

Draft Report

Transportation Impact Study for the Dominican Valley Subdivision Project

Prepared for the City of San Rafael

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490 Mendocino Avenue, Suite 201 SANTA ROSA, CA 95401 707.542.9500 414 13th Street, 5th Floor OAKLAND, CA 94612 510.444.2600 w-trans.com



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Executive Summary

The project as proposed would construct 50 residential units in the Dominican/Black Canyon neighborhood in the City of San Rafael on a 20.79-acre site. The proposed units include 27 single family homes, 17 townhomes, and six duplex units, as well as 14 junior accessory dwelling units (JADUs). The proposed units would be located along the periphery of the site; five units would be accessed from Gold Hill Grade, while 35 units would be accessed from two driveways on Deer Park Ave and 10 units would be accessed via a driveway from Margarita/Highland.

The project is expected to generate an average of 421 new daily trips, including 30 a.m. peak hour trips and 38 p.m. peak hour trips.

Under Existing conditions, all three study intersections operate at an acceptable Level of Service (LOS) of C or better during both the a.m. and p.m. peak hours and would continue to do so upon the addition of project-generated traffic. Under Future conditions, all intersections are expected to operate acceptably without and with the project during both peak hours.

With respect to multimodal circulation, the site is located one-half mile from the nearest transit stops served by Marin Transit. The project is located in the hillside residential area, where sidewalks are not required. The Dominican University campus is located on the west side of Deer Park Avenue across from the site; sidewalks are present within the campus and along streets connecting the campus to central San Rafael. Bicycles are required to share the road with vehicle traffic along most streets in the vicinity of the project. Grand Avenue is designated as a Class III bike route, as is 4th Street, while sections of Point San Pedro Road are designated as Class II and Class III bicycle facilities.

The project would potentially have a significant impact with respect to vehicle miles traveled (VMT). Various measures are recommended to reduce the VMT associated with the project; however, it may not be feasible to fully mitigate these impacts.

The project frontage streets are currently substandard and would all be widened to 26 feet as required by the San Rafael Fire Department. The project would therefore meet emergency vehicle access requirements and would improve emergency vehicle access to properties in the surrounding neighborhoods.

Sight distances at the project access points were evaluated based on the proposed widenings of the frontage streets and the locations of the project driveways. Based on the slow vehicle speeds and low traffic volumes along these streets, the sight distances were determined to be adequate.

The proposed project would provide 169 parking spaces, which is more than the 100 spaces required under the San Rafael Municipal Code.



Introduction

This report presents an analysis of the potential traffic impacts and adverse operational effects that would be associated with development of a proposed 50-unit residential development in the Dominican/Black Valley neighborhood of San Rafael. The traffic study was completed in accordance with the criteria established by the City of San Rafael and is consistent with standard traffic engineering techniques.

Prelude

The purpose of a traffic impact study is to provide City staff and policy makers with data that they can use to make an informed decision regarding the potential transportation impacts of a proposed project, and any associated improvements that would be required to mitigate these impacts to an acceptable level under CEQA, the City's General Plan, or other policies. This report provides an analysis of those items that are identified as areas of environmental concern under the California Environmental Quality Act (CEQA) and that, if significant, require an EIR. Impacts associated with access for pedestrians, bicyclists, and to transit; the vehicle miles traveled (VMT) generated by the project; potential safety concerns such as increased queuing in dedicated turn lanes, adequacy of sight distance, need for turn lanes, and need for additional right-of-way controls; and emergency access are addressed in the context of the CEQA criteria. While no longer a part of the CEQA review process, vehicular traffic service levels at key intersections were evaluated for consistency with General Plan policies by determining the number of new trips that the proposed use would be expected to generate, distributing these trips to the surrounding street system based on anticipated travel patterns specific to the proposed project, then analyzing the effect the new traffic would be expected to have on the study intersections and need for improvements to maintain acceptable operation. The adequacy of parking is also addressed as a policy issue.

Applied Standards and Criteria

The report is organized to provide background data that supports the various aspects of the analysis, followed by the assessment of CEQA issues and then evaluation of policy-related issues. The CEQA criteria evaluated are as follows.

Would the project:

- a. Conflict with a program, plan, ordinance, or policy addressing the circulation system, including transit, roadway, bicycle, and pedestrian facilities?
- b. Conflict or be inconsistent with CEQA Guidelines § 15064.3, subdivision (b)?
- c. Substantially increase hazards due to a geometric design feature (e.g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment)?
- d. Result in inadequate emergency access?

The project was also evaluated against the City of San Rafael's policies, which provide guidance relative to traffic impacts for CEQA issues as well as the effects caused by traffic associated with new development. The *Transportation Impact Analysis Guidelines*, City of San Rafael, March 2021, detail mobility deficiency criteria for development projects. For intersection traffic control, the Guidelines refer to the Level of Service (LOS) standard published in the *San Rafael General Plan 2040*, City of San Rafael, August 2021. General Plan Policy M-2.5 outlines a general citywide standard of LOS D operation, with exemptions for intersections in the Downtown Precise Plan boundary and signalized freeway ramp intersections.

The Guidelines state that an adverse effect would occur If the addition of project traffic would cause a deficient level of delay at an intersection, or if the delay at an intersection operating deficiently without project traffic would increase by five seconds or more with the addition of project traffic.



Project Profile

The project as proposed is comprised of 50 residential units, including 27 single-family homes, 17 townhomes, and six duplex units. In addition, it includes 14 attached junior accessory dwelling units (JADUs). The property is a 20.79-acre site in the Dominican/Black Canyon neighborhood of San Rafael and is bounded by Deer Park Avenue, Gold Hill Grade, and Margarita Avenue. The proposed units would be clustered near the street frontages. The location of the project site is shown in Figure 1.





Transportation Impact Study for the Dominican Valley Subdivision Project Figure 1 – Study Area and Existing Lane Configurations



Transportation Setting

Study Area and Periods

The study area varies depending on the topic. For pedestrian trips it consists of all streets within a half-mile of the project site that would lie along primary routes of pedestrian travel, or those leading to nearby attractors. For bicycle trips it consists of all streets within one mile of the project site that would lie along primary routes of bicycle travel. For the safety and operational analyses, it consists of the project frontage and the following intersections:

- 1. Grand Avenue/Mission Avenue
- 2. Grand Avenue/ Jewell Street
- 3. Grand Avenue/Locust Avenue

Operating conditions during the a.m. and p.m. peak periods were evaluated to capture the highest potential impacts for the proposed project as well as the highest volumes on the local transportation network. The morning peak hour occurs between 7:00 and 9:00 a.m. and reflects conditions during the home to work or school commute, while the p.m. peak hour occurs between 4:00 and 6:00 p.m. and typically reflects the highest level of congestion during the homeward bound commute. Counts were obtained for the study intersections on February 15, 2024, and February 22, 2024.

Study Intersections

Grand Avenue/Mission Avenue is a four-way stop-controlled intersection with one travel lane in each direction at all approaches. On-street parking is permitted along both sides of Grand Avenue as well as along both sides of Mission Avenue. Crosswalks are provided on each leg, and all approaches have speed limits of 25 miles per hour (mph). Class III shared bike routes are signed along the north and south legs of Grand Avenue.

Grand Avenue/Jewell Street is a four-way stop-controlled intersection with a speed limit of 25 mph on all approaches. Parking is permitted along both sides of the south, east and west legs of the intersection. Parking is prohibited at bus stops on both sides of the north leg of the intersection. Yellow school crosswalks are provided on each leg and each approach consists of one lane per direction. Class III bike routes are designated along the north and south legs.

Grand Avenue/Locust Avenue is a three-way intersection with stop controls on the eastern Locust Avenue approach. A driveway is also present near the southeast corner of the intersection. Each approach has a 25-mph speed limit, and yellow school-zone crosswalks are provided on the south and east legs of the intersection. Grand Avenue is designated as a Class III bike route.

The locations of the study intersections and the existing lane configurations and controls are shown in Figure 1.

Study Roadways

Deer Park Avenue is generally a north-south roadway approximately 14 feet wide, serving traffic in both directions. It is classified as a local street with a *prima facie* speed limit of 25 mph.

Gold Hill Grade is a two-way east-west roadway approximately 18 feet wide. It is classified as a local street with a *prima facie* speed limit of 25 mph.

Margarita Drive is two-way east-west roadway approximately 16 feet wide. It is classified as a local street with a *prima facie* speed limit of 25 mph.



Collision History

The collision history for the study area was reviewed to determine any trends or patterns that may indicate a safety issue. Collision rates were calculated based on records available from the California Highway Patrol as published in their Statewide Integrated Traffic Records System (SWITRS) reports. The most current five-year period available is October 1, 2018, through September 30, 2023.

As presented in Table 1, the calculated collision rates for the study intersections were compared to average collision rates for similar facilities statewide, as indicated in *2021 Collision Data on California State Highways*, California Department of Transportation (Caltrans). These average rates statewide are for intersections in the same environment (urban), with the same number of approaches (three or four), and the same controls (all-way stop or two-way stop). The calculated collision rate for Grand Avenue/Mission Avenue is higher than the statewide average. Of the eight collisions recorded at this intersection during the analysis period, three were sideswipes, two were broadsides, two involved pedestrians, and one was a rear-end collision. While the injury rate was lower than the statewide average, the two injury collisions were both due to pedestrian right-of-way violations. The intersection has all-way stop controls, but vegetation is present in the vicinity of the crossings, so visibility of pedestrians may have been a factor at the time the collisions occurred. Otherwise, the collision history does not suggest any underlying safety concerns at this location. The collision rate calculations are provided in Appendix A.

Tal	Table 1 – Collision Rates for the Study Intersections									
Study Intersection		Number of Collisions (2018-2023)	Calculated Collision Rate (c/mve)	Statewide Average Collision Rate (c/mve)						
1.	Grand Ave/Mission Ave	8	0.40	0.21						
2.	Grand Ave/Jewell St	1	0.10	0.21						
3.	Grand Ave/Locust Ave	1	0.13	0.13						

Note: c/mve = collisions per million vehicles entering; **Bold** text = collision rate exceeds statewide average

One collision was recorded along each of the study segments during the analysis period. It is noted that Gold Hill Grade and Margarita Drive provide access to a small number of residences, and speeds are low due to the narrow street width and limited sight lines. The one collision recorded on Margarita Drive resulted from a head-on collision but resulted in no injuries. Deer Park Avenue provides access to Dominican University; however, few vehicles enter or exit the campus at this location. Based on the low volumes and physical conditions along these segments, there do not appear to be any underlying safety concerns.



Project Data

The project consists of 50 residential units, including 27 single-family homes, 17 townhomes and six duplex units, as well as 14 junior accessory dwelling units. The project units are proposed to be clustered around the periphery of the site, along Gold Hill Grade, Deer Park Avenue, and Margarita Drive. The Gold Hill Grade homes would have driveway access directly onto the street, while internal project roadways would be constructed at the other two locations. The segments of Gold Hill Grade, Deer Park Avenue, and Margarita Drive along the project frontages would be widened to 26 feet, and the internal access roads would also be 26 feet wide. The proposed project site plan is shown in Figure 2.

Trip Generation

The anticipated trip generation for the proposed project was estimated using standard rates published by the Institute of Transportation Engineers (ITE) in *Trip Generation Manual*, 11th Edition, 2021, for Single Family Detached Housing (LU #210) and Single Family Attached Housing (LU #215) as these descriptions most closely match the proposed project. Since accessory dwelling units can be built by right, they were not included in the trip generation estimate. Based on application of these rates, the proposed project is expected to generate an average of 421 trips per day, including 30 a.m. peak hour trips and 38 trips during the p.m. peak hour. These results are summarized in Table 2.

