PRELIMINARY HYDROLOGY STUDY

FOR

NORTHGATE WALK

San Rafael, California

Prepared For: Empire USA Real Estate Investments 1801 Century Park E., Suite 2400 Los Angeles, CA 90067

Prepared By: CSW/Stuber-Stroeh Engineering Group, Inc. 45 Leveroni Court Novato, California 94949 (415)-883-9850

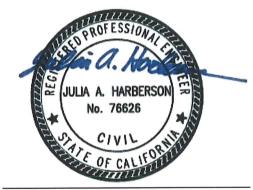
Prepared: July 1, 2016

CSW | ST2 File No.: 5.1455.00

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Julia A. Harberson R.C.E. # 76626, Exp. 12/31/2016

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1. INTRODUCTION

This Hydrology Study is prepared at the request of the Empire USA Real Estate Investments. This report analyzes the existing and proposed 25- and 100-year peak discharge rates to ensure the proposed peak discharge rate does not exceed the existing.

2. SCENARIOS ANALYZED

2.1 <u>Existing Condition</u>:

The Northgate Walk project is located in the City of San Rafael, California, in the county of Marin, at the intersection of Manuel T. Freitas Parkway and Highway 101. The site is bounded to the south by an office building and Manuel T. Freitas Parkway, to the east by an existing drainage channel and to the west by Highway 101. The site is relatively flat with embankments of either side leading towards the existing drainage channel and Highway 101.

The Northgate Walk site consists of two parcels, one developed as a gas station and the second developed as a hotel. The existing site is split into twelve (12) subwatersheds. Runoff discharges from the site at six (6) points of concentration (POC #A, POC #B, POC #C, POC #D, POC #Channel and POC #E). POC #A through POC #D and POC #Channel all discharge into the existing drainage channel east of the project site. POC #E discharges towards Highway 101. See H1-Exisiting Conditions Hydrology Map.

2.2 <u>Proposed Condition</u>:

The Northgate Walk project site is a redevelopment of the existing site. The proposed redevelopment is divided into eighteen (18). Runoff discharges from the site at seven (7) points of concentration (POC #A, POC #B, POC #B' (new), POC #C, POC #D, POC #Channel and POC #E). POC #A through POC #D and POC #Channel all discharge into the existing drainage channel east of the project site. POC #E discharges towards Highway 101. See H2-Proposed Conditions Hydrology Map.

3. ANALYSIS

3.1 Criteria

This report follows the criteria contained within the "County of Marin Department of Public Works Hydrology Manual Simplified Instructions," dated 8/2/00. The analysis herein utilizes the Rational Method to calculate pre- and post-project peak flows. Rainfall Intensities for use with the Rational Method are developed from

Intensity-Duration-Frequency data available from the National Oceanic Atmospheric Administration (NOAA) specific to the geographic location of the project site.

3.2 <u>Hydrology</u>

a. <u>Rational Method</u>: The Rational Method was utilized to calculate design peak discharge in accordance with the County of Marin Department of Public Works Hydrology Manual Simplified Instructions. The Rational Method is based on the following formula:

Q=CIA

Where: Q = Flow Rate (cubic feet per second, cfs)

C = Runoff Coefficients

I = Rainfall Intensity (inches per hour, in/hr)

A = Tributary Area (acres, ac)

- b. <u>Time of Concentration</u>: The time of concentration (T_c) is composed of three parts, including:
 - Overland flow travel time (length limit < 500feet) which is based on the overland flow equation:

$$T_o = \frac{1.8(1.1-c)\sqrt{L}}{\sqrt[3]{S(100)}} + 5 \ min$$

Where: T_0 = Overland Flow Travel Time (minutes, min)

C = Runoff Coefficient

L = Longest Run (linear feet)

S = Average Slope (ft/ft)

2. Channelized flow/shallow concentrated flow which is calculated by using:

$$T_{c} = L/(60*V)$$

Where: T_C = Shallow Concentrated Flow Travel Time (min)

L = Length of flow (feet)

V = Velocity (feet per second)

Where the velocity was calculated by using the computer program Hydraflow Express Extension for AutoCAD C3D 2012.

3. Pipe flow which is calculated by using:

$$T_p = L/(60*V)$$

Where: T_p = Shallow Concentrated Flow Travel Time (min)
L = Length of flow (feet)
V = Velocity (feet per second)

Where the velocity was calculated by using the computer program Hydraflow Express Extension for AutoCAD C3D 2012.

The total time of concentration is determined by using the following equation:

$$T_C = T_O + T_C + T_P$$

- c. <u>Rainfall Intensity</u>: Intensities for Rational Method calculations were determined using the intensity-duration-frequency (IDF) curves created from the National Oceanic and Atmospheric Administration's (NOAA) Point Precipitation Frequency Estimates. See Appendix 6.1.
- d. <u>Basin Delineation</u>: The watershed basins were based on contour data a topographic field survey and supplemented with data from the Marin County Geographical Information System (GIS, Marin Maps). See Hydrology Maps.
- e. <u>Runoff Coefficient</u>: Runoff coefficients for the project were assigned based on the surface type. For permeable surfaces (landscape and natural hillside) a runoff coefficient of 0.7 was utilized. For impervious surfaces (pavement and roofs) a runoff coefficient of 0.9 was used. For areas of mixed surface types, a weighted runoff coefficient was calculated. See Appendix 6.2.
- f. Hydrograph Analysis: The existing and proposed watersheds were analyzed using the computer modeling program Hydraflow Hydrograph Extension for AutoCAD Civil3D 2014. Hydraflow Hydrograph utilized the rational method and the hydrologic characteristics describe above to create hydrographs of each scenario. The hydrographs were modeled for each watershed in the existing and proposed condition for the 25- and 100-year storm events. The existing and proposed conditions were compared to confirm the proposed condition 25- and 100-year peak discharge rate did not exceed the existing condition. The synthetic hydrograph was created using the rational method to determine the peak discharge rates. The National Resources Conservation Services (NRCS, formerly the Soil Conservations Survey or SCS) recommends a 8/3 time base to time to peak ratio. This results in a 1 to 1.66 lag to receding leg ratio. A conservative 1 to 2 lag to receding leg ratio was applied to the hydrographs in this analysis. See Appendix 6.3.

4. RESULTS

4.1 Existing Conditions

Table 4.1.1 –Peak Discharge Calculations for 25-Year Storm Event

Watershed	Tributary Watershed (ac)	C-Factor	Time of Concentration (minutes)	Discharge (cfs)
Channel	8.58	0.85	12	18.36
Highway 101	0.69	0.70	14	1.176

- 1. See Appendix 6.2 Hydrology Calculations
- 2. See Appendix 6.3 Hydrograph Model Output

Table 4.1.1 -Peak Discharge Calculations for 100-Year Storm Event

Watershed	Tributary Watershed (ac)	C-Factor	Time of Concentration (minutes)	Discharge (cfs)
Channel	8.58	0.85	12	24.01
Highway 101	0.69	0.70	14	1.539

- 1. See Appendix 6.2 Hydrology Calculations
- 2. See Appendix 6.3 Hydrograph Model Output

4.2 <u>Proposed Conditions</u>

Table 4.1.1 -Peak Discharge Calculations for 25-Year Storm Event

Watershed	Tributary Watershed (ac)	C-Factor	Time of Concentration (minutes)	Discharge (cfs)
Channel	8.72	0.87	13	18.25
Highway 101	0.55	0.75	14	1.005

- 1. See Appendix 6.2 Hydrology Calculations
- 2. See Appendix 6.3 Hydrograph Model Output

Table 4.1.1 - Peak Discharge Calculations for 100-Year Storm Event

Watershed	Tributary Watershed (ac)	C-Factor	Time of Concentration (minutes)	Discharge (cfs)
Channel	8.72	0.87	13	23.88
Highway 101	0.55	0.75	14	1.315

- 1. See Appendix 6.2 Hydrology Calculations
- 2. See Appendix 6.3 Hydrograph Model Output

5. CONCLUSIONS

The proposed redevelopment of the Northgate Walk project does not increase the peak discharge rates for the 25- and 100-year recurrence interval storm event.

6.0 APPENDICES

Appendix 6.1 – Intensity-Duration-Frequency Data



NOAA Atlas 14, Volume 6, Version 2 Location name: San Rafael, California, US* Latitude: 38.0087°, Longitude: -122.5436° Elevation: 58 ft* * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹								in inches/	hour) ¹
				Averag	ge recurrenc	e interval (y	ears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	1.76 (1.57-2.00)	2.17 (1.93-2.46)	2.75 (2.44–3.13)	3.24 (2.84-3.73)	3.97 (3.35-4.75)	4.56 (3.74-5.60)	5.20 (4.15-6.58)	5.88 (4.55-7.69)	6.86 (5.05-9.43)	7.68 (5.42–11.0)
10-min	1.27 (1.13-1.43)	1.55 (1.39–1.77)	1.97 (1.75–2.24)	2.32 (2.04–2.68)	2.84 (2.40-3.41)	3.27 (2.69-4.01)	3.73 (2.98-4.71)	4.22 (3.26-5.51)	4.92 (3.62–6.76)	5.50 (3.89-7.87)
15-min	1.02 (0.908-1.16)	1.26 (1.12-1.42)	1.59 (1.41–1.81)	1.88 (1.64–2.16)	2.29 (1.93-2.74)	2.64 (2.17–3.24)	3.00 (2.40-3.80)	3.40 (2.62-4.44)	3.97 (2.92–5.45)	4.44 (3.13-6.34)
30-min	0.750 (0.668-0.850)	0.924 (0.822-1.05)	1.17 (1.04–1.33)	1.38 (1.21–1.59)	1.69 (1.42-2.02)	1.94 (1.60-2.38)	2.21 (1.77–2.80)	2.50 (1.93-3.27)	2.92 (2.15–4.01)	3.27 (2.31-4.67)
60-min	0.537 (0.479-0.609)	0.662 (0.589-0.751)	0.837 (0.742-0.954)	0.988 (0.868-1.14)	1.21 (1.02–1.45)	1.39 (1.14–1.71)	1.58 (1.26–2.00)	1.79 (1.39-2.34)	2.09 (1.54–2.87)	2.34 (1.65-3.35)
2-hr	0.404 (0.360-0.458)	0.498 (0.443-0.566)	0.630 (0.558-0.717)	0.742 (0.652-0.854)	0.906 (0.764-1.09)	1.04 (0.854–1.28)	1.18 (0.944-1.49)	1.33 (1.03-1.75)	1.55 (1.14–2.13)	1.73 (1.22-2.48)
3-hr	0.342 (0.304-0.387)	0.421 (0.374-0.478)	0.531 (0.471-0.605)	0.625 (0.549-0.720)	0.762 (0.642-0.912)	0.872 (0.718-1.07)	0.990 (0.791-1.25)	1.12 (0.863-1.46)	1.30 (0.955-1.78)	1.45 (1.02-2.07)
6-hr	0.252 (0.225-0.286)	0.311 (0.277-0.354)	0.393 (0.348-0.448)	0.462 (0.405-0.532)	0.560 (0.472-0.671)	0.639 (0.526-0.785)	0.722 (0.577-0.914)	0.811 (0.627-1.06)	0.937 (0.689-1.29)	1.04 (0.733-1.49)
12-hr	0.178 (0.159-0.202)	0.224 (0.199-0.254)	0.284 (0.252-0.324)	0.335 (0.294-0.386)	0.407 (0.343-0.487)			0.584 (0.451-0.764)	0.670 (0.493-0.920)	
24-hr	0.120 (0.108-0.136)	0.153 (0.137-0.173)	0.196 (0.176-0.223)	0.232 (0.207-0.266)	0.282 (0.244-0.333)	0.321 (0.272-0.386)	0.361 (0.299-0.444)	0.402 (0.326-0.508)	0.460 (0.358-0.602)	
2-day	0.081 (0.073-0.092)	0.103 (0.093-0.117)	0.132 (0.119-0.151)	0.156 (0.139-0.179)	0.189 (0.163-0.223)	0.214 (0.182-0.258)	0.240 (0.199-0.295)			0.332 (0.251-0.448)
3-day	0.062 (0.056-0.071)	0.079 (0.071-0.090)	0.101 (0.091-0.115)	0.119 (0.106-0.137)	0.144 (0.125-0.170)	0.163 (0.138-0.196)	0.182 (0.151-0.224)			
4-day	0.052 (0.047-0.059)	0.066 (0.059-0.075)	0.084 (0.075-0.096)	0.099 (0.088-0.113)	0.119 (0.103-0.140)	0.134 (0.114-0.162)		0.166 (0.134-0.209)	0.187 (0.146-0.245)	0.204 (0.154-0.275)
7-day	0.036 (0.032-0.041)	0.046 (0.041-0.052)	0.058 (0.052-0.066)	0.069 (0.061-0.079)	0.082 (0.071-0.097)				0.127 (0.099-0.167)	0.138 (0.104-0.186)
10-day	0.029 (0.026-0.033)	0.037 (0.034-0.042)	0.048 (0.043-0.054)	0.056 (0.050-0.064)	0.067 (0.058-0.079)	0.075 (0.064-0.090)	0.083 (0.069-0.102)	0.091 (0.074-0.115)	0.102 (0.079-0.134)	0.110 (0.083-0.149
20-day	0.040	0.005	0.024	0.027	0.044 (0.038-0.052)	0.049 (0.041-0.058)	0.053 (0.044-0.066)	0.058 (0.047-0.073)	0.064 (0.050-0.084)	(0.052-0.092
30-day	0.015	0.020	0.025	0.030	0.035 (0.030-0.041)	0.039 (0.033-0.047	0.042 (0.035-0.052)	0.046 (0.037-0.058)	0.050 (0.039-0.066	0.053 (0.040-0.072
45-day	0.042	0.016	0.021	0.024	0.028 (0.024-0.033)	0.031 (0.026-0.038	0.034 (0.028-0.042)	0.037 (0.030-0.046)		0.042 (0.032-0.057
60-day		0.045	0.040	0.024	0.025 (0.021-0.029)	0.027	0.030	11 0.032	0.034 (0.027-0.045	0.036) (0.027-0.049

