>	Ratio =	<b>0</b> <360
Max Downward Total Deflection	<b>0.238 in</b>	Ratio =	<b>604</b> >=180
Max Upward Total Deflection	<b>0.000 in</b>	Ratio =	<b>0</b> <180

### Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values						Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega	
D Only															
Dsgn. L = 12.00 ft		1	0.187	0.069	5.70		5.70	51.00	30.54	1.00	1.00	1.85	40.44	26.96	
+D+L															
Dsgn. L = 12.00 ft		1	0.540	0.202	16.50		16.50	51.00	30.54	1.00	1.00	5.45	40.44	26.96	
+D+0.750L															
Dsgn. L = 12.00 ft		1	0.452	0.169	13.80		13.80	51.00	30.54	1.00	1.00	4.55	40.44	26.96	
+0.60D															
Dsgn. L = 12.00 ft		1	0.112	0.041	3.42		3.42	51.00	30.54	1.00	1.00	1.11	40.44	26.96	

### Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.2385	6.034		0.0000	0.000

### Vertical Reactions

Load Combination	Support notation : Far left is #1		Values in KIPS	
	Support 1	Support 2		
Overall MAXimum	5.450	5.450		
Overall MINimum	1.110	1.110		
D Only	1.850	1.850		

Project Title:  
Engineer:  
Project ID:  
Project Descr:

## Steel Beam

Lic. # : KW-06001779

File: WF beam check.ec6  
Software copyright ENERCALC, INC. 1983-2020, Build:12.20.8.24  
DELTA GROUPS ENGINEERING

DESCRIPTION: (E) WF beam

### Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
+D+L	5.450	5.450
+D+0.750L	4.550	4.550
+0.60D	1.110	1.110
L Only	3.600	3.600

Project Title:  
 Engineer:  
 Project ID:  
 Project Descr:

## Steel Beam

File: WF beam check.ec6  
 Software copyright ENERCALC, INC. 1983-2020, Build:12.20.8.24  
 DELTA GROUPS ENGINEERING

Lic. #: KW-06001779

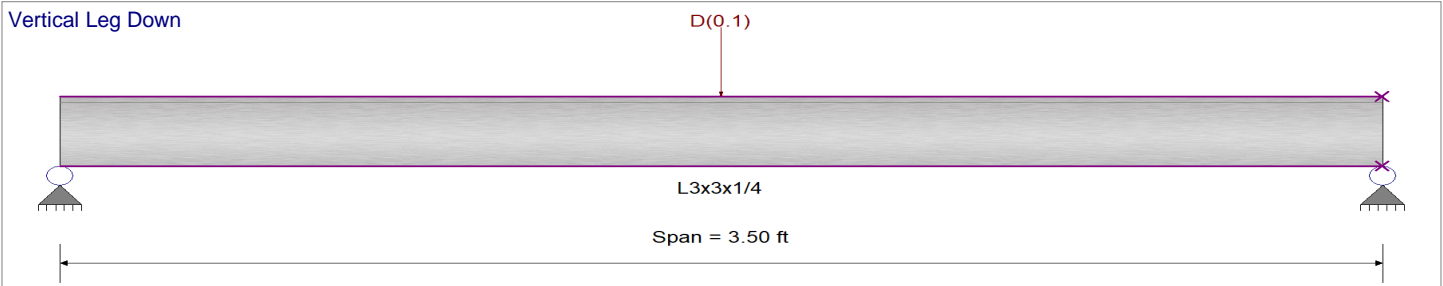
DESCRIPTION: (N) 3X3X1/4

### CODE REFERENCES

Calculations per AISC 360-16, IBC 2018, CBC 2019, ASCE 7-16  
 Load Combination Set : ASCE 7-16

### Material Properties

Analysis Method : Allowable Strength Design  
 Beam Bracing : Beam is Fully Braced against lateral-torsional buckling  
 Bending Axis : Major Axis Bending  
 Fy : Steel Yield : 50.0 ksi  
 E : Modulus : 29,000.0 ksi



### Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added  
 Load(s) for Span Number 1  
 Point Load : D = 0.10 k @ 1.750 ft

### DESIGN SUMMARY

**Design OK**

Maximum Bending Stress Ratio =	<b>0.041</b> : 1	Maximum Shear Stress Ratio =	<b>0.004</b> : 1
Section used for this span	<b>L3x3x1/4</b>	Section used for this span	<b>L3x3x1/4</b>
Ma : Applied	0.088 k-ft	Va : Applied	0.050 k
Mn / Omega : Allowable	2.127 k-ft	Vn/Omega : Allowable	13.473 k
Load Combination	D Only	Load Combination	D Only
Location of maximum on span	1.750ft	Location of maximum on span	1.760 ft
Span # where maximum occurs	Span # 1	Span # where maximum occurs	Span # 1
<b>Maximum Deflection</b>			
Max Downward Transient Deflection	0.000 in	Ratio =	0 < 360
Max Upward Transient Deflection	0.000 in	Ratio =	0 < 360
Max Downward Total Deflection	0.004 in	Ratio =	9665 >= 180
Max Upward Total Deflection	0.000 in	Ratio =	0 < 180

### Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values						Summary of Shear Values			
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
D Only	Dsgn. L = 3.50 ft	1	0.041	0.004	0.09		0.09	3.55	2.13	1.00	1.00	0.05	22.50	13.47
+0.60D	Dsgn. L = 3.50 ft	1	0.025	0.002	0.05		0.05	3.55	2.13	1.00	1.00	0.03	22.50	13.47

### Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
D Only	1	0.0043	1.750		0.0000	0.000

### Vertical Reactions

Load Combination	Support 1	Support 2
Overall MAXimum	0.050	0.050
Overall MINimum	0.030	0.030
D Only	0.050	0.050
+0.60D	0.030	0.030