Table 2 – Trip Generation Summary											
Land Use	Units	Daily		AM Peak Hour		F	PM Peak	Hour			
		Rate	Trips	Rate	Trips	In	Out	Rate	Trips	In	Out
SF Detached Housing	27 du	9.43	255	0.70	19	5	14	0.94	25	16	9
SF Attached Housing	23 du	7.20	166	0.48	11	3	8	0.57	13	8	5
Total			421		30	8	22		38	24	14

Note: SF = Single Family; du = dwelling unit

Trip Distribution

The pattern used to allocate new project trips to the street network was determined in consideration of journey to work data included in the 2010 census, familiarity with the study area including nearby attractors, and review of existing traffic patterns in the vicinity. The assumptions applied are shown in Table 3.

Table 3 – Trip Distribution Assumptions							
Route	Percent						
To/From the South via Grand Ave	70%						
To/From the North via Grand Ave	30%						
TOTAL	100%						



ARCHITECTS

FAR CALCULATIONS									
LOT #	LOT AREA (SF)	UNIT TYPE	BUILDING AREA (NSF)	MAX BUILDING AREA (2,500 SF + 10% Lot Area)	FLOO AREA RATIO				
1	7,500	E	2,595	3,300	0.35				
2	7,993	E	2,595	3,349	0.32				
3	7,930	E	2,595	3,343	0.33				
4	7,500	E	2,595	3,300	0.35				
5	7,500	E	2,595	3,300	0.35				
6	7,606	F	3,165	3,311	0.42				
7	7.658	F	3.165	3,316	0.41				
8	8,410	F	3,165	3,391	0.35				
9	22.735	F	3.165	4.824	0.14				
10	14,855	В	2,825	4,036	0.19				
11	14.855	В	2.825	4.036	0.19				
12	11.085	В	2.825	3,659	0.25				
13	10.967	B	2.825	3.647	0.26				
14	8.937	В	2.825	3.444	0.32				
15	2.276	D2 (+ ADU)	1380	2,778	0.61				
16	1.207	D2 (+ ADU)	1.380	2.671	114				
17	1207	D2 (+ ADLI)	1380	2.671	114				
18	1.207	D2 (+ ADU)	1.380	2.671	1.14				
19	1207	D2 (+ ADL)	1380	2.671	114				
20	1207	D2 (+ ADLB	1290	2.671	154				
21	1207	D2 (+ ADU)	1380	2.671	114				
22	1207	D2 (+ ADU)	1,300	2,671	114				
22	1207	D2 (+ ADU)	1,300	2,671	114				
24	1207	D2 (+ ADU)	1,300	2,671	114				
24	1,207	D2 (+ ADU)	1,300	2,071	114				
20	1,207	D2 (+ ADU)	1,380	2,671	154				
22	1,207	D2 (FADU)	1,300	2,071	114				
20	1,207	D2 (+ ADU)	1,300	2,671	114				
20	1,207	D2 (F ADU)	1150	2,670	0.00				
20	1,204	DI	1,150	2,670	1.02				
30	1022	DI	1,150	2,002	114				
31	1,000	6	1,150	2,031	0.00				
32	11,210	F	3,165	3,671	0.28				
33	7,5/1	F	3,165	3,307	0.4				
34	7,500	F	3,105	3,300	0.42				
33	7,500	F	3,165	3,300	0.42				
.20	7.500	F	3.165	3,300	0.42				
37	7,500	F	3,165	3,300	0.4,				
38	7,650	F	3.165	3.315	0.4				
39	9,300	F	3,105	3,48U	0.34				
40	7,502	F	3,165	3,300	0.42				
41	7.133	C	3.030	3,203	0.42				
42	/,/59	C	3,030	3,326	0.35				
43	7,893	C	3,030	3,339	0.38				
44	7,/3/	C	3.030	3,324	0.39				
45	3,509	A	1,805	2,901	0.5				
46	4,818	A	1.805	3.032	0.37				
47	3,344	A	1,805	2,884	0.54				
48	3,443	A	1.805	2,894	0.5;				
49	4.407	A	1.805	2,991	0.4				
50	7,030	A	1,805	3,253					

SQUARE FOOTAGE DEFINITION

NSF: Sum of all enclosed areas, measured to the interior of enclosing walls, excluding non conditioned areas. Stairs counte at one floor only.

GSF: Thiskide areas gross building square footager means the un of all enclosed or covered areas of each floor or all structures on the site, measured to the exterior of the enclosing walls, columns or posts including basement areas, uninitable datic or loft papecs and other areas capable of being finished that habitable bages and extermined by the California Building Code; garages and the structure of the structure of the structure of posts; other roots covered areas supported by walls; columns or posts; and capable of being enclosed, measured to the exterior posts; other roots covered areas supported by walls; columns or posts; other roots covered areas supported by walls; columns or posts; other roots covered areas supported by walls; columns or posts; other roots careas. Excluded are areas permanenty open to the sity, between areas under root eaves; helliss or contreleveed the sity categories areas. In the structure areas areas permanenty open to the sity, between areas under root eaves; helliss or contreleveed cable of being included to the patient areas areas of contactive and accessions of the structure areas areas permanenty open to the sity, between areas under root eaves; helliss or contactive and accessions of the root eaves; helliss or contactive and accessions of the site of the structure areas areas areas areas and accessions areas and areas areas areas areas areas areas areas areas and and accessions areas and and and accessions areas ar



Source: BAR Architects 3/22

Transportation Impact Study for the Dominican Valley Subdivision Project Figure 2 – Site Plan





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Circulation System

This section addresses the first transportation bullet point on the CEQA checklist, which relates to the potential for a project to conflict with a program, plan, ordinance, or policy addressing the circulation system, including transit, roadway, bicycle, and pedestrian facilities.

Pedestrian Facilities

Existing Pedestrian Facilities

Pedestrian facilities include sidewalks, crosswalks, pedestrian signal phases, curb ramps, curb extensions, and various streetscape amenities such as lighting, benches, etc. There are no pedestrian facilities along the streets fronting the project, and sidewalks are not generally present or required by the City in the hillside residential area. Sidewalks are provided within the Dominican University campus and along streets connecting the University to central San Rafael. It is noted that the University is the primary generator of pedestrian trips near the project site; otherwise, the project area is characterized by single family residential development. Given the low traffic volumes, narrowness of the streets, and slow vehicle speeds along the project frontage streets, existing facilities adequately meet the needs of the nominal number of anticipated pedestrian trips that might be generated by the project.

Pedestrian Safety

The collision history for the study area was reviewed to determine any trends or patterns that may indicate a safety issue for pedestrians. Collision records available from the California Highway Patrol as published in their Statewide Integrated Traffic Records System (SWITRS) reports were reviewed for the most current five-year period available, which was October 1, 2018, through September 30, 2023, at the time of the analysis. During the five-year study period there were two reported collisions involving pedestrians at the study intersection of Grand Avenue/Mission Avenue with the primary collision factor being a pedestrian right-of-way violation. Each of these collisions resulted in one pedestrian injury. As previously noted, all-way stop controls are present at this location, but nearby vegetation could potentially have impacted visibility of pedestrians crossing at this intersection.

Project Impacts on Pedestrian Facilities

Pedestrian demand is expected to be minimal for trips to and from the project site, and the City does not require sidewalks in the hillside residential area as it is characterized by low density and challenging topography. The project therefore would not conflict with policies related to multimodal circulation.

Finding – Pedestrian facilities serving the project site are considered adequate for the project context and anticipated demand.

Bicycle Facilities

Existing and Planned Bicycle Facilities

The Highway Design Manual, Caltrans, 2020, classifies bikeways into four categories:

- **Class I Multi-Use Path** a completely separated right-of-way for the exclusive use of bicycles and pedestrians with cross flows of motorized traffic minimized.
- **Class II Bike Lane** a striped and signed lane for one-way bike travel on a street or highway.



- **Class III Bike Route** signing only for shared use with motor vehicles within the same travel lane on a street or highway.
- Class IV Bikeway also known as a separated bikeway, a Class IV Bikeway is for the exclusive use of bicycles and includes a separation between the bikeway and the motor vehicle traffic lane. The separation may include, but is not limited to, grade separation, flexible posts, inflexible physical barriers, or on-street parking.

While there are no bicycle facilities in the immediate project area, Grand Avenue is a Class III bike route between 4th Street and Newhall Drive-Belle Avenue and Class IV bikeways are currently under construction along Grand Avenue from 4th Street to 2nd Street. Bicyclists ride in the roadway along all other streets within the project study area. Table 4 summarizes the existing and planned bicycle facilities in the project vicinity, as contained in the *San Rafael Bicycle Pedestrian Master Plan 2018 Update*.

Table 4 – Bicycle Facility Summary									
Status Location	Class	Length (miles)	Begin Point	End Point					
Existing									
Grand Ave	III	0.80	4 th St	Newhall Dr-Belle Ave					
4 th St	111	0.30	lrwin St	Union St					
Pt San Pedro Rd	11/111	0.54	Montecito Dr	City Limits (East)					
Planned									
3 rd St	I	0.40	Grand Ave	City Limits (East)					
4 th St	TBD	1.39	2 nd St	Union St					
Grand Ave	IV	0.11	2 nd St	4 th St					

Source: San Rafael Bicycle Pedestrian Master Plan 2018 Update, City of San Rafael, 2018

Bicyclist Safety

Collision records for the study area were reviewed to determine if there had been any bicyclist-involved crashes. During the five-year study period between October 1, 2018, and September 30, 2023, there were no reported collisions involving bicyclists at any of the study intersections or along the study roadway segments.

Project Impacts on Bicycle Facilities

Existing facilities together with shared use of minor streets provide adequate access for bicyclists around the project site. The City's adopted plans do not include bicycle facilities along any of the project frontage streets, and bicycle access is permitted on all streets throughout the project area. Therefore, the project would not conflict with City policy and would have a less-than-significant impact on bicycle circulation.

Bicycle Storage

The San Rafael Municipal Code, Section 14.18.090 includes bicycle parking requirements for multifamily residential projects, which are defined as buildings containing three or more attached dwelling units on a single lot. Since the proposed project would include only one dwelling unit per lot, including some lots with a JADU, bicycle parking is not required.

Finding – Bicycle storage is not required and is therefore adequate.



Transit Facilities

Existing Transit Facilities

The transit stop nearest the project site is located approximately one-half mile west at Grand Avenue/Acacia Way and is served by Marin Transit Routes 57 and 233.

Route 57 provides service to destinations between downtown San Rafael and Novato and stops on Grand Avenue, circling Dominican University. It operates Monday through Friday with headways of between approximately one-half-hour to one-hour between 6:25 a.m. and 9:45 p.m. On weekends, Route 57 does not serve San Rafael.

Route 233 services downtown San Rafael to Santa Venetia. It operates with one-hour headways between 6:30 a.m. and 7:25 p.m. on weekdays and between 8:00 a.m. and 5:25 p.m. on weekends.

Two bicycles can be carried on most Marin Transit buses. Bike rack space is on a first come, first served basis.