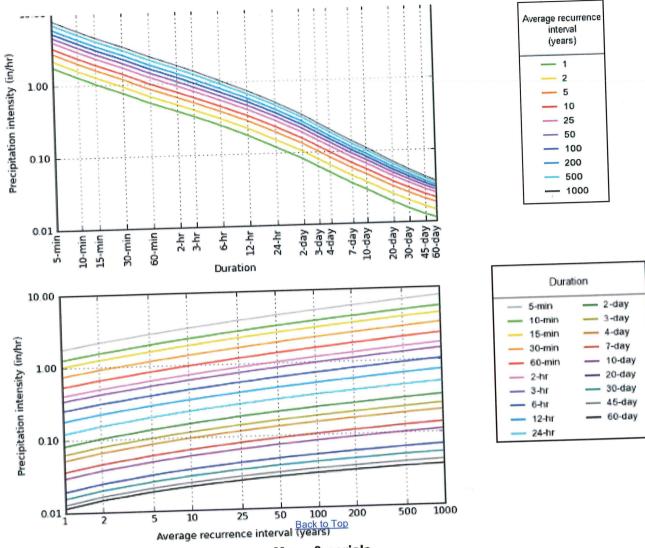
Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

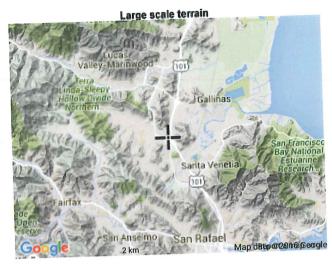
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PF graphical



Maps & aerials
Created (GMT): Wed Jun 29 22:20:21 2016
NOAA Atlas 14, Volume 6, Version 2









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Appendix 6.2 – Hydrology Calculations

Northgate Walk

Date Prepared: 07/01/2016

Prepared By: JAH

				Existing	Conditions	Hydrology	Calculation	ons		
Points of	Watershed I.D.	Area (ac)	Area (sf)	Impervious Area (sf)	Pervious Area (sf)	C _{IMP}	C _{PERV}	C _{WT}	T _c (min)	(in
Concentration			12013	10854	1159	0.9	0.7	0.88		
	1	0.28		26030	1370	0.9	0.7	0.89		
	2	0.63	27400	47560	2503	0.9	0.7	0.89	12.2	2
Α	3	1.15	50063	31612	1664	0.9	0.7	0.89	12.2	-
Tota	4	0.76	33275		2300	0.9	0.7	0.89		
	5	1.06	45991	43691	8996	0.9	0.7	0.89		
	Total - A	3.87	168742	159747	11988	0.9	0.7	0.85		
	6	1.09	47427	35440		0.9	0.7	0.89	11.4	
В	7	1.13	49389	46919	2469		0.7	0.87		
	Total - B	2.22	96816	82359	14457	0.9	0.7	0.89	9.9	
С	8	0.34	14676	13942	734	0.9		0.89	0.0	
	9	0.62	27162	25803	1358	0.9	0.7	0.85	9.2	-
D	10	0.21	9125	6816	2309	0.9	0.7		3.2	
	Total - D	0.83	36286	32619	3667	0.9	0.7	0.88	6.5	_
	11	1.32	57412	0	57412	0.9	0.7	0.70		_
Channel		0.69	30071	0	30071	0.9	0.7	0.70	14.5	
E	12	0.05	330,2	Colored to Man State Colored						

Northgate Walk

Date Prepared: 07/01/2016

Prepared By: JAH

				Propose	d Conditions	Hydrolog	y Calculati	ons		Tropies
Points of Concentration	Watershed I.D.	Area (ac)	Area (sf)	Impervious Area (sf)	Pervious Area (sf)	C _{IMP}	C _{PERV}	C _{WT}	T _c (min)	(iı
Concentration	1	0.17	7324	7324	0	0.9	0.7	0.90		
•	2	0.16	6920	6920	0	0.9	0.7	0.90	6.0	
Α	Total - A	0.33	14244	14244	0	0.9	0.7	0.90		
	3	0.16	7086	6647	439	0.9	0.7	0.89	440	
	4	0.52	22834	20036	2798	0.9	0.7	0.88	14.9	
В	Total - B	0.69	29919	26682	3237	0.9	0.7	0.88		
51 (11)	10tar - B	0.80	34702	31377	3325	0.9	0.7	0.88	8.8	_
B' (New)	6	1.59	69464	65991	3473	0.9	0.7	0.89	11.3	+
C (New)	7	0.16	6875	6013	862	0.9	0.7	0.87		
	8	0.40	17604	16302	1301	0.9	0.7	0.89	-	
	9	0.08	3368	3012	356	0.9	0.7	0.88		
	10	0.06	2650	1984	666	0.9	0.7	0.85		
	11	0.38	16714	15925	789	0.9	0.7	0.89	12.6	
D	12	0.28	12001	10842	1159	0.9	0.7	0.88	4	
	13	0.63	27400	26030	1370	0.9	0.7	0.89	-	
	14	1.00	43407	41237	2170	0.9	0.7	0.89		
	15	0.76	33208	31548	1660	0.9	0.7	0.89		
	Total - D	3.75	163227	152893	10334	0.9	0.7	0.89		+
	16	0.55	23919	23120	799	0.9	0.7	0.89	0.0	
Channel	17	1.02	44556	4498	40058	0.9	0.7	0.72	9.8	
Channel	Total - Chan		68475	27618	40857	0.9	0.7	0.78	12.7	+
E	18	0.55	23980	6479	17501	0.9	0.7	0.75	13.7	

CSW ST2

45 Leveroni Ct Novato, CA 94948

ation Calc					Pipe Flow					
V (ft/s)	T _s (min)	Q _{100 EST} (cfs)	Length (ft)	Elev. Up		Slope (ft/ft)	V (ft/s)	T _P (min)	Total T _c (min)	
(11/3)	(111111)		414	100	85.9	0.03	8.78	8.0	12.2	
		6.44				0.01	5.13	0.3	11.4	
4.1	0.5	3.70	95	78.8	78	0.01	3.13	0.0	9.9	
			n/a							
		0.76	110	67.5	64.7	0.03	4.66	0.4	9.2	
		0.76	110	07.5	n/a			•	6.5	
									14.5	
					n/a				14.5	

	culations		Pipe Flow							
V (**/c)	T _s (min)	Q _{100 EST} (cfs)	Length (ft)	Elev. Up		Slope (ft/ft)	V (ft/s)	T _P (min)	Total T _o (min)	
(ft/s)	(111111)		464	104.5	70.0	0.07	8.10	1.0	6.0	
		1.54		75.2	65.5	0.08	8.85	0.2	14.9	
		1.85	118		59.5	0.15	13.13	0.3	8.8	
		3.12	203	89.0			10.15	0.8	11.3	
		5.20	516	87.3	59.0	0.05			12.7	
		15.09	753	100.1	64.7	0.05	13.27	0.9		
		123.00			n/a				9.8	
	1				n/a				13.7	
2.8	1.0				11/4					

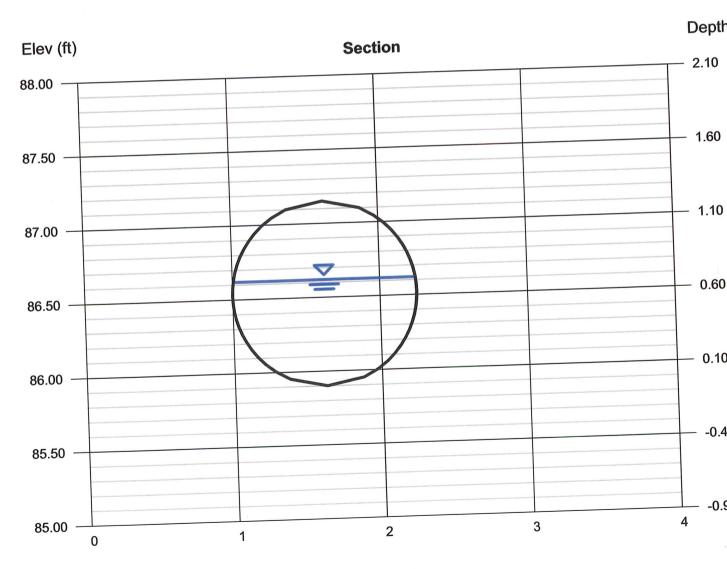
Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Thursday, Jun 30 2016

POC A - Pipe Flow (Existing)

Circular Diameter (ft)	= 1.25	Highlighted Depth (ft) Q (cfs) Area (sqft)	= 0.72 = 6.440 = 0.73
Invert Elev (ft) Slope (%) N-Value	= 85.90 = 3.00 = 0.014	Velocity (ft/s) Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)	= 8.78 = 2.16 = 1.03 = 1.24 = 1.92
Calculations Compute by: Known Q (cfs)	Known Q = 6.44		

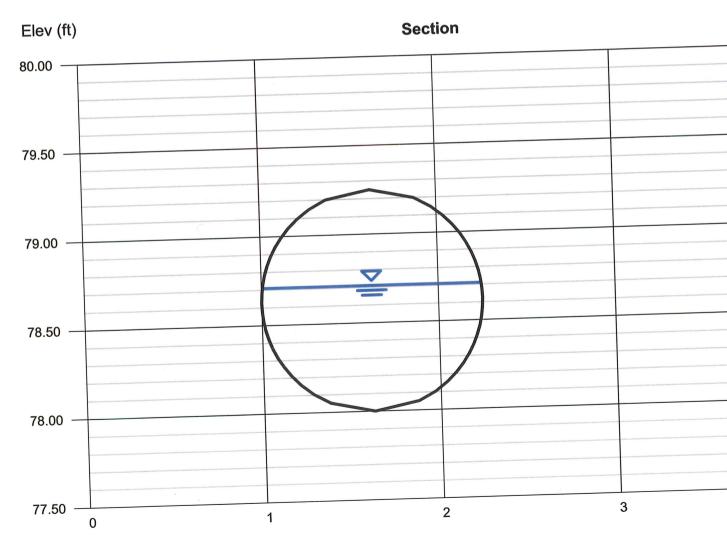


Reach (ft)

Thursday, Jun 30 2016

POC B - Pipe Flow (Existing)

Circular Diameter (ft)	= 1.25	Highlighted Depth (ft) Q (cfs) Area (sqft)	= 0.71 = 3.700 = 0.72
Invert Elev (ft) Slope (%) N-Value	= 78.00 = 1.00 = 0.014	Velocity (ft/s) Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)	= 5.13 = 2.14 = 0.78 = 1.24 = 1.12
Calculations Compute by: Known Q (cfs)	Known Q = 3.70	LGL (it)	



Reach (ft)

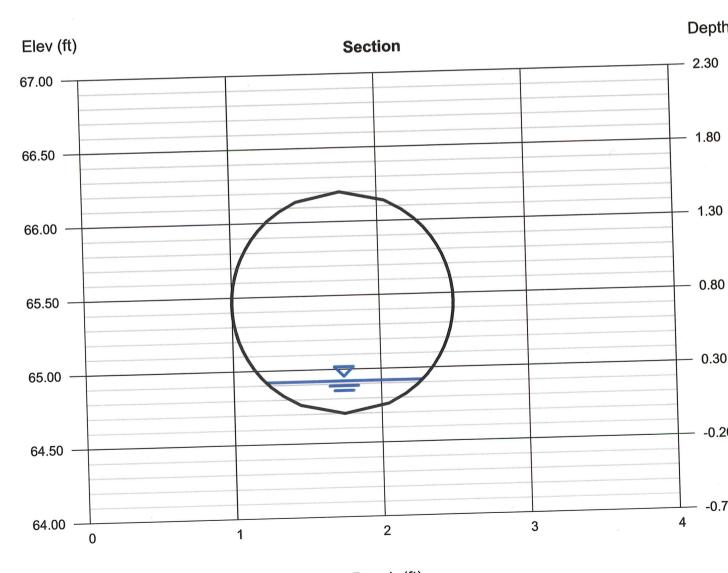
Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Wednesday, Jun 29 2016

POC D - Pipe Flow (Existing)

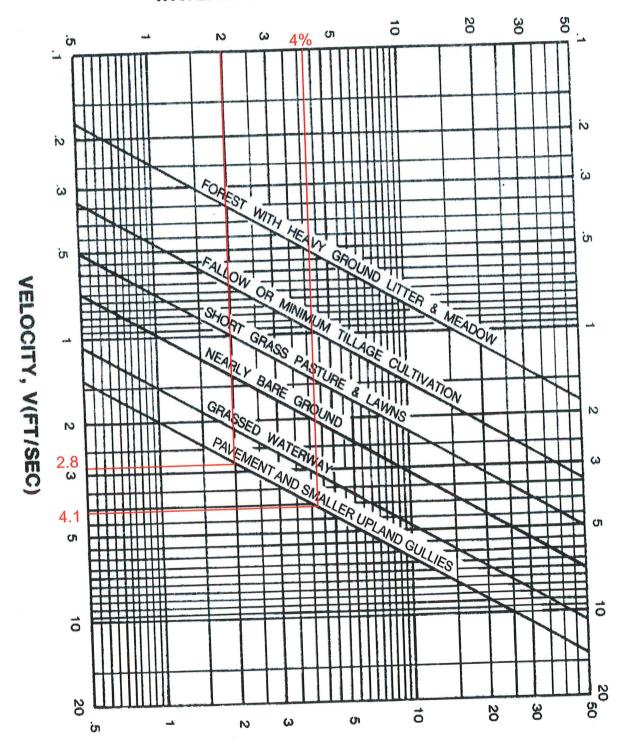
Circular Diameter (ft)	= 1.50	Highlighted Depth (ft) Q (cfs) Area (sqft)	= 0.22 = 0.760 = 0.16
Invert Elev (ft) Slope (%) N-Value	= 64.70 = 3.00 = 0.014	Velocity (ft/s) Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)	= 4.66 = 1.18 = 0.33 = 1.07 = 0.56
Calculations Compute by: Known Q (cfs)	Known Q = 0.76	EGL (III)	



Reach (ft)

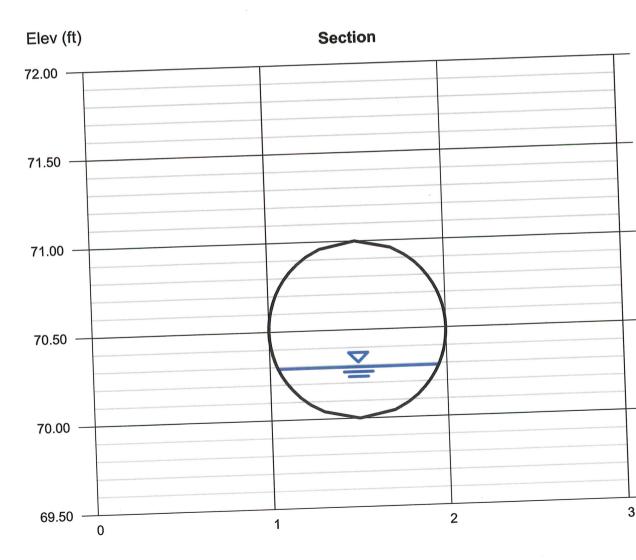
Figure 816.6

Velocities for Upland Method of Estimating Travel Time for Shallow Concentrated Flow WATERCOURSE SLOPE IN PERCENT



POC A - Pipe Flow (Proposed)

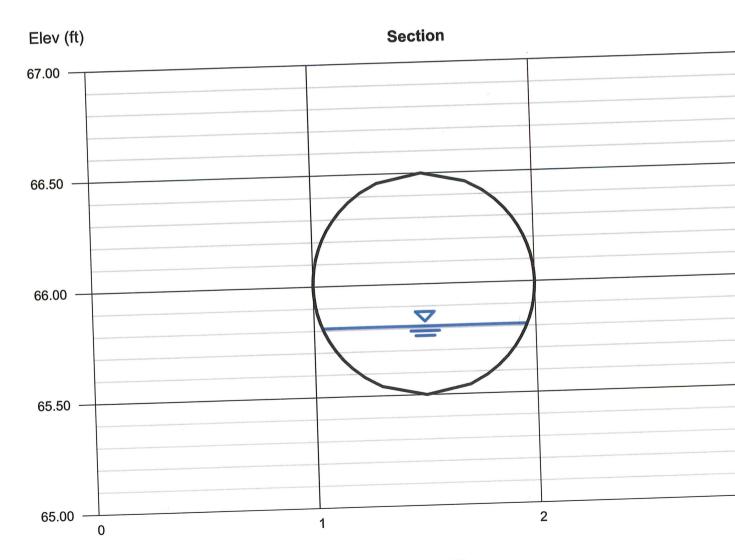
Circular Diameter (ft)	= 1.00	Highlighted Depth (ft) Q (cfs) Area (sqft)	= 0.29 = 1.540 = 0.19
Invert Elev (ft) Slope (%) N-Value	= 70.00 = 7.00 = 0.014	Velocity (ft/s) Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)	= 8.10 = 1.14 = 0.53 = 0.91 = 1.31
Calculations Compute by: Known Q (cfs)	Known Q = 1.54		



Reach (ft)

POC B - Pipe Flow (Proposed)

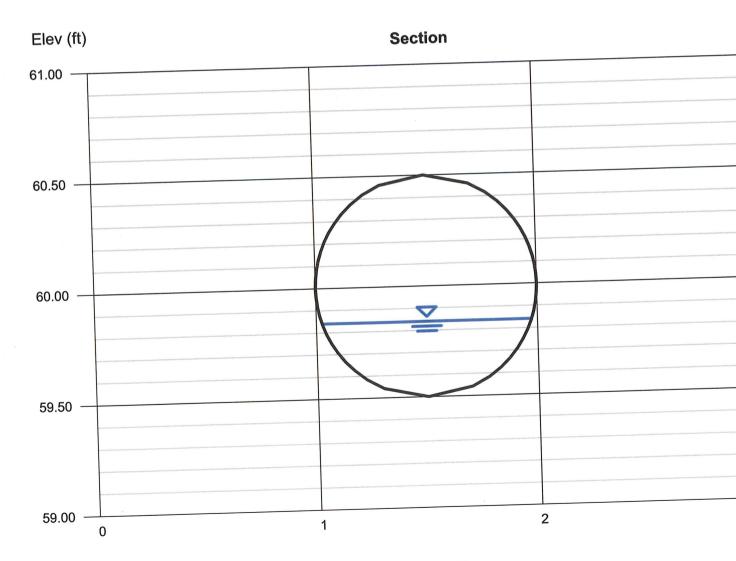
Circular Diameter (ft)	= 1.00	Highlighted Depth (ft) Q (cfs) Area (sqft)	= 0.31 = 1.850 = 0.21
Invert Elev (ft) Slope (%) N-Value	= 65.50 = 8.00 = 0.014	Velocity (ft/s) Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)	= 8.85 = 1.18 = 0.58 = 0.93 = 1.53
Calculations Compute by: Known Q (cfs)	Known Q = 1.85	LOL (IV)	



Reach (ft)

POC B' (New) - Pipe Flow (Proposed)

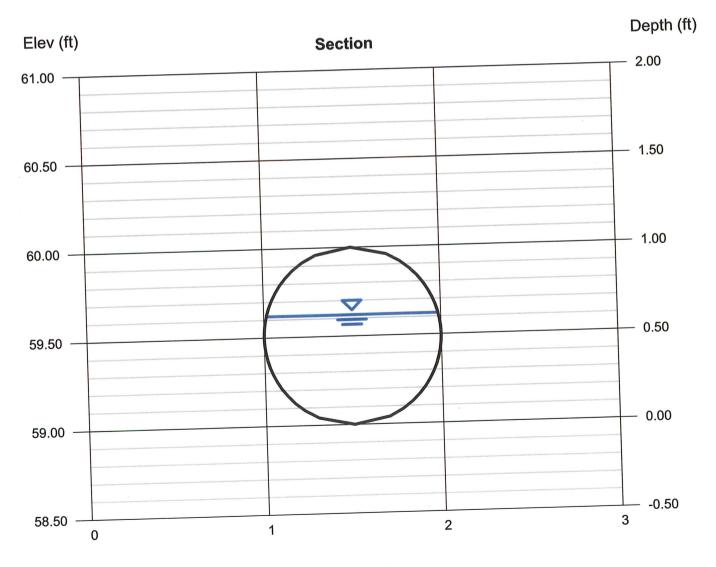
Circular Diameter (ft)	= 1.00	Highlighted Depth (ft) Q (cfs) Area (sqft)	= 0.34 = 3.120 = 0.24
Invert Elev (ft) Slope (%) N-Value	= 59.50 = 15.00 = 0.014	Velocity (ft/s) Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)	= 13.13 = 1.25 = 0.76 = 0.95 = 3.02
Calculations Compute by: Known Q (cfs)	Known Q = 3.12	LOE (II)	



Reach (ft)

POC C - Pipe Flow (Proposed)

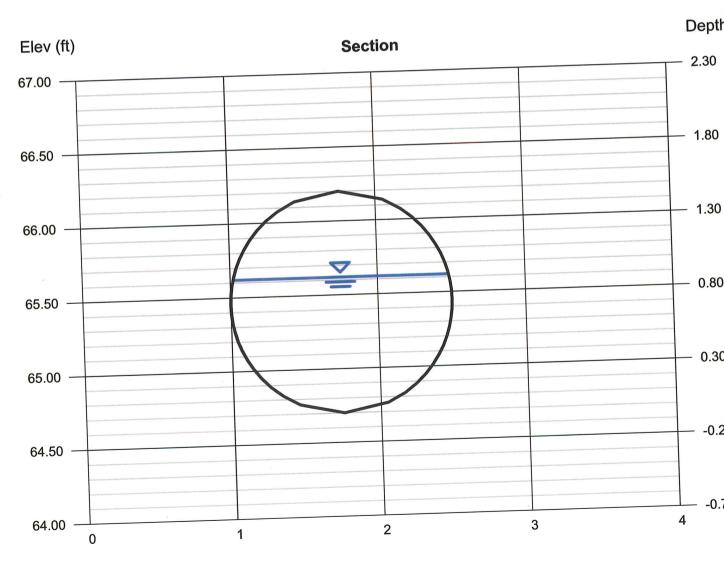
Circular Diameter (ft)	= 1.00	Highlighted Depth (ft) Q (cfs) Area (sqft)	= 0.62 = 5.200 = 0.51
Invert Elev (ft) Slope (%) N-Value	= 59.00 = 5.00 = 0.014	Velocity (ft/s) Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)	= 10.15 = 1.81 = 0.93 = 0.97 = 2.22
Calculations Compute by: Known Q (cfs)	Known Q = 5.20	LOL (II)	



Reach (ft)

POC D - Pipe Flow (Proposed)

Circular Diameter (ft)	= 1.50	Highlighted Depth (ft) Q (cfs) Area (sqft)	= 0.92 = 15.09 = 1.14
Invert Elev (ft) Slope (%) N-Value	= 64.70 = 5.00 = 0.014	Velocity (ft/s) Wetted Perim (ft) Crit Depth, Yc (ft) Top Width (ft) EGL (ft)	= 13.27 = 2.70 = 1.41 = 1.46 = 3.66
Calculations Compute by: Known Q (cfs)	Known Q = 15.09		



Reach (ft)

Appendix 6.3 – Hydrograph Model Output

Hydraflow Table of Contents 45500\Calculations_and_Spreadsheets\Hydrology\Hydrographs\Northgate Walk.gpw

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

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		. 33
	IDF Report	

I. Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)		Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
	9.029	1	12	9,751				POC A - Existing
Rational	5.277	1	11	5,224				POC B - Existing
Rational	0.865	1	10	779				POC C - Existing
Rational	2.195	1	9	1,778				POC D - Existing
Rational	3.362	1	6	1,815				POC Channel - Existing
Rational	18.36	1	12	19,348	1, 2, 3,			Discharge to Channel - Existing
Combine Rational	1.176	1	14	1,482	4, 5			POC E - Existing
Rational				504				POC A - Proposed
9 Rational	1.081	1	6	584				POC B - Proposed
10 Rational	1.431	1	15	1,932				POC B' (New) - Proposed
11 Rational	2.116	1	9	1,714				POC C - Proposed
12 Rational	3.867	1	11	3,828				POC D - Proposed
13 Rational	8.422	1	13	9,853				POC Channel - Proposed
14 Rational	3.501	1	10	3,151				Discharge to Channel - Proposed
15 Combine	18.25	1	13	21,061 1,266	9, 10, 11 12, 13, 1	4		POC E - Proposed