Dial-a-ride, also known as paratransit, or door-to-door service, is available for those who are unable to independently use the transit system due to a physical or mental disability. Marin Access Paratransit is designed to serve the needs of individuals with disabilities within three-quarters of a mile from regular fixed-routes in Marin County.

Impact on Transit Facilities

Transit service is not present along the streets fronting the project site. The nearest bus stop access to the project site is considered to be within an acceptable walking distance of one-half mile, but given the low-density residential uses a substantial number of transit trips to and from the proposed project is not anticipated. The project would not conflict with any policies relative to transit.

Finding – Transit facilities and service in the project area are adequate for the expected limited demand.

Significance Finding – The proposed project would not conflict with any plans or policies for transportation facilities. It would therefore have a less-than-significant impact on multimodal circulation.



Vehicle Miles Traveled (VMT)

The potential for the project to conflict or be inconsistent with CEQA Guidelines § 15064.3, subdivision (b) was evaluated based the project's anticipated Vehicle Miles Traveled (VMT).

The City of San Rafael Transportation Analysis Guidelines, 2021, includes procedures for analyzing VMT and thresholds of significance to assess project-related impacts. This document indicates that a residential project with VMT per capita that is greater than 15 percent below the nine-county Bay Area average would be considered to have a significant transportation impact.

In accordance with City guidelines, the project's potential VMT impact was assessed based on data from the Transportation Authority of Marin Demand Model (TAMDM). The TAMDM model includes traffic analysis zones (TAZ) covering geographic areas throughout Marin County, including 1,400 Micro Analysis Zones (MAZ) for which VMT is calculated. The 2019 version of the TAMDM was used for this analysis, and it includes updates made for the City of San Rafael General Plan. The nine-county Bay Area has a VMT per capita of 12.6, and 15 percent below this level is 10.7, which is the significance threshold. The project is located in MAZ 811769, which has a VMT per capita of 13.5. To reduce the VMT per capita from 13.5 to less than 10.7 and a less-than-significant impact would require a reduction of 20.7 percent.

Trip Reduction Strategies

Project Features

Since VMT is calculated by multiplying the number of vehicle trips by the trip length, project-related VMT is influenced by numerous factors such as the land use context, density, and inclusion of affordable housing.

Inclusion of Affordable Housing

As proposed, 20 percent of the proposed units in the Dominican Valley project would be designated as deedrestricted affordable housing. A methodology published in *Income, Location Efficiency, and VMT: Affordable Housing as a Climate Strategy*, The California Housing Partnership, 2015, was used to determine the VMT reductions associated with provision of onsite affordable housing (this method is also currently used by the City of San Jose). Applying the reductions for the proposed affordable units, the project's VMT would be reduced by 2.0 percent. This assumes that the residents would meet the "low income" criteria.



Pedestrian Infrastructure

While the lack of pedestrian infrastructure is consistent with existing development in the area, some residents of the project would have the ability to reach their destinations by walking; this would be especially true for residents living in units along Deer Park Avenue that work or study at Dominican University. Although there are few vehicles traveling along this segment, improvement of the infrastructure to allow for more comfortable pedestrian access from project site to the Dominican University campus would encourage additional walking trips. This would be expected to largely impact short trips, both to the University and the surrounding area, where a sidewalk network currently exists. While the number of vehicle trips would be reduced as a result, and there would be a reduction in VMT, the percentage reduction compared to the project VMT would be nominal.

Project Context

The land use context of the project should also support reduced VMT when compared with similar projects located farther away from a mixed-use downtown area like San Rafael. Since VMT is calculated by multiplying the number of vehicle trips by the trip length, project-related VMT is influenced by numerous factors. For example, the project is located approximately one-half mile from the nearest transit stop, which is considered an acceptable walking distance. However, there are numerous destinations within a relatively short distance of the project site. This includes the Downtown San Rafael SMART station, San Rafael Transit Center, and numerous grocery stores and other retail opportunities on the east side of US 101 that are within approximately 1.2 miles of the project site. The Transportation Authority of Marin (TAM) conducted an analysis of travel patterns throughout the County and determined that the average trip length in San Rafael is 8.2 miles. Therefore, while walking, bicycling and transit are not expected to be used for a high percentage of trips to destinations near the project site, the ability of residents to access nearby destinations via relatively short vehicle trips would have a beneficial impact on VMT in comparison with many other locations in Marin County.

Transportation Demand Management

Transportation Demand Management (TDM) measures have the potential to further reduce VMT by supporting use of non-vehicle transportation options. The project would establish a homeowner's association, which could serve as a mechanism to distribute transportation information to residents on a periodic basis and as new owners and tenants arrive. This would raise awareness of residents of Marin Commutes, which serves as a commuter information hub throughout Marin County, providing information about how to access a wide range of commuting options as well as incentive programs based on participation.

Ridesharing

Ridesharing can be a highly effective strategy for reducing vehicle trips and VMT. There are various options for carpooling in the Bay Area, through platforms including Marin Commutes and 511, which would enable local residents to identify ridesharing partners through a regional system. Ridesharing tends to have the lowest cost per passenger-mile of any motorized mode of transportation since it makes use of a vehicle seat that would otherwise be empty. It also provides financial savings for the consumer by decreasing fuel and parking costs. Further supporting the use of ridesharing and other nonvehicle transportation modes is the availability of the Emergency Ride Home (ERH) program administered through the Transportation Authority of Marin. This provides a greater level of security for people who use non-vehicle transportation options for commuting by offering reimbursement for a taxi or equivalent in case of an emergency.

The project would have a homeowner's association (HOA) to manage private streets and other facilities on the site. One option for encouraging ridesharing would be for the HOA to provide current and incoming project residents with information about how to take advantage of existing ridesharing options in the area. Encouragement of ridesharing is estimated to reduce VMT by approximately 2.0 percent.



Combined VMT Reduction Measures

The various strategies described are the most feasible options for reducing project VMT. As noted, the trip reduction for some measures can be quantified based on previous research. Other suggested measures are also expected to support VMT reductions but there is insufficient research available to estimate the magnitude of the reduction. The estimated VMT reduction for each measure is summarized in Table 5.

Table 5 – Summary of Potential Vehicle Miles Traveled (VMT) Reduction Measures								
Project Feature/TDM Strategy	Assumption	Estimated VMT Reduction						
Affordable Housing	20% of units	2.0%						
Ridesharing	N/A	2.0%						

Source: CAPCOA, 2021; TAMDM, 2022

Significance Finding – As currently proposed, the project would be expected to have a significant impact on VMT.



Safety Issues

The potential for the project to impact safety was evaluated in terms of the adequacy of sight distance and need for turn lanes at the project accesses. This section addresses the third transportation bullet on the CEQA checklist which is whether or not the project would substantially increase hazards due to a geometric design feature (e.g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment).

Site Access

The project includes frontages on Gold Hill Grade, Deer Park Avenue, and Margarita Drive, with the following access points.

- Gold Hill Grade: Five single family units would be accessed directly from Gold Hill Grade via individual driveways.
- Deer Park Avenue: Thirty-five (35) units would be accessed from an interior street that would connect to Deer Park Avenue, including 18 single family homes and 17 townhomes. Two access points are proposed along Deer Park Avenue, one at the existing Magnolia Avenue/Deer Park Avenue intersection and one approximately 360 feet south of that intersection.
- Margarita Drive: Ten (10) units, including four single family homes and six duplex units, would be accessed from a private street that would connect to Margarita Drive.

Gold Hill Grade, Deer Park Avenue, and Margarita Drive would all be widened to 26 feet along the project frontages. The private streets within the project would be 26 feet wide.

Sight Distance

Sight distances at the project access points and driveways were evaluated based on sight distance criteria contained in the *Guidelines for Geometric Design of Very Low-Volume Local Roads* published by AASHTO. Sight distance guidelines developed in this document are based on research that indicates increased sight distance on low-volume roadways would have minimal effect on crash frequency or severity, meaning that any work done to upgrade a low-volume roadway to the sight distance requirements contained in the Caltrans *Highway Design Manual* or the AASHTO *A Policy on Geometric Design of Highways and Streets* would likely not be economically beneficial. The guide provides recommended minimum stopping sight distance requirements using the approach travel speeds as the basis for determining the recommended sight distance appropriate for the case of roadways with volumes below 400 vehicles per day.

Sight distances at the project access points and driveways were evaluated using topographic survey and proposed site design data in AutoCAD format. Based on a design speed of 25 mph, the minimum stopping sight distance recommended is 125 feet in both directions at all access locations. Sight distances at all driveways on Gold Hill Grade, Deer Park Avenue, Margarita Drive, and the internal roadways would exceed 125 feet and therefore be adequate. Similarly, sight distances along Deer Park Avenue at the intersection of the western internal roadways and at the two connections to Deer Park Avenue would also exceed the minimum recommended distance.

Sight distances along Highland Drive at the Margarita Drive/Highland Drive intersection would exceed the minimum recommended distance of 125 feet to the north. To the south, only approximately 70 feet of sight distance would be available, which is appropriate for low-volume roadways with approach speeds of 15 mph or less. Given the steep grade, curvature, and paved width of Highland Avenue approaching the intersection from this direction, drivers on Highland Drive are likely traveling at speeds of 15 mph or less as they approach the intersection. This would make the available sight distance adequate. Further, drivers would be able to and are expected to creep into the intersection slightly to get a better vantage of traffic approaching from the opposite



lane. This creeping would extend the available sight distance to over 125 feet, which would satisfy the minimum recommendation for the *prima facie* speed limit of the roadway even if drivers are traveling much slower.

The connection of the new roadway, Margarita Drive, and Highland Avenue creates a six-legged intersection with complex sight line requirements, especially between the new roadway and Margarita Drive since they would come in at almost the same angle and directly adjacent to one another. There would be a large grade difference between Margarita Drive and the proposed roadway which would necessitate a retaining wall. However, the wall ends far enough back from the intersection and the pavement is wide enough that two drivers who arrive from these approaches at the same time would have sufficient pavement width and time to allow them to observe one another and yield as is required at uncontrolled intersections. The merging point of these two approaches is also set back from the intersection with Highland Avenue so drivers would only have to be concerned about merging with one stream of traffic at a time.

Significance Finding – The project would not introduce any hazards as a result of its design as sightlines are adequate at all proposed connections to the public street system.



Emergency Access

The final transportation bullet on the CEQA checklist requires an evaluation as to whether the project would result in inadequate emergency access or not.

The project is subject to the San Rafael's street design requirements for hillside development, as described in Section 15.07.030(a) of the City's municipal code. The minimum street width for hillside areas is 25 feet, although the existing frontage roadways are less than 20 feet wide. The San Rafael Fire Department access requirements exceed the minimum widths specified in the hillside development requirements, as they have established a minimum of 26 feet to allow for adequate emergency vehicle access. As indicated in the site plan, interior project roadways would be constructed to be 26 feet wide, and turnaround areas for fire trucks are included along the interior project roadways and along Gold Hill Grade. In addition, the segments of Gold Hill Grade, Deer Park Avenue, and Margarita Drive along the project frontages would be widened as part of the project to meet the Fire Department's minimum street width requirement.

Off-Site Impacts

In addition to enabling emergency vehicles to adequately serve the project, the widening of the frontage roads would provide improved emergency vehicle access to existing development in the area and would therefore be expected to improve emergency response times to the surrounding neighborhood.

Significance Finding – The proposed project would be designed to accommodate emergency response vehicles and would not impede emergency responders, resulting in a less-than-significant impact on emergency response.