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Hyd. No. 1

POC A - Existing

= Rational Hydrograph type = 25 yrsStorm frequency = 1 min Time interval = 3.870 acDrainage area Intensity

IDF Curve

= 2.621 in/hr

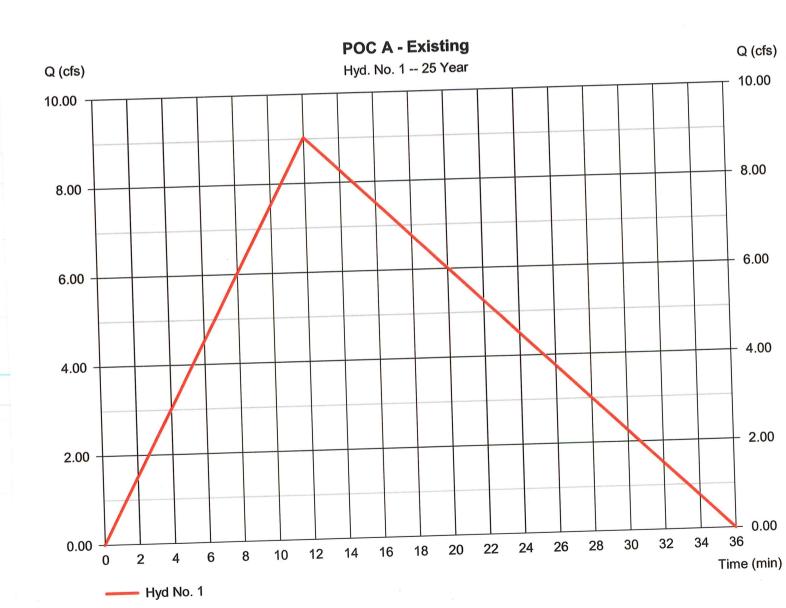
= Northgate Walk.IDF

= 9.029 cfsPeak discharge = 12 min Time to peak = 9,751 cuft Hyd. volume = 0.89

Runoff coeff.

= 12.00 min Tc by User

= 1/2Asc/Rec limb fact



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Friday, 07 / 1 / 2016

Hyd. No. 2

POC B - Existing

Hydrograph type = 25 yrsStorm frequency = 1 min Time interval = 2.220 acDrainage area = 2.732 in/hrIntensity

IDF Curve

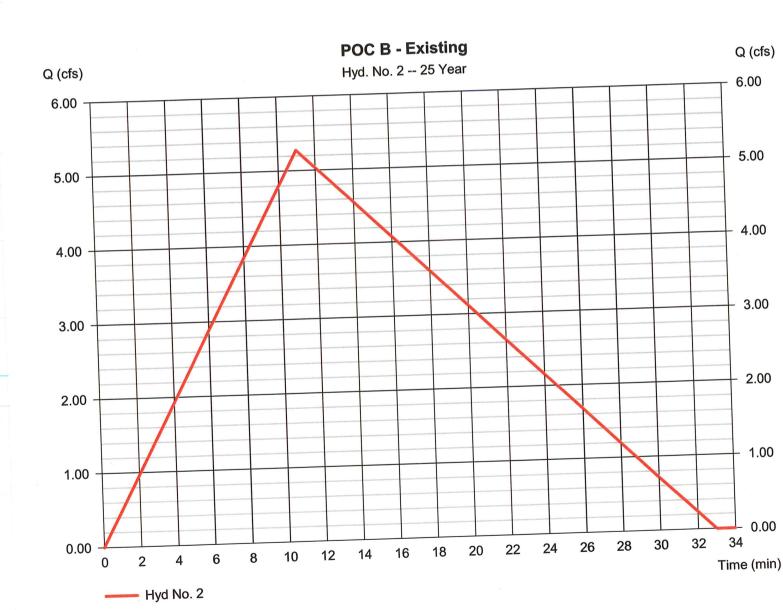
= Rational

= Northgate Walk.IDF

= 5.277 cfsPeak discharge = 11 min Time to peak = 5,224 cuftHvd. volume = 0.87Runoff coeff.

= 11.00 min Tc by User

Asc/Rec limb fact = 1/2



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Hyd. No. 3

POC C - Existing

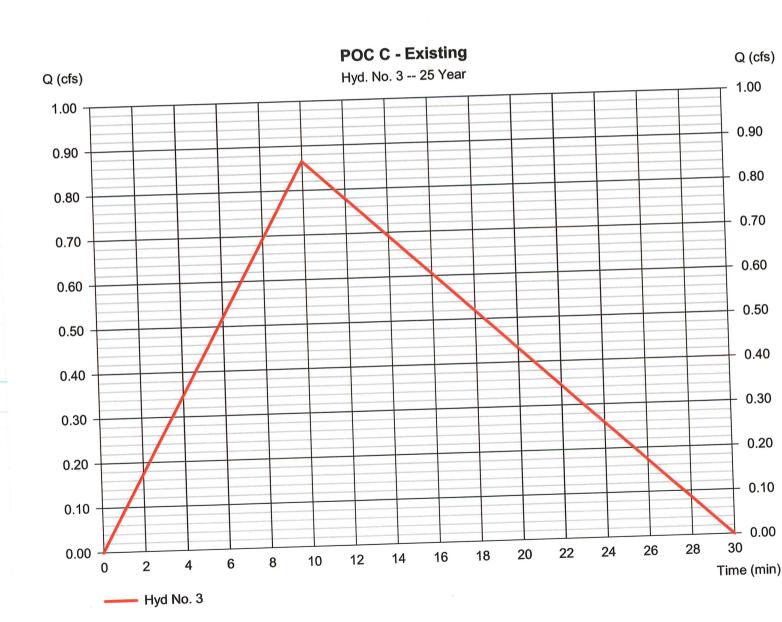
= Rational Hydrograph type = 25 yrsStorm frequency = 1 min Time interval = 0.340 acDrainage area = 2.859 in/hrIntensity

IDF Curve

= Northgate Walk.IDF

= 0.865 cfsPeak discharge = 10 min Time to peak = 779 cuft Hyd. volume = 0.89Runoff coeff. $= 10.00 \, \text{min}$ Tc by User

Asc/Rec limb fact = 1/2



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Hyd. No. 4

POC D - Existing

Hydrograph type Storm frequency = 25 yrs= 1 min Time interval = 0.830 acDrainage area

Intensity **IDF** Curve = Rational

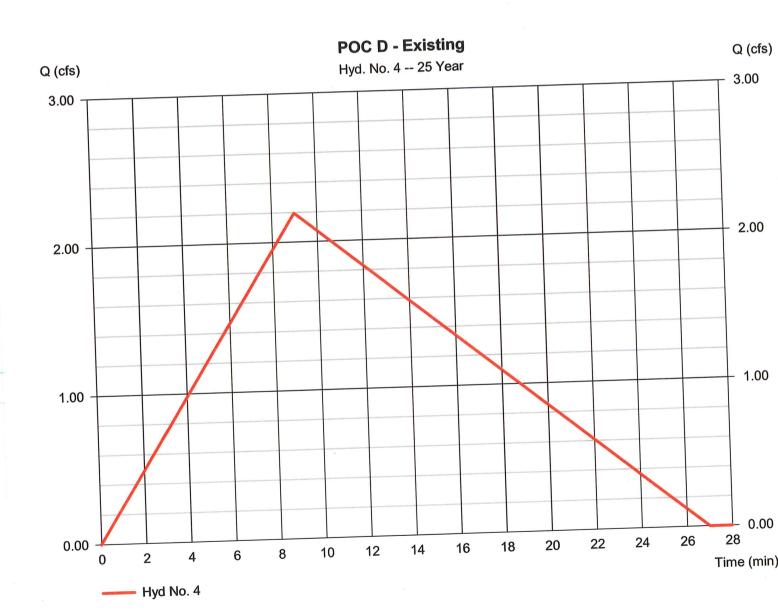
= 3.005 in/hr

= Northgate Walk.IDF

= 2.195 cfsPeak discharge = 9 min Time to peak = 1,778 cuftHyd. volume = 0.88Runoff coeff.

 $= 9.00 \, \text{min}$ Tc by User

Asc/Rec limb fact = 1/2



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Hyd. No. 5

POC Channel - Existing

= Rational Hydrograph type Storm frequency = 25 yrs= 1 min Time interval = 1.320 acDrainage area Intensity

IDF Curve

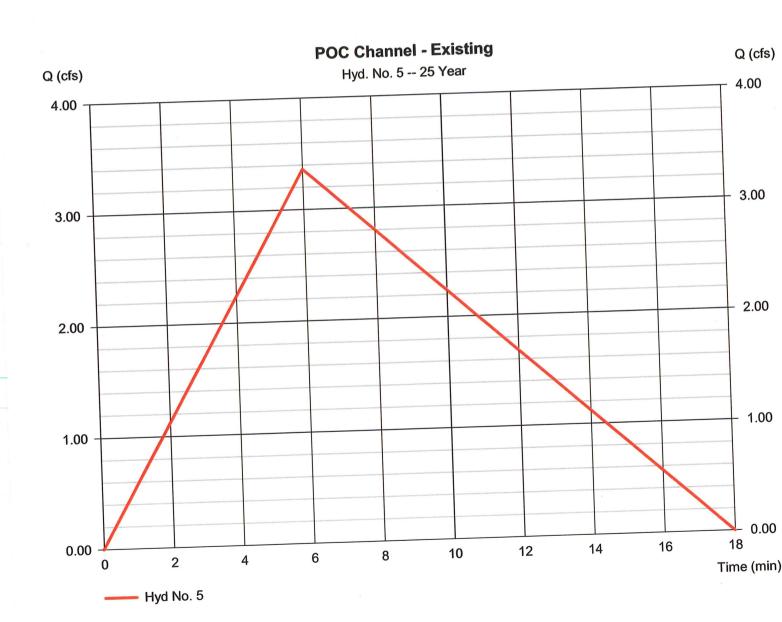
= 3.638 in/hr

= Northgate Walk.IDF

= 3.362 cfsPeak discharge = 6 minTime to peak = 1,815 cuft Hvd. volume

= 0.7Runoff coeff. $= 6.00 \, \text{min}$ Tc by User

= 1/2Asc/Rec limb fact



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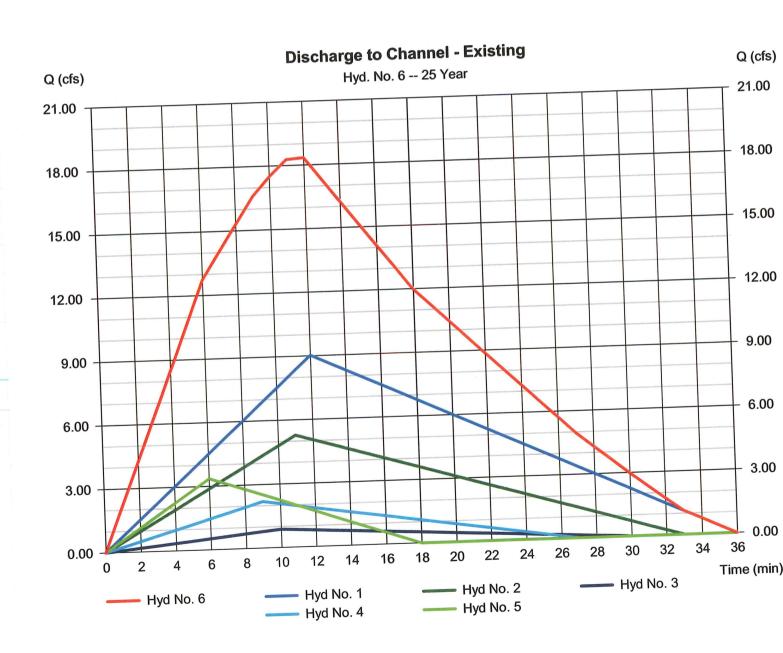
Friday, 07 / 1 / 2016

Hyd. No. 6

Discharge to Channel - Existing

Hydrograph type = Combine
Storm frequency = 25 yrs
Time interval = 1 min
Inflow hyds. = 1, 2, 3, 4, 5

Peak discharge = 18.36 cfs
Time to peak = 12 min
Hyd. volume = 19,348 cuft
Contrib. drain. area = 8.580 ac



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Hyd. No. 7

POC E - Existing

Hydrograph type Storm frequency Time interval

Drainage area

= Rational = 25 yrs

= 1 min = 0.690 ac= 2.436 in/hr

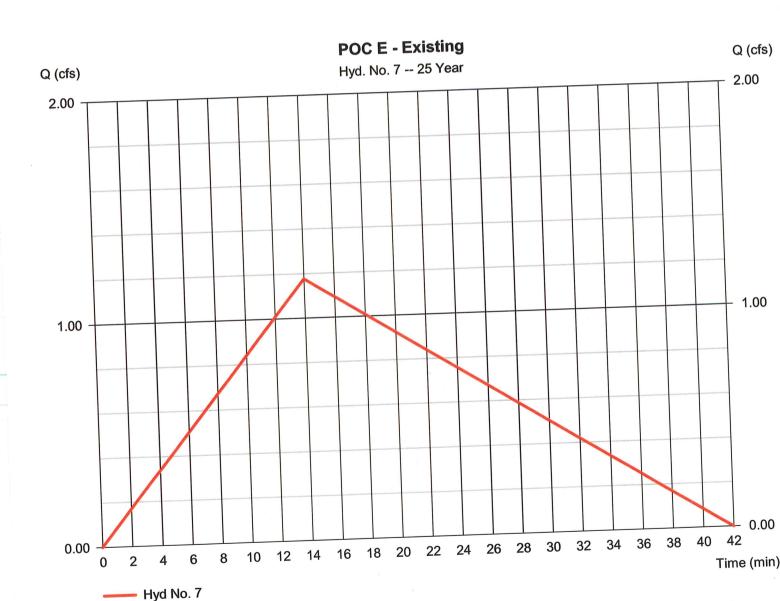
Intensity = Northgate Walk.IDF **IDF** Curve

= 1.176 cfsPeak discharge = 14 min Time to peak = 1,482 cuft

Hyd. volume Runoff coeff.

= 0.7 $= 14.00 \, \text{min}$ Tc by User

= 1/2Asc/Rec limb fact



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Friday, 07 / 1 / 2016

Hyd. No. 9

POC A - Proposed

Hydrograph type Storm frequency Time interval

= 25 yrs= 1 min = 0.330 acDrainage area = 3.638 in/hrIntensity

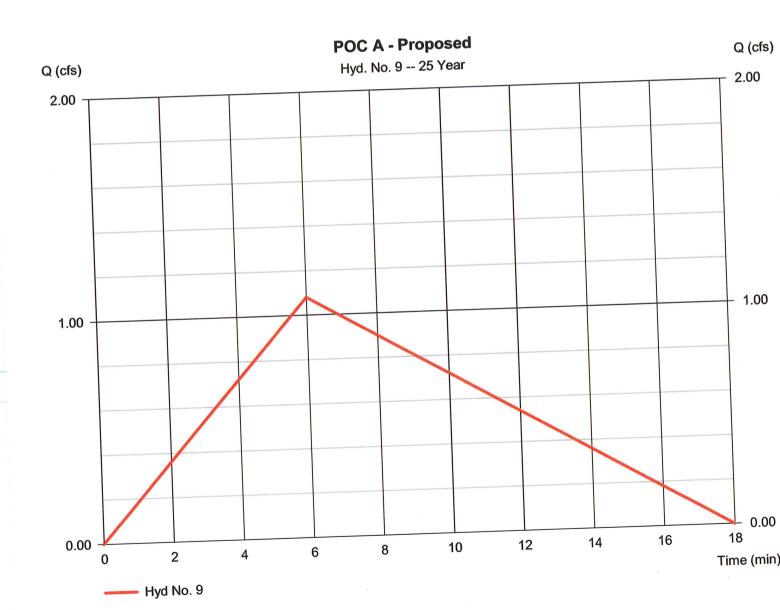
IDF Curve

= Rational

= Northgate Walk.IDF

= 1.081 cfsPeak discharge = 6 min Time to peak = 584 cuft Hvd. volume = 0.9Runoff coeff. $= 6.00 \, \text{min}$

Tc by User Asc/Rec limb fact = 1/2



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Friday, 07 / 1 / 2016

Hyd. No. 10

POC B - Proposed

= Rational Hydrograph type = 25 yrsStorm frequency = 1 min Time interval = 0.690 acDrainage area = 2.357 in/hr

Intensity **IDF** Curve

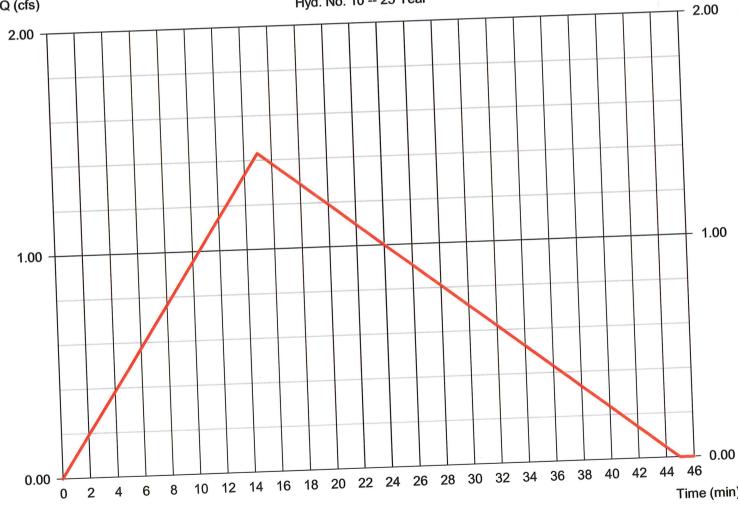
= Northgate Walk.IDF

= 1.431 cfsPeak discharge = 15 min Time to peak = 1,932 cuftHyd. volume = 0.88Runoff coeff.

= 15.00 min Tc by User = 1/2

Asc/Rec limb fact

POC B - Proposed Q (cfs) Hyd. No. 10 -- 25 Year Q (cfs) 2.00 2.00



Hyd No. 10

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Hyd. No. 11

POC B' (New) - Proposed

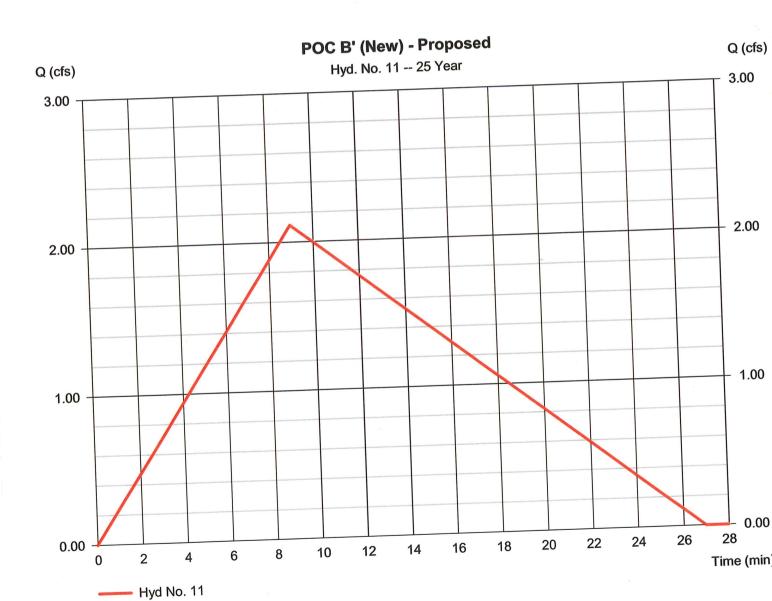
= Rational Hydrograph type = 25 yrsStorm frequency = 1 min Time interval = 0.800 acDrainage area = 3.005 in/hrIntensity

IDF Curve

= Northgate Walk.IDF

= 2.116 cfsPeak discharge = 9 min Time to peak = 1,714 cuft Hyd. volume = 0.88Runoff coeff. $= 9.00 \, \text{min}$

Tc by User Asc/Rec limb fact = 1/2



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Hyd. No. 12

POC C - Proposed

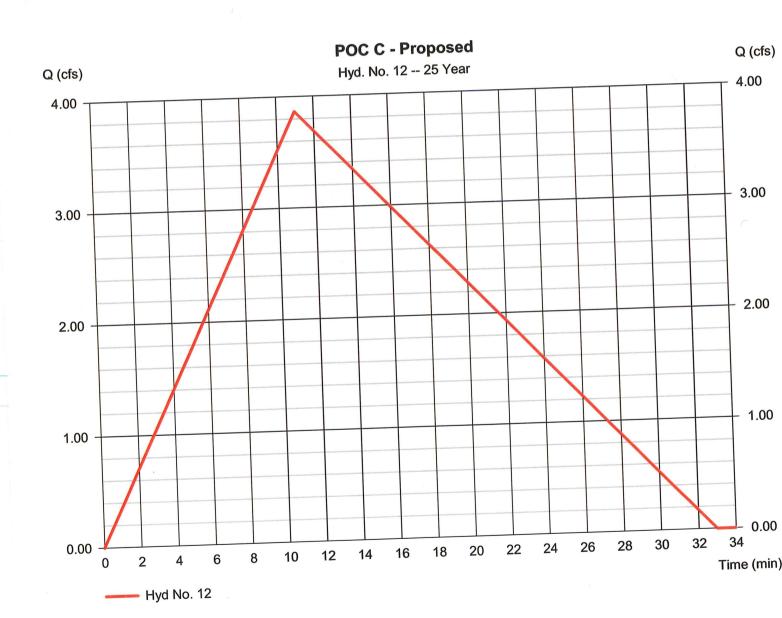
= Rational Hydrograph type Storm frequency Time interval Drainage area

Intensity **IDF** Curve = 25 yrs= 1 min = 1.590 ac= 2.732 in/hr

= Northgate Walk.IDF

= 3.867 cfsPeak discharge = 11 min Time to peak = 3,828 cuftHvd. volume = 0.89

Runoff coeff. $= 11.00 \, \text{min}$ Tc by User



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Hyd. No. 13

POC D - Proposed

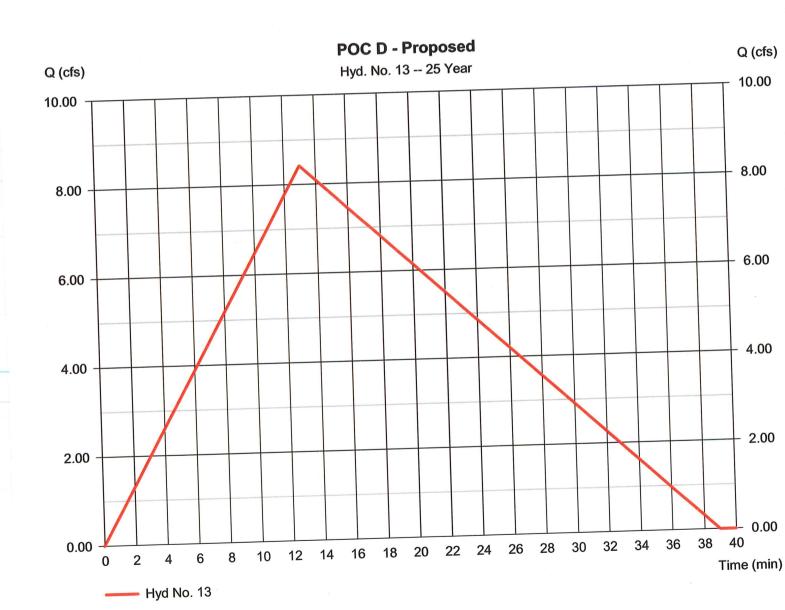
Hydrograph type = Rational
Storm frequency = 25 yrs
Time interval = 1 min
Drainage area = 3.750 ac
Intensity = 2.523 in/hr

IDF Curve = Northgate Walk.IDF

Peak discharge = 8.422 cfs
Time to peak = 13 min
Hyd. volume = 9,853 cuft

Runoff coeff. = 0.89

Tc by User = 13.00 min



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Friday, 07 / 1 / 2016

Hyd. No. 14

POC Channel - Proposed

Hydrograph type = Rational = 25 yrs
Time interval = 1 min

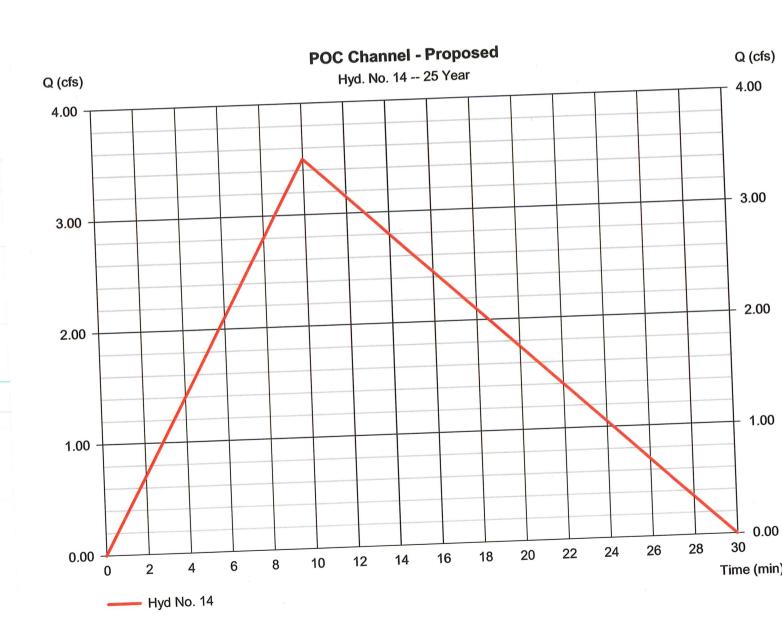
Drainage area
Intensity
IDF Curve

= 1 min = 1.570 ac = 2.859 in/hr

= Northgate Walk.IDF

Peak discharge = 3.501 cfs
Time to peak = 10 min
Hyd. volume = 3,151 cuft

Runoff coeff. = 0.78 Tc by User = 10.00 min



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Friday, 07 / 1 / 2016

Hyd. No. 15

Discharge to Channel - Proposed

Hydrograph type Storm frequency = Combine

Time interval Inflow hyds.