Intersection Level of Service Methodologies

Level of Service (LOS) is used to rank traffic operation on various types of facilities based on traffic volumes and roadway capacity using a series of letter designations ranging from A to F. Generally, Level of Service A represents free flow conditions and Level of Service F represents forced flow or breakdown conditions. A unit of measure that indicates a level of delay generally accompanies the LOS designation.

The study intersections were analyzed using methodologies published in the *Highway Capacity Manual* (HCM), Transportation Research Board, 2010. This source contains methodologies for various types of intersection control, all of which are related to a measurement of delay in average number of seconds per vehicle.

The Levels of Service for the intersection of Grand Avenue/Locust Avenue, which has stop controls only on Locust Avenue, were analyzed using the "Two-Way Stop-Controlled" intersection capacity method from the HCM. This methodology determines a level of service for each minor turning movement by estimating the level of average delay in seconds per vehicle. Results are presented for individual movements together with the weighted overall average delay for the intersection.

The remaining two study intersections have stop signs on all approaches and were analyzed using the "All-Way Stop-Controlled" Intersection methodology from the HCM. This methodology evaluates delay for each approach based on turning movements, opposing and conflicting traffic volumes, and the number of lanes. Average vehicle delay is computed for the intersection as a whole and is then related to a Level of Service.

The ranges of delay associated with the various levels of service are indicated in Table 6.

Table	e 6 – Intersection Level of Service Criteria	
LOS	Two-Way Stop-Controlled	All-Way Stop-Controlled
А	Delay of 0 to 10 seconds. Gaps in traffic are readily available for drivers exiting the minor street.	Delay of 0 to 10 seconds. Upon stopping, drivers are immediately able to proceed.
В	Delay of 10 to 15 seconds. Gaps in traffic are somewhat less readily available than with LOS A, but no queuing occurs on the minor street.	Delay of 10 to 15 seconds. Drivers may wait for one or two vehicles to clear the intersection before proceeding from a stop.
С	Delay of 15 to 25 seconds. Acceptable gaps in traffic are less frequent, and drivers may approach while another vehicle is already waiting to exit the side street.	Delay of 15 to 25 seconds. Drivers will enter a queue of one or two vehicles on the same approach, and wait for vehicle to clear from one or more approaches prior to entering the intersection.
D	Delay of 25 to 35 seconds. There are fewer acceptable gaps in traffic, and drivers may enter a queue of one or two vehicles on the side street.	Delay of 25 to 35 seconds. Queues of more than two vehicles are encountered on one or more approaches.
E	Delay of 35 to 50 seconds. Few acceptable gaps in traffic are available, and longer queues may form on the side street.	Delay of 35 to 50 seconds. Longer queues are encountered on more than one approach to the intersection.
F	Delay of more than 50 seconds. Drivers may wait for long periods before there is an acceptable gap in traffic for exiting the side streets, creating long queues.	Delay of more than 50 seconds. Drivers enter long queues on all approaches.

Table 6 – Intersection Level of Service Criteria

Reference: Highway Capacity Manual, Transportation Research Board, 2010



Traffic Operation Standards

San Rafael General Plan Policy M-2.5 outlines a general citywide standard of LOS D operation, with exemptions for intersections in the Downtown Precise Plan boundary and signalized freeway ramp intersections.

Existing Conditions

The Existing Conditions scenario provides an evaluation of current operation based on existing traffic volumes during the a.m. and p.m. peak periods. This condition does not include project-generated traffic volumes. Volume data was collected at the study intersections on February 15 and February 22, 2024, while local schools were in session.

Under existing conditions all of the study intersections are operating acceptably. The existing traffic volumes are shown in Figure 3. A summary of the intersection Level of Service calculations is contained in Table 7, and copies of the calculations are provided in Appendix B.

Та	ble 7 – Existing Peak Hour Intersection Levels of Servio	ce			
Study Intersection		AM F	Peak	PM F	Peak
	Approach	Delay	LOS	Delay	LOS
1.	Grand Ave/Mission Ave	12.1	В	16.4	С
2.	Grand Ave/Jewell St	8.9	А	9.6	А
3.	Grand Ave/Locust Ave	1.9	А	2.2	А
	Westbound (Locust Ave) Approach	10.5	В	11.5	В

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*

Future Conditions

Segment volumes for the base and future years of 2019 and 2040, respectively, were obtained from TAMDM and translated to calculated growth factors. Future traffic volumes were developed based on these growth factors. The increment of new traffic projected was added to the actual counts used in the Existing Conditions scenario.

The model projected traffic volume decreases at the minor legs of the study intersections, and minimal volume decreases were observed elsewhere in the model. Such decreases are attributable to assumed infrastructure improvements and forecast changes in demographic data throughout the region. Rather than assume volume decreases, growth factors for the p.m. peak hours were calculated solely based on the major road volumes along Grand Avenue. For the a.m. peak hours, growth factors were calculated using all intersection arrival and departure volumes. This approach was used to ensure that the projections of future traffic volumes are conservative.

Under the anticipated Future volumes, all three study intersections are expected to operate at acceptable service levels. Future volumes are shown in Figure 4 and operating conditions are summarized in Table 8.





Transportation Impact Study for the Dominican Valley Subdivision Project Figure 3 – Existing Traffic Volumes





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Transportation Impact Study for the Dominican Valley Subdivision Project Figure 4 – Future Traffic Volumes



Та	Fable 8 – Future Peak Hour Intersection Levels of Service								
Study Intersection		AM F	Peak	PM F	PM Peak				
	Approach	Delay	LOS	Delay	LOS				
1.	Grand Ave/Mission Ave	12.6	В	17.3	С				
2.	Grand Ave/Jewell St	9.1	А	9.9	А				
3.	Grand Ave/Locust Ave	2.0	А	2.2	А				
	Westbound (Locust Ave) Approach	10.8	В	11.8	В				

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*

Project Conditions

Existing plus Project Conditions

Upon the addition of project-related traffic to the existing volumes, the study intersections are expected to operate acceptably. These results are summarized in Table 9. Project traffic volumes are shown in Figure 5.

Та	Table 9 – Existing and Existing plus Project Peak Hour Intersection Levels of Service									
Study Intersection		E	Condition	Ex	Existing plus Project					
	Approach		AM Peak		PM Peak		Peak	PM Peak		
		Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS	
1.	Grand Ave/Mission Ave	12.1	В	16.4	С	12.4	В	17.3	С	
2.	Grand Ave/Jewell St	8.9	А	9.6	А	9.0	А	9.9	А	
3.	Grand Ave/Locust Ave	1.9	А	2.2	А	2.1	А	2.4	А	
	Westbound (Locust Ave) Approach	10.5	В	11.5	В	10.5	В	11.6	В	

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*

It should be noted that with the addition of project-related traffic volumes, average delay at each intersection increases slightly during the a.m. and p.m. peak hours. However, these nominal increases in delay do not affect the overall Levels of Service at any of the three study intersections.

Finding – The study intersections are expected to continue operating acceptably at the same Levels of Service upon the addition of project-generated traffic as without it.

Future plus Project Conditions

Upon the addition of project-generated traffic to the anticipated future volumes, the study intersections are expected to operate acceptably. Future plus Project volumes are shown in Figure 6, and operating conditions are summarized in Table 10.

Finding – The study intersections are expected to continue operating acceptably with project traffic added to anticipated future volumes, at the same service levels as without it.





Transportation Impact Study for the Dominican Valley Subdivision Project Figure 5 – Project Traffic Volumes and Existing plus Project Traffic Volumes





Transportation Impact Study for the Dominican Valley Subdivision Project Figure 6 – Future plus Project Traffic Volumes



Study Intersection Approach		F	Future Conditions				Future plus Project			
		AM	AM Peak		PM Peak		AM Peak		PM Peak	
		Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS	
1.	Grand Ave/Mission Ave	12.6	В	17.3	С	12.9	В	18.3	С	
2.	Grand Ave/Jewell St	9.1	А	9.9	А	9.3	А	10.3	В	
3.	Grand Ave/Locust Ave	2.0	А	2.2	А	2.1	А	2.4	А	
	Westbound (Locust) Approach	10.8	В	11.8	В	10.8	В	11.9	В	

Table 10 – Future and Future plus Project Peak Hour Intersection Levels of Service

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*



Parking

The project was analyzed to determine whether the proposed parking supply would be sufficient for the anticipated parking demand. The project as proposed would provide a total of 169 standard parking spaces for the proposed 50 single-family housing units.

Jurisdiction parking supply requirements are provided in the San Rafael Municipal Code, Chapter 14.18; Parking Standards. Table 14.48.040 defines the minimum parking requirements for each land use; the proposed project falls under the "Single-family residential, hillside" classification. Typical single-family residential land uses typically require two covered parking spaces per unit. For hillside housing, residences on streets less than 26 feet wide are required to provide a minimum of two additional parking spaces for each housing unit. However, the project frontages and the interior project streets would all be 26 feet wide, so guest spaces are not required. It is noted that per Table 14.16.285 of the code no parking spaces are required for JADUs.

The project would provide 86 covered spaces and uncovered spaces. All of the units would include two covered spaces, with the exception of 14 of the townhomes, which would include one covered space. While guest parking is not required, all units would include at least one guest space. As a result, all units would meet or exceed the number of required parking spaces; however, not all spaces would meet the requirement for the spaces to be covered. The proposed parking supply and City requirements are shown in Table 11.

Table 11 – Parking Anal	ysis Summ	ary		
Land Use	Units	City Require	ements	Proposed Supply
		Rate	Spaces Required	
Single-Family Housing	27 du	2 covered spaces/unit	54 covered spaces	54 covered spaces, 54 guest spaces
Townhomes	17 du	2 covered spaces/unit	34 covered spaces	20 covered spaces, 17 guest spaces
Duplexes	6 du	2 covered spaces/unit	12 covered spaces	12 covered spaces, 12 guest spaces
Total	50 du		100 covered spaces	86 covered spaces, 83 guest spaces
Total Proposed Parking S	upply			169 spaces

Notes: du = dwelling unit

Finding – The proposed parking supply would exceed the City requirements based on capacity, but the project would not provide the required number of covered spaces.



Conclusions and Recommendations

Conclusions

- The proposed project is expected to generate an average of 421 trips per day, including 30 a.m. peak hour trips and 38 p.m. peak hour trips.
- The project would be consistent with City policies regarding pedestrian, bicycle, and transit facilities and would therefore have a less-than-significant impact on multimodal circulation.
- The project would have a VMT per capita that exceeds the City's significance threshold, so as currently proposed, the project's VMT impact is deemed significant.
- Emergency vehicle access would be adequate, and frontage improvements would result in improved access for emergency vehicles to properties in the surrounding neighborhood. Therefore, the impact of the project on emergency vehicle access is less than significant.
- The study intersections operate acceptably overall during both peak hours under existing conditions and would be expected to continue doing so with the addition of project trips.
- Under future volumes, all three study intersections are expected to continue to operate acceptably during the a.m. and p.m. peak hours, without and with the addition of project trips.
- The proposed parking supply would exceed the number of spaces specified in the City's requirements but would not include the required number of covered spaces for all units.

Recommendations

• Transportation demand management measures should be implemented through the project's homeowner's association to encourage use of non-vehicle transportation and reduce the VMT associated with project trips.



Study Participants and References

Study Participants

Principal in Charge	Dalene J. Whitlock, PE (Civil, Traffic), PTOE
Senior Traffic Engineer	Kenny Jeong, PE (Traffic)
Transportation Planner	Barry Bergman, AICP
Associate Engineer	Nick Brunetto, PE (Civil)
Assistant Engineer	Joseph Faria-Poynter, EIT, Alyssa Labrador, EIT
Graphics	Jessica Bender
Editing/Formatting	Jessica Bender
Quality Control	Dalene J. Whitlock, PE (Civil, Traffic), PTOE

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Appendix A

Collision Rate Calculations





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Intersec	tion Collisio	n Rate Workshe	et	
Dominica	n Valley Subdiv	ision Project		
Intersection # 3:	Grand Avenue &	& Locust Avenue		
Date of Count:	Thursday, Febru	uary 15, 2024		
Number of Collisions: Number of Injuries: Number of Fatalities: Average Daily Traffic (ADT): Start Date: End Date: Number of Years: Intersection Type: Control Type:	1 1 0 4200 October 1, 2018 September 30, 5 5 Tee Stop & Yield Co	3 2023 ntrols		
Area:	Urban			
Collision Rate =	Nun ADT x D	nber of Collisions x 1 Days per Year x Numb	Million er of Years	_
Collision Data	1	x 1,00	0,000	
Collision Rate =	4,200 x	365	x 5	
Study Intersection	Collision Rate	E Fatality Rate	Injury Rate 100.0%	_
Statewide Average*	0.13 c/mve	1.3%	47.3%	
Notes ADT = average daily total v c/mve = collisions per milli * 2021 Collision Data on C	ehicles entering on vehicles enter alifornia State Hi	intersection ring intersection ghways, Caltrans		

Appendix B

Intersection Level of Service Calculations





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HCM 6th AWSC 1: Grand Ave & Mission Ave

Intersection

Intersection Delay, s/veh Intersection LOS

Movement Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Peak Hour Factor Heavy Vehicles, % Mvmt Flow Number of Lanes

Number of Lanes Approach Opposing Approach Opposing Lanes Conflicting Lanes Left Conflicting Lanes Left Conflicting Lanes Right HCM Control Delay HCM LOS

Lane Vol Left, % Vol Left, % Vol Right, % Sign Conitol Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of UNI (X) Depatrure Headway (Hd) Convergence, VN Cap Service Time HCM Lane V/C Ratio HCM Lane LOS HCM 59th-tile Q

03/11/2024

HCM 6th AWSC 2: Grand Ave & Jewell St

03/11/2024

12.1											_
В											
EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
	4			4			4			4	
41	135	41	7	147	26	93	127	10	20	161	27
41	135	41	7	147	26	93	127	10	20	161	27
).89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89
2	2	2	2	2	2	2	2	2	2	2	2
46	152	46	8	165	29	104	143	11	22	181	30
0	1	0	0	1	0	0	1	0	0	1	0
В			WB			NB			SB		
WB			EB			SB			NB		
1			1			1			1		
SB			NB			EB			WB		
1			1			1			1		
NB			SB			WB			EB		
1			1			1			1		
12.1			11.5			12.6			11.9		
В			В			В			В		
	NBI n1	FBI n1	WBI n1	SBI n1							
	40%	19%	1%	10%							
	55%	62%	82%	77%							
	4%	19%	14%	13%							
	Stop	Stop	Stop	Stop							
	230	217	180	208							
	93	41	7	20							
	127	135	147	161							
	10	41	26	27							
	258	244	202	234							
	1	1	1	1							
	0.407	0.381	0.32	0.364							
	5.674	5.623	5.696	5.611							
	Yes	Yes	Yes	Yes							
	631	636	627	638							
	3.737	3.686	3.763	3.676							
	0.409	0.384	0.322	0.367							
	12.6	12.1	11.5	11.9							
	В	В	В	В							
	2	1.8	1.4	1.7							

Dominican Valley Subdivision VMT Study - Existing AM

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Dominican Valley Subdivision VMT Study - Existing AM

HCM 6th	TWSC
0.0.1	A O I

2: Crand Ave 8	, 1	ot As					03/11/
3: Grand Ave &	LOCU	ISL AV	/e				03/11/
Intersection							
Int Delay, s/veh	1.9						
Movement	WRI	WRR	NRT	NBR	SBI	SBT	
Lane Configurations	M	mon	1	Horr	002	4	
Traffic Vol. veh/h	12	37	131	26	37	173	
Future Vol. veh/h	12	37	131	26	37	173	
Conflicting Peds. #/hr	19	11	0	19	11	0	
Sian Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	-	None	-	None	-	None	
Storage Length	0	-					
Veh in Median Storage	,# 0	-	0	-	-	0	
Grade, %	0		0			0	
Peak Hour Factor	86	86	86	86	86	86	
Heavy Vehicles, %	2	2	2	2	2	2	
Mvmt Flow	14	43	152	30	43	201	
Major/Minor I	Minor1	1	Major1	I	Major2		
Conflicting Flow All	492	197	0	0	201	0	
Stage 1	186	-	-	-	-	-	
Stage 2	306	-	-	-		-	
Critical Hdwy	6.42	6.22	-	-	4.12	-	
Critical Hdwy Stg 1	5.42	-	-	-		-	
Critical Hdwy Stg 2	5.42	-	-	-	-	-	
Follow-up Hdwy	3.518	3.318	-	-	2.218	-	
Pot Cap-1 Maneuver	536	844	-	-	1371	-	
Stage 1	846	-	-	-	-	-	
Stage 2	747	-	-	-	-	-	
Platoon blocked, %			-	-		-	
Mov Cap-1 Maneuver	498	820	-	-	1346	-	
Mov Cap-2 Maneuver	498	-	-	-		-	
Stage 1	831	-	-	-		-	
Stage 2	707	-	-	-		-	
Approach	WB	_	NB	_	SB	_	
HCM Control Delay, s	10.5	_	0		1.4	_	
HCM LOS	В						
	_						
Minor Lane/Maior Mvm	ıt	NBT	NBR	VBLn1	SBL	SBT	
Capacity (veh/h)		-	-	708	1346	-	
HCM Lane V/C Ratio				0.08	0.032		
HCM Control Delay (s)			-	10.5	7.8	0	
1 15 7191 5 75 71 1115 71 1 75 37 4 9 1.17					1.0		
HCM Lane LOS		-	-	В	A	A	

Dominican Valley Subdivision VMT Study - Existing AM

Synchro 11 Report Page 3

HCM 6th AWSC 1: Grand Ave & Mission Ave

03/11/2024

Intersection												
Intersection Delay, s/veh	16.4											
Intersection LOS	С											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4.			4			4.			afa.	
Traffic Vol. veh/h	33	184	58	14	190	55	129	133	16	32	200	46
Future Vol. veh/h	33	184	58	14	190	55	129	133	16	32	200	46
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	35	196	62	15	202	59	137	141	17	34	213	49
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	C
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	16.4			15.7			17			16.5		
HCM LOS	С			С			С			С		
Lane		NBLn1	EBLn1	WBLn1	SBLn1							
Vol Left, %		46%	12%	5%	12%							
Vol Thru, %		48%	67%	73%	72%							
Vol Right, %		6%	21%	21%	17%							
Sign Control		Stop	Stop	Stop	Stop							
Traffic Vol by Lane		278	275	259	278							
LT Vol		129	33	14	32							
Through Vol		133	184	190	200							
RT Vol		16	58	55	46							
Lane Flow Rate		296	293	276	296							
Geometry Grp		1	1	1	1							
Degree of Util (X)		0.537	0.522	0.494	0.527							
Departure Headway (Hd)		6.534	6.421	6.448	6.412							
Convergence, Y/N		Yes	Yes	Yes	Yes							
Сар		550	559	557	559							
Service Time		4.611	4.494	4.524	4.488							
HCM Lane V/C Ratio		0.538	0.524	0.496	0.53							
HCM Control Delay		17	16.4	15.7	16.5							
HCM Lane LOS		С	С	С	С							
HCM 95th-tile Q		3.2	3	2.7	3.1							

Dominican Valley Subdivision VMT Study - Existing PM

HCM 6th AWSC	
2: Grand Ave & Jewell	St

03/11/2024

HCM 6th TWSC 3: Grand Ave & Locust Ave

Intersection Int Delay, s/veh 2.2

 Int Delay, siven
 2.2

 Movement
 WBL
 WBR
 NBT
 NBR
 SBL
 SBT

 Lane Configurations
 Y⁴
 P
 P
 off
 Taffic Valuehh
 15
 45
 213
 22
 31
 98

 Future Vol, veh/h
 15
 45
 213
 22
 31
 98

 Conflicting Peds,#hrh
 30
 17
 0
 30
 17
 0
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 17
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 Sign Control
 Stop Stop
 Free
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 Free
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 Free
 TRE
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 None
 - None
 - None
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 Grade, %
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 Grade, %
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 Peak Hour Factor
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SB 1.9

NB

 Major/Minor
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 Conflicting Flow All
 511
 311
 0
 307
 0

 Stage 1
 294

 Stage 2
 217

 Critical Hdwy
 642
 6.22

 Critical Hdwy Stg
 5.42

 Follow-up Hdwy
 3.518
 3.318
 2.218

 Follow-up Hdwy
 3.518
 3.318
 2.218

 Pot Cap-1 Maneuver
 523
 729
 1254

 Stage 1
 766

 Mov Cap-1 Maneuver
 477
 697
 1218

 Mov Cap-1 Maneuver
 477
 697
 1218

 Mov Cap-2 Maneuver
 474

03/11/2024

Intersection												
Intersection Delay, s/yel	h 9.6											
Intersection LOS	A											
Movement	FRF	ERI	EBK	WBL	WRI	WBR	NBL	NRI	NRK	SBL	SBI	SBR
Lane Configurations		-	0		-		0	()	54	40	↔	0
Traffic Vol, ven/n	4	/	9	55	6	14	6	217	54	13	156	3
Future Vol, ven/n	4	0.05	0.05	55	0.05	14	0.05	217	54	13	156	0.05
Peak Hour Factor	0.00	0.00	0.65	0.00	0.65	0.00	0.00	0.65	0.00	0.00	0.00	0.00
Heavy Venicles, %	2	2	11	2	2	16	2	2	2 64	15	10/	2
Number of Lense	0	0		00	1	10	1	200	04	10	104	4
NUMBER OF Lanes	U	1	0	U	1	U	U	1	U	U	1	U
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Le	eft SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Ri	ghNB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	8.2			9			10.2			9.2		
HCM LOS	A			A			В			A		
Lane	1	VBLn1	EBLn1V	VBLn1	SBLn1							
Vol Left, %		2%	20%	73%	8%							
Vol Thru, %		78%	35%	8%	91%							
Vol Right, %		19%	45%	19%	2%							
Sign Control		Stop	Stop	Stop	Stop							
Traffic Vol by Lane		277	20	75	172							
LT Vol		6	4	55	13							
Through Vol		217	7	6	156							
RT Vol		54	9	14	3							
Lane Flow Rate		326	24	88	202							
Geometry Grp		1	1	1	1							
Degree of Util (X)		0.393	0.033	0.127	0.257							
Departure Headway (Ho	d)	4.337	5.006	5.167	4.573							
Convergence, Y/N		Yes	Yes	Yes	Yes							
Сар		831	712	692	785							
Service Time		2.365	3.06	3.214	2.606							
HCM Lane V/C Ratio		0.392	0.034	0.127	0.257							
HCM Control Delay		10.2	8.2	9	9.2							
HCM Lane LOS		В	A	A	A							
HCM 95th-tile Q		1.9	0.1	0.4	1							