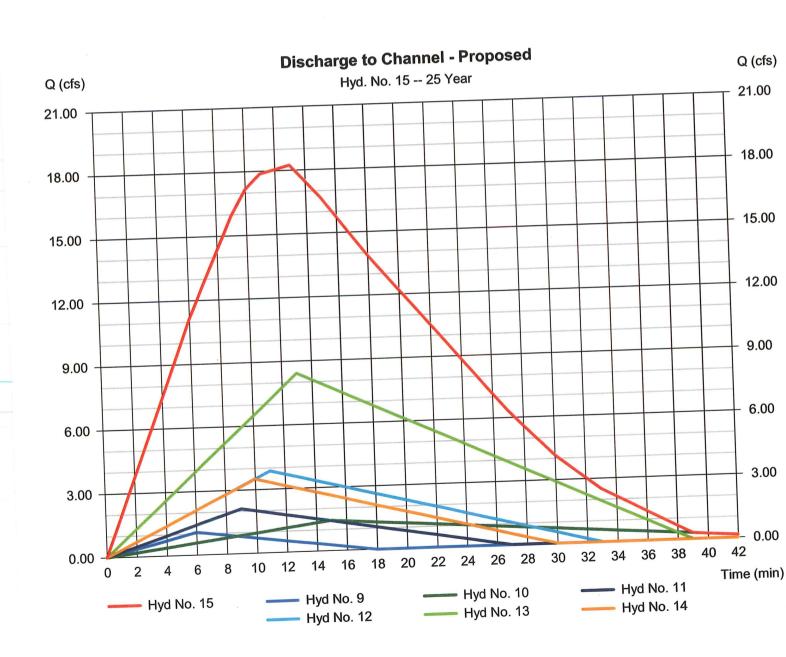
= 25 yrs = 1 min

= 9, 10, 11, 12, 13, 14

= 18.25 cfsPeak discharge = 13 min Time to peak

= 21,061 cuftHyd. volume = 8.730 ac

Contrib. drain. area



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Friday, 07 / 1 / 2016

Hyd. No. 16

POC E - Proposed

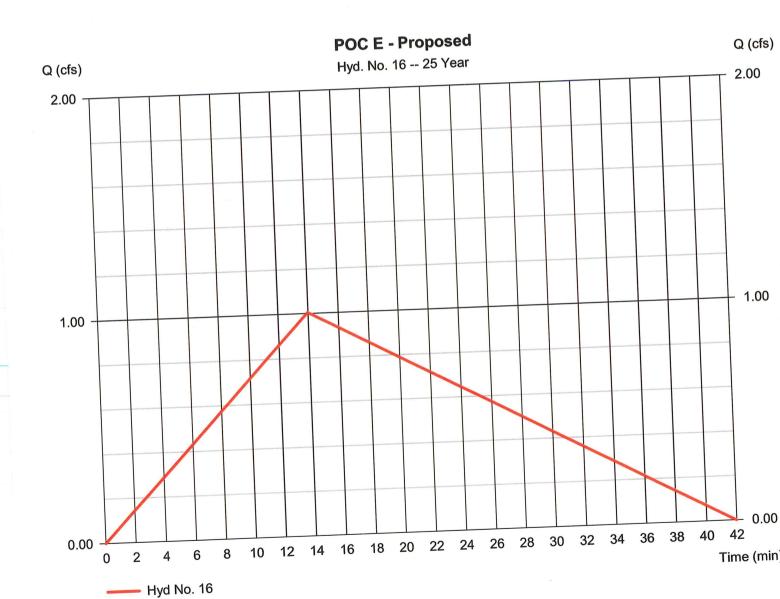
Hydrograph type = Rational
Storm frequency = 25 yrs
Time interval = 1 min
Drainage area = 0.550 ac
Intensity = 2.436 in/hr

Intensity = 2.436 II/III = Northgate Walk.IDF

Peak discharge = 1.005 cfs
Time to peak = 14 min
Hyd. volume = 1,266 cuft
Runoff coeff. = 0.75

Tc by User = 14.00 min

Aso/Rec limb fact = 1/2



drograph type origin)	Peak flow	Time interval	Time to Peak (min)		Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
	24	4	12	12,760				POC A - Existing
ational			1					POC B - Existing
ational								POC C - Existing
ational								POC D - Existing
tational								POC Channel - Existing
Rational					1, 2, 3,			Discharge to Channel - Existing
Combine	24.01				4, 5			POC E - Existing
Rational	1.539	1	14	1,940				POC A - Proposed
Dational	1 412	1	6	762				
			15	2,528				POC B - Proposed
			9	2,242				POC B' (New) - Proposed
			11	5,008				POC C - Proposed
			1	12,893				POC D - Proposed
				,				POC Channel - Proposed
					9, 10, 1	',		Discharge to Channel - Proposed
Combine					12, 13,	14		POC E - Proposed
	drograph type origin) ational ational ational ational	drograph type origin) ational 11.81 ational 6.905 ational 2.871 ational 4.392 ational 1.539 Rational 1.412 Rational 2.768 Rational 5.059 Rational 1.02 Rational 4.580 Combine 23.88	drograph type origin) Peak flow (cfs) Time interval (min) ational 11.81 1 ational 6.905 1 ational 1.132 1 ational 2.871 1 ational 4.392 1 combine 24.01 1 Rational 1.539 1 Rational 1.873 1 Rational 2.768 1 Rational 5.059 1 Rational 11.02 1 Rational 4.580 1 Combine 23.88 1	drograph type Peak flow (cfs) Time interval (min) Time to Peak (min) ational 11.81 1 12 ational 6.905 1 11 ational 1.132 1 10 ational 2.871 1 9 ational 4.392 1 6 combine 24.01 1 12 cational 1.539 1 14 Rational 1.873 1 15 Rational 2.768 1 9 Rational 5.059 1 11 Rational 11.02 1 13 Rational 4.580 1 10 Combine 23.88 1 13	drograph type origin) Peak flow (cfs) Time interval (min) Time to Peak (min) Hyd. volume (cuft) ational 11.81 1 12 12,760 ational 6.905 1 11 6,836 ational 1.132 1 10 1,019 ational 2.871 1 9 2,326 ational 4.392 1 6 2,372 combine 24.01 1 12 25,311 combine 1.539 1 14 1,940 Rational 1.873 1 15 2,528 Rational 2.768 1 9 2,242 Rational 5.059 1 11 5,008 Rational 11.02 1 13 12,893 Rational 4.580 1 10 4,122 Combine 23.88 1 13 27,556	drograph type origin) Peak flow (cfs) Time interval (min) Time to Peak (min) Hyd. volume (cuft) Inflow hyd(s) ational 11.81 1 12 12,760	drograph type origin) Peak flow (cfs) Time interval (min) Time to Peak (min) Hyd. volume (cuft) Inflow hyd(s) Maximum elevation (ft) ational 11.81 1 12 12,760	drograph type origin) Peak flow (cfs) Time interval (min) Time to Peak (min) Hyd. volume (cuft) Inflow hyd(s) elevation strge used (cuft) ational 11.81 1 12 12,760

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Friday, 07 / 1 / 2016

Hyd. No. 1

POC A - Existing

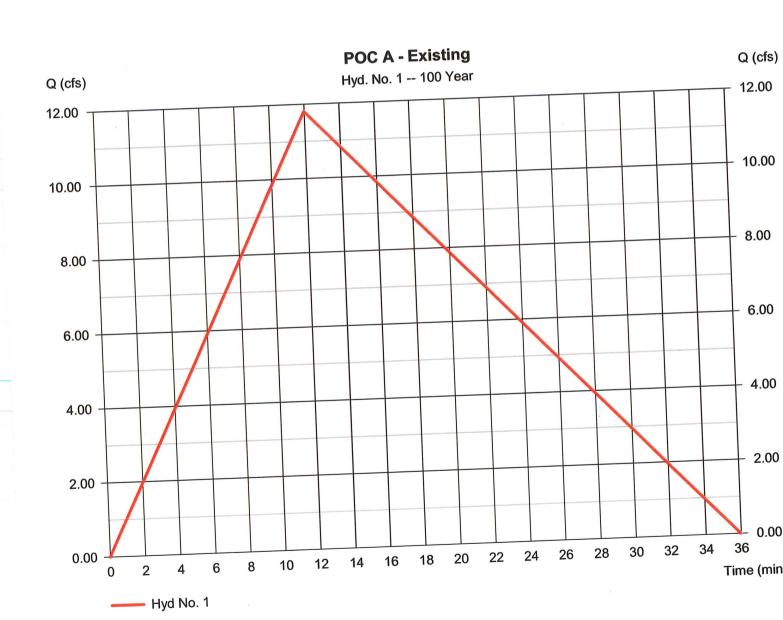
= Rational Hydrograph type = 100 yrsStorm frequency = 1 minTime interval = 3.870 acDrainage area

Intensity **IDF** Curve = 3.430 in/hr

= Northgate Walk.IDF

= 11.81 cfsPeak discharge = 12 min Time to peak = 12,760 cuftHyd. volume

= 0.89Runoff coeff. = 12.00 min Tc by User



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Hyd. No. 2

POC B - Existing

= Rational Hydrograph type = 100 yrsStorm frequency = 1 min Time interval Drainage area = 3.575 in/hrIntensity

IDF Curve

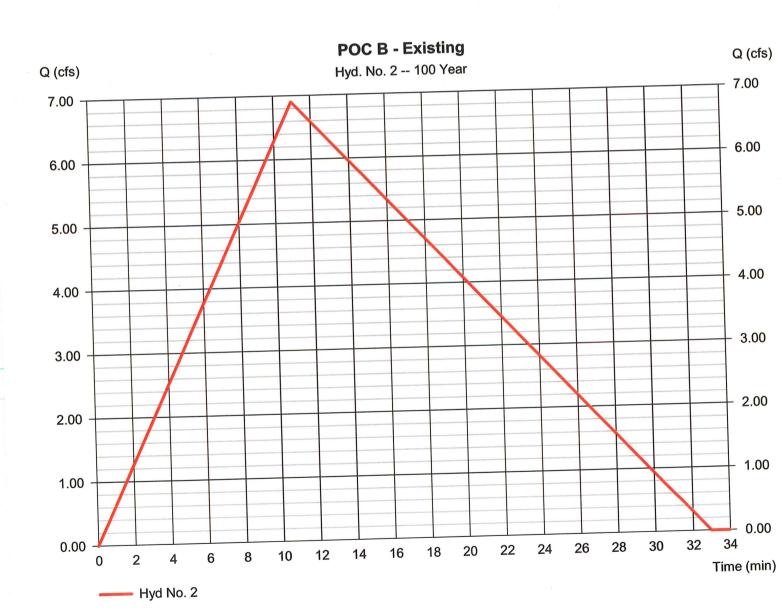
= 2.220 ac

= Northgate Walk.IDF

= 6.905 cfsPeak discharge = 11 min Time to peak = 6,836 cuft Hyd. volume

= 0.87Runoff coeff.

 $= 11.00 \, \text{min}$ Tc by User



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Hyd. No. 3

POC C - Existing

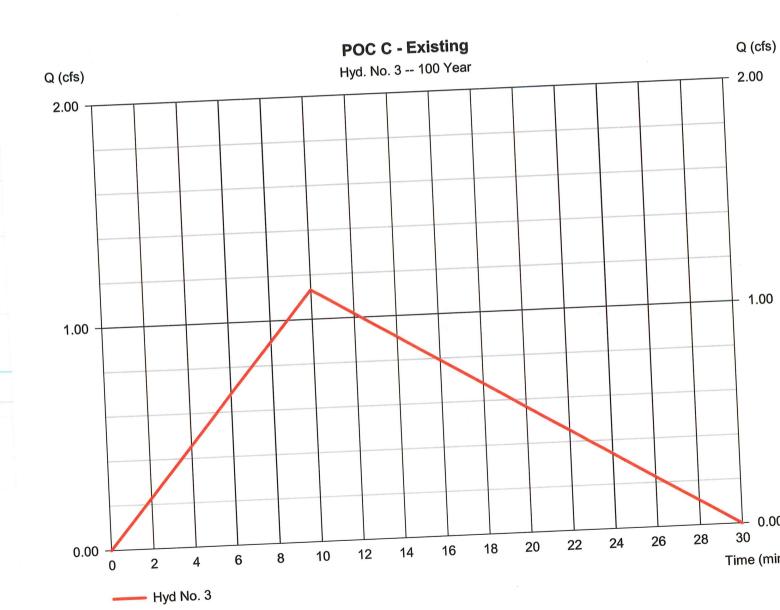
= Rational Hydrograph type = 100 yrsStorm frequency = 1 min Time interval = 0.340 acDrainage area = 3.740 in/hr

Intensity

= Northgate Walk.IDF **IDF** Curve

= 1.132 cfsPeak discharge = 10 min Time to peak = 1,019 cuftHyd. volume = 0.89Runoff coeff.