Dominican Valley Subdivision VMT Study - Existing PM

Synchro 11 Report Page 2

Dominican Valley Subdivision VMT Study - Existing PM

 Ninor Lane/Major Mvmt
 NBT
 NBRWBLn1
 SBL
 SBT

 Capacity (veh/h)
 625
 1218

 HCM Lane V/C Ratio
 0.113
 0.03

 HCM Control Delay (s)
 11.5
 8
 0

 HCM Lane LOS
 B
 A
 A

 HCM Stih %tile Q(veh)
 0.4
 0.1

 Approach
 WB

 HCM Control Delay, s
 11.5

 HCM LOS
 B

HCM 6th AWSC	

Intersection Intersection Delay, s/veh Intersection LOS 12.6 B Movement Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Peak Hour Factor Heavy Vehicles, % Mvmt Flow Number of Lanes WBT NBT NBR EBL EBT EBR WBL NBL SBT SBR
 43
 141
 43
 7
 153
 27
 97
 133
 10
 21
 168
 28

 43
 141
 43
 7
 153
 27
 97
 133
 10
 21
 168
 28

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 0.8 2 2 48 158 0 1 2 2 2 30 109 149 24 189 48 8 172 11 31 0 0 Aurober of Lanes Approach Opposing Approach Opposing Lanes Conflicting Lanes Left Conflicting Lanes Right HCM Control Delay HCM LOS EB NB SB NB SB 1 EB EB 1 WB 1 SB NB WB 1 NB 1 SB 1 EB 1 WB 1 12.7 1 11.9 1 13.3 1 12.4 В В В Lane
Vol Left, %
Vol Try, %
Vol Right, %
Sigin Control
Sigin Control
Traffic Vol by Lane
LT Vol
Lane Flow Rate
Geometry Grp
Degree of Ulii (X)
Departure Headway (Hd)
Convergence of Uli (X)
Gap
Service Time
HCM Lane V/C Ratio
HCM Lane LOS
HCM 59th-Ilie Q NBLn1 EBLn1 WBLn1 SBLn1 40% 55% 4% 19% 62% 19% 4% 10% 82% 77% 14% 13%
 4%
 19%
 14%
 13%

 Slop
 Slop
 Slop
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 Slop

 240
 227
 187
 217

 37
 43
 27
 28

 133
 141
 153
 168

 10
 43
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 270
 255
 210
 244

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 0433
 0.406
 0.339
 0.388

 5.784
 5.784
 5.816
 5.725

 Yes
 Yes
 Yes
 Yes

 Yes
 Yes
 Yes
 Yes

 0.437
 0.41
 0.342
 0.391

 0.437
 0.41
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 0.391

 13.
 12
 11.9
 124
 B B B B 2.2 2 1.5 1.8

Dominican Valley Subdivision VMT Study - Future AM

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HCM 6th AWSC 2: Grand Ave & Jewell St

	_	_										
Intersection												
Intersection Delay, s/veh	9.1											
Intersection LOS	A											
Movement	FBI	FBT	FBR	WBI	WBT	WBR	NBI	NBT	NBR	SBI	SBT	SBR
Lane Configurations		1			1			1			4	
Traffic Vol. veh/h	5	11	14	52	14	39	2	159	48	35	162	4
Future Vol. veh/h	5	11	14	52	14	39	2	159	48	35	162	4
Peak Hour Factor	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	5	12	15	57	15	43	2	175	53	38	178	4
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	ED			\//D			ND			CD		
Opposing Approach	W/D			ED			CD			ND		
Opposing Approach	1			1			30			1		
Conflicting Approach Lot	1 00			ND			ED			WD		
Conflicting Lance Left	1			IND 1			LD 1			1		
Conflicting Approach Ric	hNR			SR			W/R			FR		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	81			8.8			92			94		
HCMIOS	A			A			A			A		
1 200	N	IDI n1 I	EDI n11	MDI n1	CDI n1							
Volloft %		10/	170/	E09/	170/							
Vol Lett, %		769/	270/	120/	010/							
Vol Tillu, 76		220/	J170	270/	0170							
Sign Control		Stop	4170 Stop	Stop	Stop							
Traffic Vol by Lane		200	30	105	201							
T Vol		205	50	52	35							
Through Vol		159	11	14	162							
RT Vol		48	14	39	4							
Lane Flow Rate		230	33	115	221							
Geometry Grp		1	1	1	1							
Degree of Util (X)		0.281	0.045	0.156	0.281							
Departure Headway (Hd)	4.412	4.86	4.865	4.572							
Convergence, Y/N		Yes	Yes	Yes	Yes							
Сар		813	734	735	784							
Service Time		2.447	2.912	2.908	2.607							
HCM Lane V/C Ratio		0.283	0.045	0.156	0.282							
HCM Control Delay		9.2	8.1	8.8	9.4							
HCM Lane LOS		A	A	A	A							
HCM 95th-tile Q		1.2	0.1	0.6	1.2							

Dominican Valley Subdivision VMT Study - Future AM

Synchro 11 Report Page 2

03/11/2024

HCM 6th TWSC	
3: Grand Ave & Locust Ave	Э
	_

/e & Locust Ave		
		_

HCM 6th AWSC 1: Grand Ave & Mission Ave

17.3 C

EBL

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EB

WB 1 SB

1 NB

1 17.3

EBT

201 36

EBR WBL

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> > WB

EB 1

NB

1 SB

1 16.5

 NBLn1
 EBLn1
 WBLn1
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 46%
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 72%

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 Stop
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 136
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 Yes

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 0.518
 0.552

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 16.5
 17.4

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C C C 3.3 2.9 3.3

C 3.4

NBLn1 EBLn1 WBLn1 SBLn1

C

WBT

WBR

NBL NBT

0

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SB 1

EB

WB

1 17.9

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1

 59
 14
 195
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 136
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NBR

Intersection Intersection Delay, s/veh Intersection LOS

Movement Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Peak Hour Factor Heavy Vehicles, % Mvmt Flow Number of Lanes

Number of Lanes

Number of Lanes Approach Opposing Approach Opposing Lanes Conflicting Lanes Left Conflicting Lanes Right Conflicting Lanes Right HCM Control Delay HCM LOS

Lane
Lane
Vol Left, %
Vol Try, %
Vol Right, %
Sign Control
Traffic Vol by Lane
LT Vol
Through Vol
Lane Flow Rate
Geometry Grp
Degrees of Ulii (X)
Departure Headway (Hd))
Camvergence, Y/N
Cap
Service Time
HCM Lane V/C Ratio
HCM Lane LOS
HCM 95th-tile Q

03/11/2024

SBR

35 218 50 0 1 0

NB 1

WB

17.4

С

1

Internetica.						
Intersection						
Int Delay, s/veh	2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	- M		ĥ			સ
Traffic Vol, veh/h	13	40	143	28	40	189
Future Vol, veh/h	13	40	143	28	40	189
Conflicting Peds, #/hr	19	11	0	19	11	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	e,# 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	86	86	86	86	86	86
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	15	47	166	33	47	220
Maior/Minor	Minor1		Maior1		Maior2	
Conflicting Flow All	535	213	0	0	218	0
Stage 1	202	210	-	-	210	-
Stage 2	333					
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stn 1	5.42	0.22				
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318			2.218	
Pot Cap-1 Maneuver	506	827	-	-	1352	-
Stage 1	832	-			-	
Stage 2	726	-	-	-	-	-
Platoon blocked, %						
Mov Cap-1 Maneuver	469	804	-	-	1328	-
Mov Cap-2 Maneuver	469	-			-	
Stage 1	817	-	-	-	-	-
Stage 2	685	-			-	
America	14/0		ND		00	
Approach	WB 40.0		NB		SB	
HCM Control Delay, s	10.8		0		1.4	
HCM LOS	В					
Minor Lane/Major Mvn	nt	NBT	NBRV	VBLn1	SBL	SBT
Capacity (veh/h)		-	-	684	1328	-
HCM Lane V/C Ratio				0.09	0.035	
HCM Control Delay (s)	-	-	10.8	7.8	0
HCM Lane LOS				В	A	A
HCM 95th %tile Q(veh	I)	-	-	0.3	0.1	-

Dominican Valley Subdivision VMT Study - Future AM

Synchro 11 Report Page 3

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Dominican Valley Subdivision VMT Study - Future PM

HCM 6th AWSC	
2: Grand Ave & Jewell St	

03/11/2024

HCM 6th TWSC 3: Grand Ave & Locust Ave

WBL WBR NBT NBR SBL SBT

 Y
 Image: block of the state of

Intersection

Lane Configurations Traffic Vol, veh/h Future Vol, veh/h

Int Delay, s/veh Movement

Intersection Intersection Delay, s/veh 9.9 Intersection LOS A Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBF Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Peak Hour Factor Heavy Vehicles, % Mvmt Flow
 Image: constraint of the state of Number of Lanes 0 0 0 0 0 0 0 1 0 Approach EB WB
 Approach
 EB

 Opposing Approach
 WB

 Opposing Lanes
 1

 Conflicting Lanes Left
 3

 HCM LOS
 A
 EB NB 1 SB 1 NB EB WB ть 1 WB 1 SB 1 EB 1 9.1 1 9.4 A Α NBLn1 EBLn1WBLn1 SBLn1 Lane
 NBLN1EBLn1WBLn1SBLn1

 2%
 19%
 74%
 8%

 78%
 33%
 7%
 91%

 20%
 48%
 19%
 2%

 Slop
 Stop
 Stop
 Stop

 296
 21
 80
 183

 6
 4
 59
 14

 232
 7
 6
 166

 58
 10
 15
 3

 348
 25
 94
 215

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 1
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 1

 0.423
 0.035
 0.137
 0.276

 4.372
 5.081
 5.248
 4.621
 Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio HCM Lontrol Delay HCM Lon LOS 4.372 5.081 5.248 4.621
 4.3/2
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 Yes
 Yes
 Yes
 Yes
 Yes

 822
 700
 680
 775

 2.406
 3.144
 3.303
 2.659

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 0.138
 0.277

 10.6
 8.3
 9.1
 9.4

 B
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 A
 A

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 0.5
 1.1
 HCM Lane LOS HCM 95th-tile Q

 Future vol, venh
 16
 48
 228
 24
 33
 105

 Conflicting Pedes, #hr
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 39
 124
 Heavy Vehicles, % Mvmt Flow Major/Minor Minor1 Major1 Major2 Conflicting Flow All Stage 1 Stage 2 Critical Hdwy Critical Hdwy Stg 1 Critical Hdwy Stg 2 Followeing Hdwy 544 329 0 0 326 312 - - -232 - - - -0 232 -6.42 6.22 5.42 -- 4.12 5.42
 Critical Howy Stg 2
 5.42

 Follow-up Howy
 3.518

 Pot Cap-1 Maneuver
 500

 T12
 Stage 1

 Stage 1
 742

 Nage 2
 807

 Platoon blocked, %

 Mov Cap-1 Maneuver
 455

 Mov Cap-1 Maneuver
 455

 Stage 1
 720

 Stage 2
 76
 2.218 - 1234 - 1199 720 756 Stage 2 ApproachWBHCM Control Delay, s11.8HCM LOSB SB NB <u>NBT NBRWBLn1 SBL SBT</u> - - 605 1199 -- 0.124 0.032 -Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s) HCM Lane LOS HCM 95th %tile Q(veh) 11.8 8.1 0 B A 0.1