 $= 10.00 \, \text{min}$ Tc by User = 1/2Asc/Rec limb fact



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Friday, 07 / 1 / 2016

Hyd. No. 4

POC D - Existing

= Rational Hydrograph type = 100 yrsStorm frequency = 1 min Time interval = 0.830 acDrainage area Intensity

IDF Curve

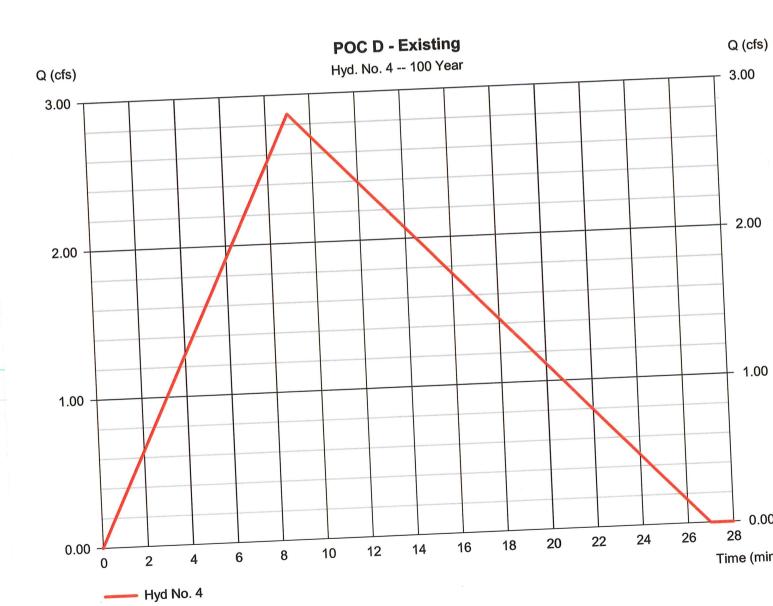
= 3.931 in/hr

= Northgate Walk.IDF

= 2.871 cfsPeak discharge = 9 min Time to peak = 2,326 cuft Hyd. volume = 0.88Runoff coeff. $= 9.00 \, \text{min}$

Tc by User Asc/Rec limb fact

= 1/2



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Hyd. No. 5

POC Channel - Existing

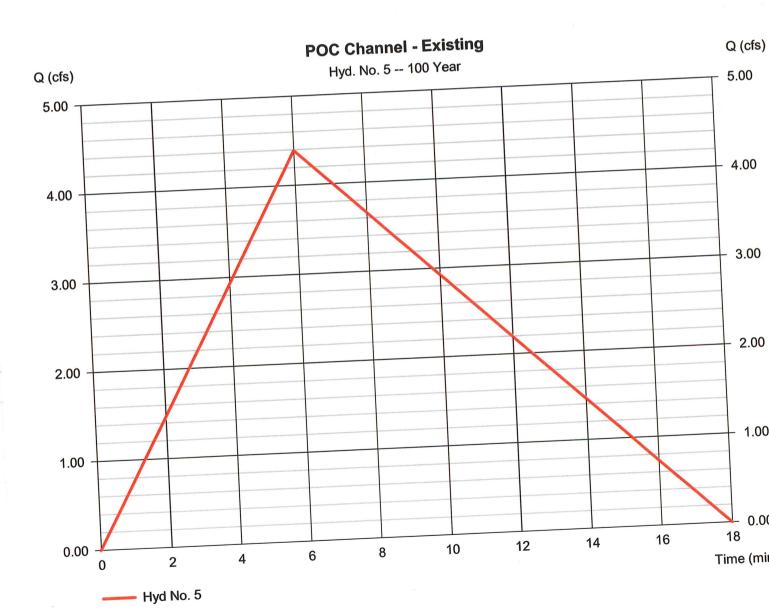
= Rational Hydrograph type = 100 yrsStorm frequency = 1 minTime interval = 1.320 acDrainage area = 4.753 in/hr Intensity

IDF Curve

= Northgate Walk.IDF

= 4.392 cfsPeak discharge = 6 minTime to peak = 2,372 cuftHyd. volume = 0.7

Runoff coeff. $= 6.00 \, \text{min}$ Tc by User



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Hyd. No. 6

Discharge to Channel - Existing

Hydrograph type Storm frequency Time interval

Inflow hyds.

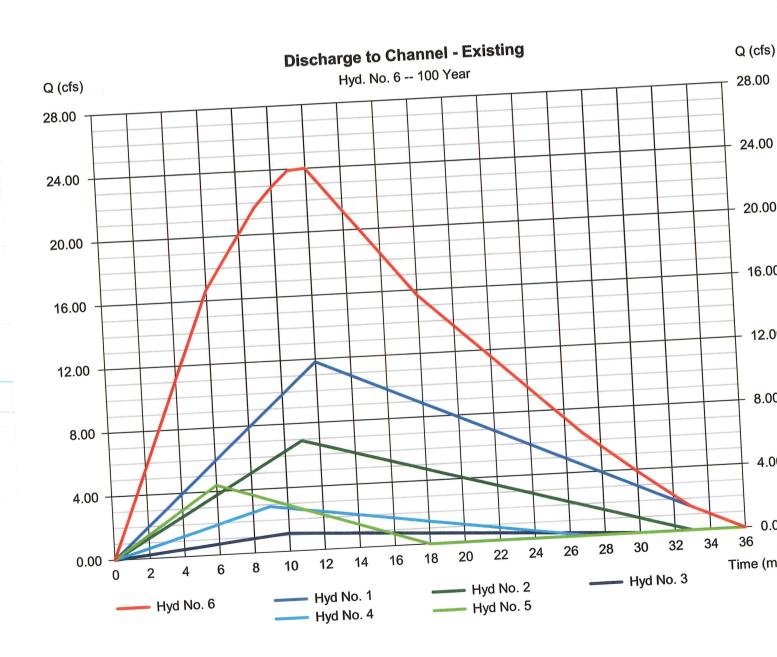
= Combine = 100 yrs

= 1 min

= 1, 2, 3, 4, 5

= 24.01 cfsPeak discharge = 12 min Time to peak = 25,311 cuftHyd. volume

= 8.580 ac Contrib. drain. area



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Hyd. No. 7

POC E - Existing

Hydrograph type Storm frequency Time interval

Drainage area

= Rational = 100 yrs

= 100 yrs = 1 min

= 0.690 ac = 3.187 in/hr

Intensity IDF Curve

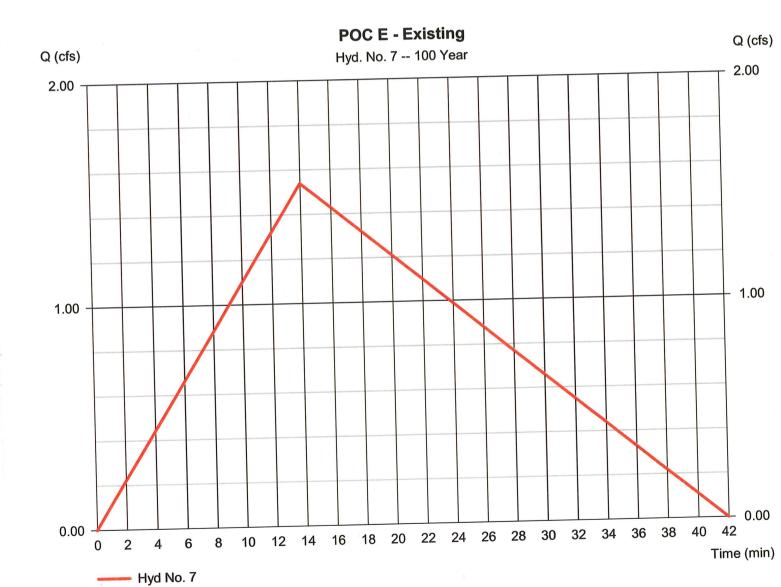
= Northgate Walk.IDF

Peak discharge = Time to peak =

= 1.539 cfs = 14 min = 1,940 cuft

Hyd. volume = 1.9^4 Runoff coeff. = 0.7

Tc by User = 14.00 min



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Hyd. No. 9

POC A - Proposed

= Rational Hydrograph type = 100 yrsStorm frequency = 1 min Time interval Drainage area = 4.753 in/hrIntensity

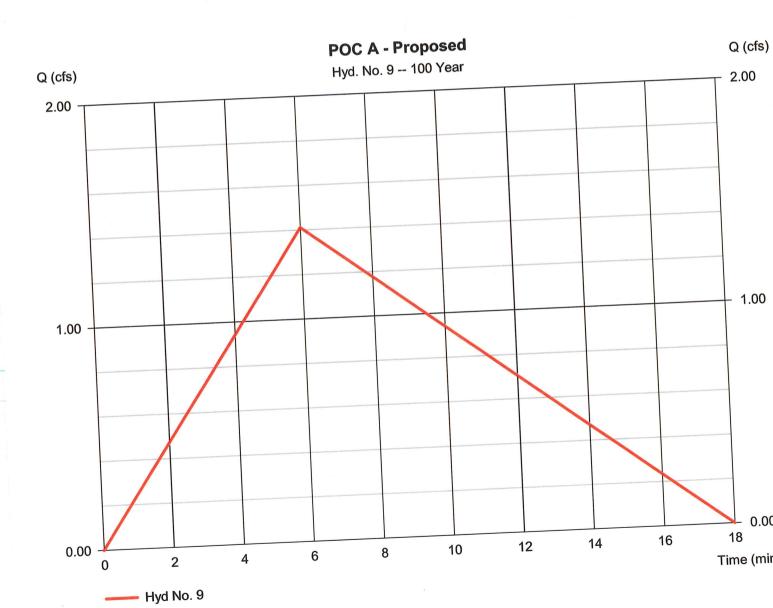
IDF Curve

= 0.330 ac

= Northgate Walk.IDF

= 1.412 cfsPeak discharge = 6 min Time to peak = 762 cuft Hyd. volume = 0.9Runoff coeff. = 6.00 min

Tc by User = 1/2Asc/Rec limb fact



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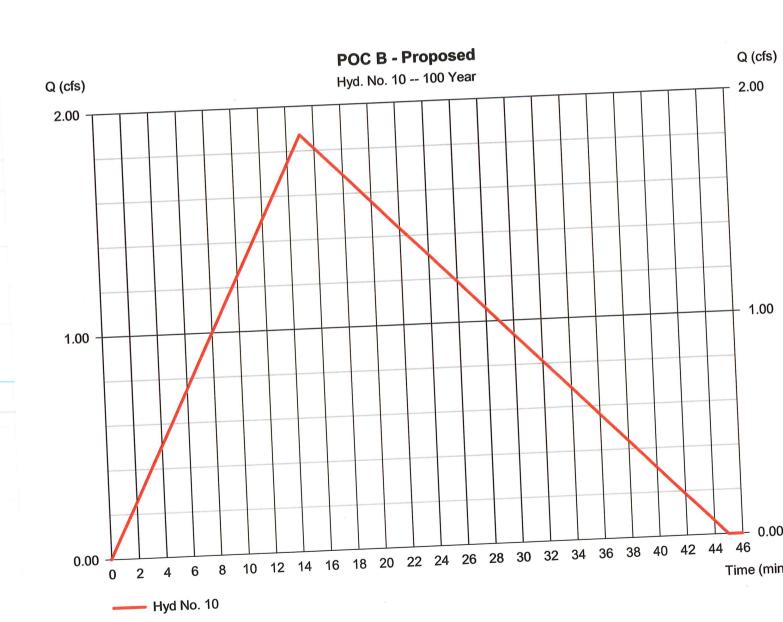
Hyd. No. 10

POC B - Proposed

IDF Curve = Northgate Walk.IDF

Peak discharge = 1.873 cfs
Time to peak = 15 min
Hyd. volume = 2,528 cuft
Runoff coeff. = 0.88

Tc by User = 15.00 min



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= 2.768 cfs

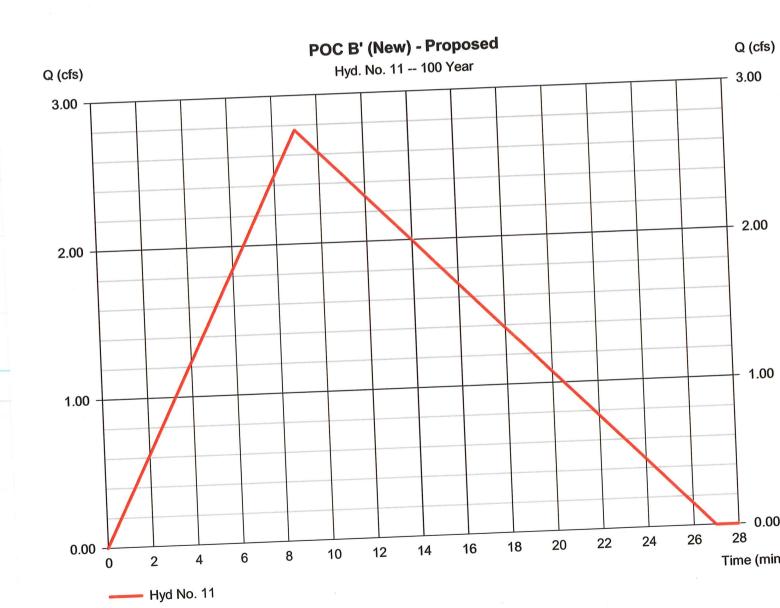
Hyd. No. 11

POC B' (New) - Proposed

= Rational Hydrograph type = 100 yrsStorm frequency = 1 minTime interval = 0.800 acDrainage area = 3.931 in/hr

Intensity = Northgate Walk.IDF **IDF** Curve

Peak discharge = 9 min Time to peak = 2,242 cuft Hyd. volume = 0.88Runoff coeff. $= 9.00 \, \text{min}$ Tc by User



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Hyd. No. 12

POC C - Proposed

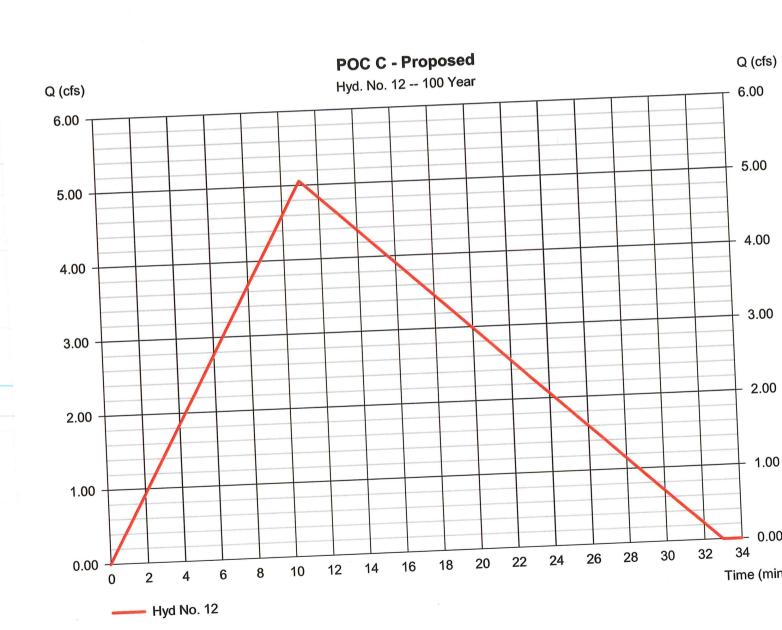
= Rational Hydrograph type = 100 yrsStorm frequency = 1 min Time interval = 1.590 acDrainage area = 3.575 in/hr

Intensity **IDF** Curve

Northgate Walk.IDF

= 5.059 cfsPeak discharge = 11 min Time to peak = 5,008 cuftHyd. volume = 0.89

Runoff coeff. $= 11.00 \, \text{min}$ Tc by User



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Hyd. No. 13

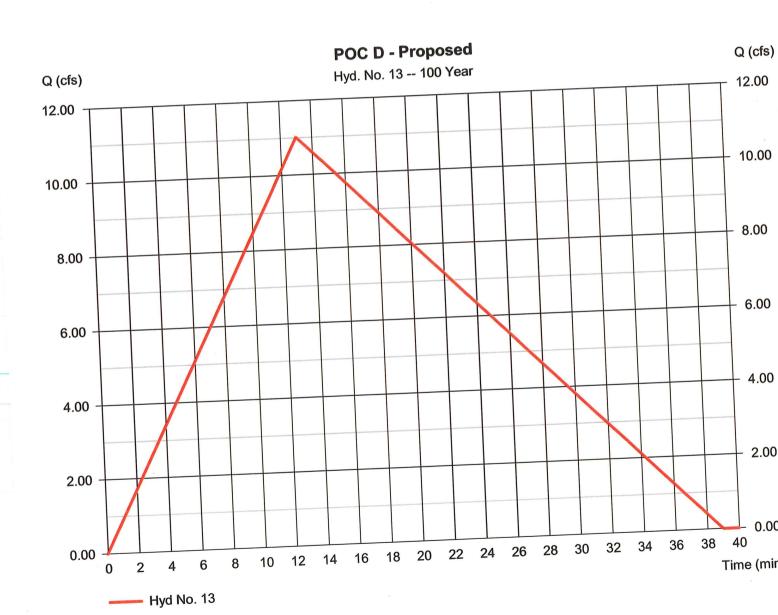
POC D - Proposed

IDF Curve

= 3.302 in/nr = Northgate Walk.IDF Peak discharge = 11.02 cfs Time to peak = 13 min Hyd. volume = 12,893 cuft

Runoff coeff. = 0.89

Tc by User = 13.00 min



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Hyd. No. 14

POC Channel - Proposed

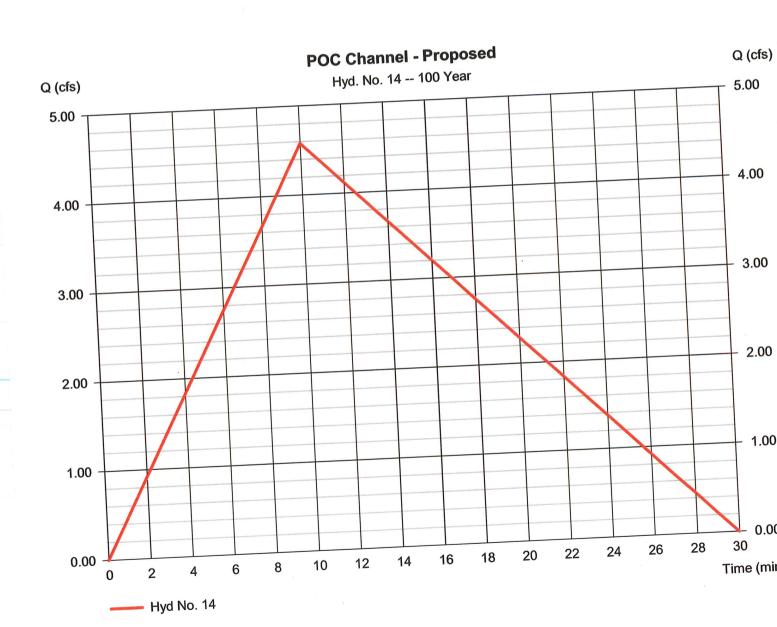
= Rational Hydrograph type = 100 yrsStorm frequency = 1 min Time interval = 1.570 acDrainage area = 3.740 in/hrIntensity

IDF Curve

= Northgate Walk.IDF

= 4.580 cfsPeak discharge = 10 min Time to peak = 4,122 cuftHyd. volume

= 0.78Runoff coeff. $= 10.00 \, \text{min}$ Tc by User



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Hyd. No. 15

Discharge to Channel - Proposed

Hydrograph type Storm frequency Time interval

= Combine = 100 yrs

= 1 min

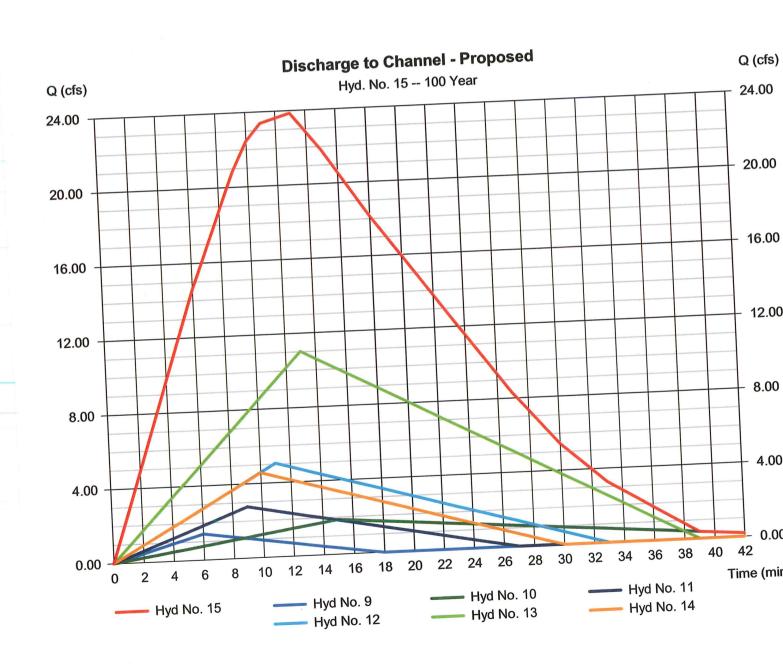
Inflow hyds.

= 9, 10, 11, 12, 13, 14

= 23.88 cfsPeak discharge = 13 min Time to peak = 27,556 cuft

Hyd. volume = 8.730 ac

Contrib. drain. area



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Hyd. No. 16

POC E - Proposed

Hydrograph type Storm frequency Time interval

Drainage area

Intensity

IDF Curve

= Rational = 100 yrs= 1 min

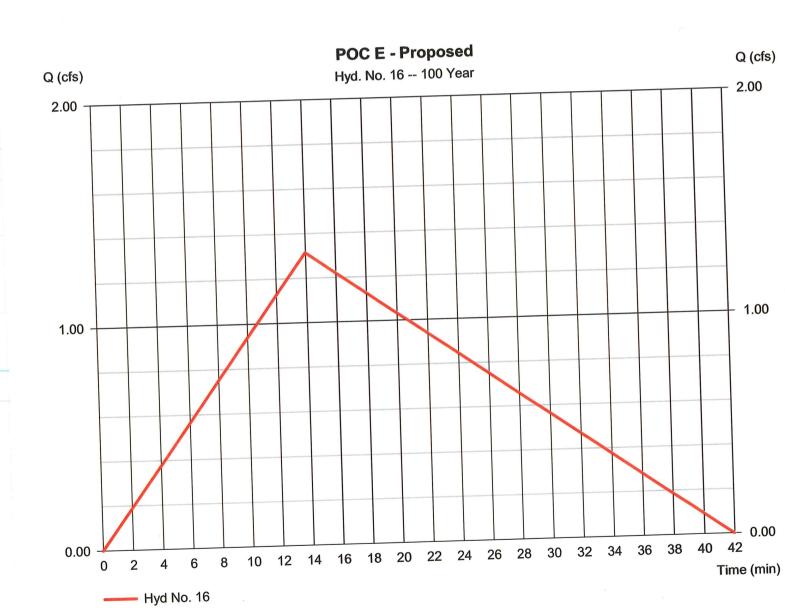
= 0.550 ac= 3.187 in/hr

= Northgate Walk.IDF

= 1.315 cfsPeak discharge = 14 min Time to peak = 1,657 cuft Hyd. volume

= 0.75Runoff coeff.

= 14.00 min Tc by User



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Friday, 07 / 1 / 2016

Return	Intensity-Duration-Frequency Equation Coefficients (FHA)									
Period (Yrs)	В	D	E	(N/A)						
1	0.0000	0.0000	0.0000							
2	0.0000	0.0000	0.0000							
3	0.0000	0.0000	0.0000							
5	0.0000	0.0000	0.0000							
10	0.0000	0.0000	0.0000							
25	8.8045	0.2000	0.4843							
50	0.0000	0.0000	0.0000							
100	11.6617	0.3000	0.4876							

File name: Northgate Walk.IDF

Intensity = $B / (Tc + D)^E$

Return	Intensity Values (in/hr)											
Period (Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
25	3.96	2.86	2.36	2.05	1.84	1.69	1.57	1.47	1.39	1.32	1.26	1.21
50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100	5.17	3.74	3.08	2.69	2.41	2.21	2.05	1.92	1.82	1.73	1.65	1.58

Tc = time in minutes. Values may exceed 60.

Precip. file name: Sample.pcp

	Rainfall Precipitation Table (in)								
Storm Distribution	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
SCS 24-hour	0.00	2.20	0.00	3.30	4.25	5.77	6.80	7.95	
SCS 6-Hr	0.00	1.80	0.00	0.00	2.60	0.00	0.00	4.00	
Huff-1st	0.00	1.55	0.00	2.75	4.00	5.38	6.50	8.00	
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Custom	0.00	1.75	0.00	2.80	3.90	5.25	6.00	7.10	

Appendix 6.4 – Hydrology Maps H1 – Existing Conditions Hydrology Map H2 – Proposed Conditions Hydrology Map