Dominican Valley Subdivision VMT Study - Future PM

Synchro 11 Report Page 2 Dominican Valley Subdivision VMT Study - Future PM

Synchro 11 Report Page 3

03/11/2024

HCM 6th AWSC	
1: Grand Ave & Mission Ave	

03/11/2024

Intersection												
Intersection Delay, s/veh	12.4											
Intersection LOS	В											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SE
Lane Configurations		\$			\$			\$			4	
Traffic Vol, veh/h	44	135	41	7	147	27	93	129	10	23	167	
Future Vol, veh/h	44	135	41	7	147	27	93	129	10	23	167	
Peak Hour Factor	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	49	152	46	8	165	30	104	145	11	26	188	
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	
Approach	EB			WB			NB			SB		
Opposing Approach	WB			FB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			FB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NR			SB			WB			FR		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	12.4			11.6			12.9			12.4		
HCMLOS	B			B			B			B		
1001200	5			5			0			5		
Lane		NBLn1	EBLn1	WBLn1	SBLn1							
Vol Left. %		40%	20%	4%	10%							_
Vol Thru, %		56%	61%	81%	75%							
Vol Right. %		4%	19%	15%	15%							
Sign Control		Stop	Stop	Stop	Stop							
Traffic Vol by Lane		232	220	181	223							
I T Vol		93	44	7	23							
Through Vol		129	135	147	167							
RT Vol		10	41	27	33							
Lane Flow Rate		261	247	203	251							
Geometry Gro		1	1	1	1							
Degree of Util (X)		0.415	0.391	0.326	0.393							
Departure Headway (Hd)		5.736	5.698	5.772	5.64							
Convergence Y/N		Yes	Yes	Yes	Yes							
Can		623	628	618	634							
Service Time		3 805	3.77	3 847	3 709							
		0.410	0.393	0.328	0.396							
HCM Lane V/C Ratio			0.000	0.020	0.000							
HCM Lane V/C Ratio		12.0	12.4	11.6	12 /							
HCM Lane V/C Ratio HCM Control Delay		12.9	12.4	11.6	12.4							

Dominican Valley Subdivision VMT Study - Existing + Project AM

Synchro 11 Report Page 1 HCM 6th AWSC 2: Grand Ave & Jewell St

Intersection	_	_	_	_	_	_	_	_	_	_	_	_
Intersection Delay, elve	h C											
Intersection Delay, sive	n 9											
IIILEISECIIOII LOS	M											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		- 4÷			- ()			4			- 4 >	
Traffic Vol, veh/h	5	10	13	63	13	36	2	146	50	32	148	4
Future Vol, veh/h	5	10	13	63	13	36	2	146	50	32	148	4
Peak Hour Factor	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91	0.91
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	5	11	14	69	14	40	2	160	55	35	163	4
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Le	eft SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Ri	ighNB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	8.1			8.8			9			9.2		
HCM LOS	A			A			A			A		
Lane	1	VBLn1	EBLn1V	VBLn1	SBLn1							
Vol Left, %		1%	18%	56%	17%							
Vol Thru, %		74%	36%	12%	80%							
Vol Right, %		25%	46%	32%	2%							
Sign Control		Stop	Stop	Stop	Stop							
Traffic Vol by Lane		198	28	112	184							
LT Vol		2	5	63	32							
Through Vol		146	10	13	148							
RT Vol		50	13	36	4							
Lane Flow Rate		218	31	123	202							
Geometry Grp		1	1	1	1							
Degree of Util (X)		0.265	0.041	0.165	0.257							
Departure Headway (He	d)	4.392	4.802	4.835	4.571							
Convergence, Y/N		Yes	Yes	Yes	Yes							
Cap		818	742	740	785							
Service Time		2.422	2.851	2.875	2.601							
HCM Lane V/C Ratio		0.267	0.042	0.166	0.257							
HOM CONTROL Delay		9	8.1	6.8	9.2							
HOM Lane LOS		A	A	A	A							
HOM 95th-tile Q		1.1	U.1	0.6	1							

Dominican Valley Subdivision VMT Study - Existing + Project AM

Synchro 11 Report Page 2

03/11/2024

HCM 6th TWSC	
3: Grand Ave & Locust Ave	

HCM 6th AWSC 1: Grand Ave & Mission Ave

17.3 C

EBL

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EB

WB 1 SB

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EBT

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Intersection Intersection Delay, s/veh Intersection LOS

Movement Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Peak Hour Factor Heavy Vehicles, % Mvmt Flow Number of Lanes

Number of Lanes

Approach Opposing Approach Opposing Lanes Conflicting Approach Left Conflicting Lanes Left Conflicting Lanes Left Conflicting Lanes Right HCM Control Delay HCM LOS

Lane Vol Left, % Vol Trynt, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, YN Cap Service Time HCM Lane V/C Ratio HCM Contro Delay HCM Lane LOS HCM S5th-tile Q

03/11/2024

SBR

36 217 53 0 1 0

NB 1

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WB

Interpetion						
Intersection	0.4					
Int Delay, s/ven	Z. I					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		f,			4
Traffic Vol, veh/h	12	44	131	26	39	173
Future Vol, veh/h	12	44	131	26	39	173
Conflicting Peds, #/hr	19	11	0	19	11	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-		-
Veh in Median Storage	e,#0	-	0	-	-	0
Grade, %	0		0			0
Peak Hour Factor	86	86	86	86	86	86
Heavy Vehicles, %	2	2	2	2	2	2
Mymt Flow	14	51	152	30	45	201
Major/Minor	Minorf		Inior1		Violar?	
		407	viajori	-		C
Conflicting Flow All	496	197	0	0	201	0
Stage 1	186	-		-	-	-
Stage 2	310	-	-	-	-	-
Critical Hdwy	6.42	6.22	-	-	4.12	
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42		-	-		-
Follow-up Hdwy	3.518	3.318	-	-	2.218	-
Pot Cap-1 Maneuver	533	844	-	-	1371	
Stage 1	846	-	-	-	-	-
Stage 2	744	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	495	820	-	-	1346	-
Mov Cap-2 Maneuver	495	-	-	-	-	-
Stage 1	831	-	-	-	-	-
Stage 2	703	-		-	-	-
, in the second s						
Annraach	14/12		ND		CD.	
Approach	10.5		DVI		30	
HCIM Control Delay, s	10.5		U		1.4	
HUM LUS	В					
Minor Lane/Major Mvn	nt	NBT	NBR	VBLn1	SBL	SBT
Capacity (veh/h)		-	-	719	1346	-
HCM Lane V/C Ratio				0.091	0.034	
HCM Control Delay (s))			10.5	7.8	0
HCM Lane LOS				B	A	Ă
HCM 95th %tile O(veh)		-	0.3	0.1	-
	/			0.0	0.1	

Dominican Valley Subdivision VMT Study - Existing + Project AM

Synchro 11 Report Page 3

03/11/2024

Dominican Valley Subdivision VMT Study - Existing + Project PM

HCM 6th	AWSC	
2. Grand	Ave & Jewell St	

03/11/2024

HCM 6th TWSC 3: Grand Ave & Locust Ave

03/11/2024

later estima												
Intersection												
Intersection Delay, s/ve	h 9.9											
Intersection LOS	A											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		44			4.			44			4	
Traffic Vol. veh/h	4	7	9	65	6	14	6	217	71	13	156	3
Future Vol, veh/h	4	7	9	65	6	14	6	217	71	13	156	3
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	5	8	11	76	7	16	7	255	84	15	184	4
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	FB	_	_	WB			NB			SB	_	_
Opposing Approach	WB			FB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Le	ft SB			NB			FB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Ri	ahNB			SB			WB			FB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	8.3			9.2			10.5			9.3		
HCM LOS	A			A			В			A		
lano	N	JRI n1 I	FRI n1\	VRI n1	SRI n1							
Vall oft 9/	- 1	20/	2000/	769/	00/							
Vol Leit, 70		Z%	20%	79/	0%							
Vol Tillu, 70		2.49/	00 %	1 70	31%							
Sign Control		24% Stop	40% Stop	Stop	Stop							
Traffic Vol by Lano		- 3ιυρ 20/	300p	310P	- 3ιυρ 172							
Tame vor by Lane		294	20	65	13							
Through Vol		217	7	6	156							
RT Vol		71	a	14	3							
I ane Flow Rate		346	24	100	202							
Geometry Gro		1	1	100	1							
Degree of Util (X)		0.418	0.033	0 145	0.26							
Departure Headway (Ho	d)	4 346	5.071	5.23	4 629							
Convergence Y/N	-)	Yes	Yes	Yes	Yes							
Cap		827	702	683	775							
Service Time		2.376	3.134	3,284	2.667							
HCM Lane V/C Ratio		0.418	0.034	0.146	0.261							
HCM Control Delay		10.5	8.3	9.2	9.3							
HCM Lane LOS		B	A	A	A							
HCM 95th-tile Q		2.1	0.1	0.5	1							

Dominican Valley Subdivision VMT Study - Existing + Project PM
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Synchro 11 Report Page 2

ITILEISECLIOIT						
Int Delay, s/veh	2.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	M		1.			1
Traffic Vol. veh/h	15	49	213	22	38	98
Future Vol. veh/h	15	40	213	22	38	98
Conflicting Dada #/hr	20	43	210	20	17	30
Contlicting Peas, #/nr	Stop	Ctop	Free	30	Free	Eree
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Unannelized	-	ivone		Ivone		None
Storage Length	0		-			-
Veh in Median Storag	e,# 0		0		-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	85	85	85	85	85	85
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	18	58	251	26	45	115
Major/Minor	Minor1		Maior1		Maior2	
Conflicting Flow All	E 20	211		0	207	0
Connicting Flow All	029	311	0	0	307	0
Stage 2	294	-	-	-	-	-
Stage Z	233	0.00	-	-	4.40	-
Critical Howy	0.42	0.22	-	-	4.12	
Critical Howy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-		-	
Follow-up Hdwy	3.518	3.318	-	-	2.218	-
Pot Cap-1 Maneuver	510	729		-	1254	-
Stage 1	756	-	-	-	-	-
Stage 2	804	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	462	697	-	-	1218	-
Mov Cap-2 Maneuver	462	-	-	-	-	-
Stage 1	734	-	-	-	-	-
Stage 2	751	-		-	-	-
Approach	W/D		ND		CD	
Approach	44.C		INB		<u>58</u>	
HCM Control Delay, s	11.6		0		2.3	
HCM LOS	В					
Minor Lane/Maior Myr	nt	NBT	NBR	VBLn1	SBL	SBT
Canacity (yeh/h)		-		623	1218	-
HCM Lane V/C Ratio				0 121	0.037	
HCM Control Delay (s)			11.6	8.1	0
HCM Lane LOS	9			- 1.0 R	Δ	Δ
HCM 95th %tile O(vet	2)			0.4	0.1	
HOW SOUL WILL OF A	9			0.4	0.1	-

Dominican Valley Subdivision VMT Study - Existing + Project PM

HCM 6th AWSC
1: Grand Ave & Mission Ave

03/11/2024

HCM 6th AWSC
2: Grand Ave & Jewell St

Intersection Intersection Delay, s/veh 9.3 Intersection LOS A

Movement Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Peak Hour Factor Heavy Vehicles, % Mvmt Flow Number of Lanes

Number of Lanes

 Number of Lanes
 0

 Approach
 EB

 Opposing Approach
 WB

 Opposing Lanes
 1

 Conflicting Approach Left SB
 Conflicting Lanes Left

 Conflicting Lanes Left
 1

 Conflicting Lanes Right
 1

 HCM Control Delay
 8.2

 HCM LOS
 A

Lane
Vol Left, %
Vol Try, %
Vol Right, %
Sign Control
Traffic Vol by Lane
LT Vol
Through Vol
Lane Flow Rate
Geometry Grp
Degree of Ull (X)
Departure Headway (Hd)
Convergence, Y/N
Cap
Service Time
HCM Lane L/C Ratio
HCM Lane LOS
HCM 95th-tile Q

A

EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR

 Construction
 Construction<

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SB

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WB

1 EB 1 9.5 A

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EB 1 NB

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03/11/2024

Intersection												
Intersection Delay, s/veh	12.9											
Intersection LOS	B											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4			4	
Traffic Vol, veh/h	46	141	43	7	153	28	97	135	10	24	174	34
Future Vol, veh/h	46	141	43	7	153	28	97	135	10	24	174	34
Peak Hour Factor	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89	0.89
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	52	158	48	8	172	31	109	152	11	27	196	38
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	13			12.1			13.5			12.9		
HCM LOS	В			В			В			В		
Lane		NBLn1	EBLn1	WBLn1	SBLn1							
Vol Left, %		40%	20%	4%	10%							
Vol Thru, %		56%	61%	81%	75%							
Vol Right, %		4%	19%	15%	15%							
Sign Control		Stop	Stop	Stop	Stop							
Traffic Vol by Lane		242	230	188	232							
LT Vol		97	46	7	24							
Through Vol		135	141	153	174							
RT Vol		10	43	28	34							
Lane Flow Rate		272	258	211	261							
Geometry Grp		1	1	1	1							
Degree of Util (X)		0.442	0.417	0.346	0.417							
Departure Headway (Hd)		5.848	5.811	5.894	5.755							
Convergence, Y/N		Yes	Yes	Yes	Yes							
Сар		612	615	604	620							
Service Time		3.931	3.896	3.985	3.838							
HCM Lane V/C Ratio		0.444	0.42	0.349	0.421							
HCM Control Delay		13.5	13	12.1	12.9							
HCM Control Delay HCM Lane LOS		13.5 B	13 B	12.1 B	12.9 B							

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Synchro 11 Report Page 1

Dominican Valley Subdivision VMT Study - Future + Project AM

3: Grand Ave & Locust Ave

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Ave & Locust Ave	03/11/2024

HCM 6th AWSC
1: Grand Ave & Mission Ave

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NBL NBT

Intersection Intersection Delay, s/veh Intersection LOS

Movement Lane Configurations Traffic Vol, veh/h Future Vol, veh/h Peak Hour Factor Heavy Vehicles, % Mvmt Flow Number of Lanes

Number of Lanes

Number of Lanes Approach Opposing Approach Opposing Lanes Conflicting Lanes Left Conflicting Lanes Right Conflicting Lanes Right HCM Control Delay HCM LOS

Lane
Lane
Vol Left, %
Vol Try, %
Vol Right, %
Sign Control
Traffic Vol by Lane
LT Vol
Through Vol
Lane Flow Rate
Geometry Grp
Degrees of Ulii (X)
Departure Headway (Hd))
Camvergence, Y/N
Cap
Service Time
HCM Lane V/C Ratio
HCM Lane LOS
HCM 95th-tile Q

03/11/2024

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 Image: Constand of the system
 Image: Constando

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Intersection						
mersection						
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in Delay, aven	۷.۱					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	- Y		- î>			୍ ଶ୍
Traffic Vol, veh/h	13	47	143	28	42	189
Future Vol, veh/h	13	47	143	28	42	189
Conflicting Peds, #/hr	19	11	0	19	11	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0		-	-		-
Veh in Median Storag	e,# 0	1.1	0	-		0
Grade, %	0		0	-		0
Peak Hour Factor	86	86	86	86	86	86
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	15	55	166	33	49	220
Major/Minor	Minor1	h	Maior1		Maior2	
Conflicting Flow All	530	213		0	218	0
Stage 1	202	213	U	0	210	0
Stage 2	202					-
Critical Uduar	6.40	6.22			/ 10	
Critical Holes Ct- 4	0.4Z	0.22	-		4.12	-
Critical Howy Stg 1	5.42					-
Critical Howy Stg 2	5.42	2.240			-	
Policiw-up Hawy	3.518	3.310			1250	
Pot Gap-1 Maneuver	003	02/	-		1352	
Stage 1	632					-
Stage 2	723		-	-		-
Platoon blocked, %			-			-
	10-				1000	
Mov Cap-1 Maneuver	465	804		-	1328	
Mov Cap-1 Maneuver Mov Cap-2 Maneuver	465	804	-	-	1328	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1	465 465 817	804 - -	-	-	1328	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2	465 465 817 680	804 - - -	-	-	1328 - - -	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2	465 465 817 680	804 - - -	-	-	1328 - -	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2	465 465 817 680	804 - -	- - - NB	-	1328 - - - -	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay s	465 465 817 680 WB	804 - -	- - - NB	-	1328 - - - - SB 1.4	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS	465 465 817 680 WB 10.8	804 - -	- - - NB 0	-	1328 - - - - - - - - - - - - - - - - - - -	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS	465 465 817 680 WB 10.8 B	804 - -	- - - NB 0	-	1328 - - - - - - - - - - - - - - - - - - -	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS	465 465 817 680 WB 10.8 B	804 - -	- - - NB 0	-	1328 - - - - - - - - - - - - - - - - - - -	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvr	465 465 817 680 WB 10.8 B	804 - - - NBT	- - - - 0 NBRV	- - - VBLn1	1328 - - - - - - - - - - - - - - - - - - -	- - - - SBT
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvr Capacity (veh/h)	465 465 817 680 WB 10.8 B mt	804 - - - - NBT	- - - - - 0 - - -	- - - VBLn1 694	1328 - - - - - - - - - - - - - - - - - - -	- - - - - -
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM Los Minor Lane/Major Mvr Capacity (veh/h) HCM Lane V/C Ratio	465 465 817 680 WB 10.8 B	804 - - - - NBT - -	- - - - - 0 - - -	- - - - VBLn1 694 0.101	1328 - - - - - - - - - - - - - - - - - - -	- - - - - - - -
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvr Capacity (veh/h) HCM Lane V/C Ratio	465 465 817 680 WB 10.8 B mt	804 - - - - - - - - - -	- - - - - - 0 - - - -	- - - - - - - - - - - - - - - - - - -	1328 - - - - - - - - - - - - - - - - - - -	- - - - - - - 0
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvr Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s HCM Lane LOS	465 465 817 680 WB 10.8 B mt	804 - - - - - - - - - - -	- - - - - - 0 - - - - -	- - - - - - - - - - - - - - - - - - -	1328 - - - - - - - - - - - - - - - - - - -	- - - - - - - - - - - 0 A

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HCM 6th AWSC	
2: Grand Ave & Jewell St	_

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HCM 6th TWSC 3: Grand Ave & Locust Ave

Intersection Int Delay, s/veh 2.

2.4

Intersection												
Intersection Delay, s/veh1	10.3											
Intersection LOS	В											
Manager			M/DI	MOT	14/00	NDI	NDT	NDD	0.01	ODT	000	
Movement E	ERL ER	I EBR	WBL	WBI	WBR	INBL	INBI	NBK	SBL	SBI	SBR	
Lane Configurations		» 7 40	00	•	45	0	000	75	4.4	400	2	
Tramic Vol, ven/n	4	7 10	69	0	15	0	232	75	14	100	3	
Future Vol, Ven/n Deek Heur Fester	4	/ IU	0.95	0 95	0.95	0 05	232	0.05	0.95	0.01	0.95	
Heaver Vehicles 9/	0.0 0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Mumt Elow	5	2 Z 9 10	81	2	18	2	273	2	16	105	2	
Number of Lance	0	1 0	01	1	0	0	213	00	0	130	4	
Number of Lanes	0	1 0	0		0	0		0	0		0	
Approach	EB		WB			NB			SB			
Opposing Approach	WB		EB			SB			NB			
Opposing Lanes	1		1			1			1			
Conflicting Approach Left	SB		NB			EB			WB			
Conflicting Lanes Left	1		1			1			1			
Conflicting Approach Righ	hNB		SB			WB			EB			
Conflicting Lanes Right	1		1			1			1			
HCM Control Delay	8.4		9.4			11			9.6			
HCM LOS	A		A			В			A			
Lane	NBLn	1 EBLn1	WBLn1	SBLn1								
Vol Left, %	29	6 19%	77%	8%								
Vol Thru, %	749	6 33%	7%	91%								
Vol Right, %	249	6 48%	17%	2%								
Sign Control	Sto	p Stop	Stop	Stop								
Traffic Vol by Lane	31	3 21	90	183								
LT Vol		6 4	69	14								
Through Vol	23	2 7	6	166								
RT Vol	7	5 10	15	3								
Lane Flow Rate	36	8 25	106	215								
Geometry Grp	0.11	1 1	0.450	1								
Degree of Util (X)	0.44	9 0.035	0.156	0.28								
Departure Headway (Hd)	4.38	0 0.148	5.311 V-	4.081								
Convergence, Y/N	Ye	s Yes	Yes	Yes								
Capico Timo	82	1 690	0/1	764								
Service Time	2.42	Z J.ZZ4 0 0.026	3.375	2.724								
HOW Control Dolay:	0.44	0 0.030	0.100	0.201								
HCM Long LOS	1	1 0.4	9.4 A	J.0								
HCM 95th tile 0	2	D A	A 0.6	A 11								
LIVAN STREET	· · · · · · · · · · · · · · · · · · ·	J U.I	0.0									
	_											

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		Þ			କ
Traffic Vol, veh/h	16	52	228	24	40	105
Future Vol, veh/h	16	52	228	24	40	105
Conflicting Peds. #/hr	30	17	0	30	17	0
Sian Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	
Veh in Median Storage	.# 0	-	0		-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	85	85	85	85	85	85
Heavy Vehicles, %	2	2	2	2	2	2
Mymt Flow	19	61	268	28	47	124
Major/Minor	Minor1	1	Major1		Major2	
Conflicting Flow All	560	329	0	0	326	0
Stage 1	312	-	-	-	-	-
Stage 2	248	-	-	-	-	-
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	-	-	2.218	
Pot Cap-1 Maneuver	489	712	-	-	1234	-
Stage 1	742	-	-	-	-	
Stage 2	793	-	-	-	-	-
Platoon blocked, %			-	-		
Mov Cap-1 Maneuver	442	680	-	-	1199	-
Mov Cap-2 Maneuver	442	-	-	-	-	
Stage 1	720	-	-	-	-	-
Stage 2	738					
otago 2	100					
Approach	WB		NB		SB	
HCM Control Delay, s	11.9		0		2.2	
HCM LOS	В					
Miner Leve Marine Mar		NDT	NDDU	NDL = 4	ODI	ODT
Minor Lane/Major MVn	11	INB I	NBRV	VBLNI	SBL	281
Capacity (ven/n)		-	-	604	1199	
HCM Lane V/C Ratio		-	-	0.132	0.039	-
HCM Control Delay (s)		-	-	11.9	8.1	0
HCM Lane LOS		-	-	В	A	A
HCM 95th %tile Q(veh)		-	0.5	0.1	

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