Macroscopic response of a Hall thruster discharge from an axial-radial PIC model

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Introduction

- HET is a mature technology but physics are still not fully understood (instabilities, wall interaction, non-Maxwellian VDF,...)
- Why kinetic (PIC)?

□ Fluid formulations are not fully consistent and can miss important physics.

- Why 2D PIC axial-radial?
 - ID PIC models
 - Affordable computational cost
 - Strong assumptions due to missing directions
 - 3D PIC models
 - Potentially captures all physics of the discharge
 - Too computationally expensive
 - 2D PIC models
 - Good compromise
 - Axial: main direction of the discharge
 - Radial: wall effects

"Macroscopic plasma analysis from a 1D-radial kinetic results of a Hall thruster discharge". PSST 30.11 (2021):115011.

"Kinetic plasma dynamics in a radial model of a Hall thruster with a curved magnetic field". PSST 31.11 (2022):115003.

Objectives:

1. Address the validity of some of the assumptions taken by 1D PIC models.

2. Compare the kinetic results with standard fluid formulation highlighting the main differences.



The kinetic model

- Electric and magnetic fields
 - Electrostatic assumption.
 - Externally imposed magnetic field, **B**.
 - Self-consistent solution of the electric field, *E*.

 $\varepsilon \nabla^2 \phi = -\rho_{el} \qquad E = -\nabla \phi$





- Particle electrons and singly charged xenon ions
- Fluid neutral background
 - n_n(z) follows a simple depletion law, computed using the steady-state mass continuity equation.
 - \Box u_{zn}=500 m/s and T_n=0.
- Electrically connected anode and cathode
 - $\hfill\square$ I_d continuity is satisfied at any instant
- SEE from lateral dielectric walls





The kinetic model

Collisions

Ionization collisions resolved self-consistently.

Anomalous electron diffusion (isotropic).

Simplified configuration

- □ Radial magnetic field. $B = B_r \mathbf{1}_r$
- □ Only *true* secondary electrons. $\delta_s = E/E_c$
- No cylindrical effects (symmetry).

Acceleration techniques

- □ Steady-state neutrals \rightarrow No breathing mode O(1 ms).
- □ Vacuum permittivity, $\epsilon = \epsilon_0 f_D^2 \rightarrow \text{larger } \Delta t, \Delta x.$
- Numerical parameters (f_D=5)
 - $\Box \Delta z = \Delta r = 0.1 \text{ mm} \rightarrow N_z = 500, N_r = 350.$
 - □ $\Delta t=5 \text{ ps, } t_{sim}=50 \text{ } \mu s \rightarrow N_t=10 \text{ } 000 \text{ } 000.$
 - □ $n_{e0} = n_{i0} = 4 \cdot 10^{17} \text{ m}^{-3}$ (20 particles per cell).







Steady-state macroscopic response



 \blacktriangleright Debye sheaths at the walls \rightarrow Thin non-neutral regions with strong gradients of ϕ and n_e



Steady-state macroscopic response

- \succ Axial profiles of main macroscopic variables along mid-radius M.
- \blacktriangleright Dotted lines mark the thruster exit location (z=2.5 cm)
- \succ Same trends than those obtained by 1Dz fluid and kinetic models.







1Dr code validation



Electron energy balance



ID radial model assumptions
No axial fluxes dl_{ze}/dz=dP_{ze}/dz=0



1Dr code validation

A



- Sheath potential drop is related to the local electron temperature
- Electron temperature anisotropy
 - T_{re}>T_{ze} near the anode
 - \Box T_{re}<T_{ze} elsewhere









The electron VDF at M

- Near exit region
 - Axial VDF is near-Maxwellian.
 - Radial VDF is depleted beyond the energy required for wall collection.
- Near anode region
 - Axial VDF is asymmetric due to electrons collected at the anode.
 - Radial VDF is still depleted beyond the energy required for wall collection.



Non-Maxwellian electron VDF features have a strong effect on wall interaction parameters



The electron momentum equation

Standard solutions along z and r directions Radial momentum $e n_e \frac{\partial \phi}{\partial r} \simeq \frac{\partial p_{rre}}{\partial r}$

□ Axial momentum
$$-j_{\theta e}B_r \simeq \frac{\partial p_{zze}}{\partial z} + e n_e E_z$$

- \succ FLR effects along θ direction
 - □ All the terms in the equation are small. $j_{ze}B_r = \frac{\partial M_{z\theta e}}{\partial z} + \frac{\partial M_{r\theta e}}{\partial r} + F_{col,\theta e}$ $\overline{\overline{M}}_e = \overline{\overline{p}}_e + m_e n_e u_e u_e$
 - Classical solution neglects \bar{M}_e





The electron energy flux vector

- Complex 2D behavior
- Dominant contributions
 - Heat flux, q
 - □ Enthalpy flux, (5/2)T_en_e**u**_e



$$\boldsymbol{P}_{e}'' = \frac{1}{2} m_{e} u_{e}^{2} n_{e} \boldsymbol{u}_{e} + \frac{5}{2} T_{e} n_{e} \boldsymbol{u}_{e} + \overline{\overline{\tau}}_{e} \cdot \boldsymbol{u}_{e} + \boldsymbol{q}_{e}$$
$$\overline{\overline{\tau}}_{e} = \overline{\overline{p}}_{e} - p_{e} \overline{\overline{I}} \qquad \text{Gyrostress tensor}$$

- \succ Axial energy flux (B \perp)
 - □ Near the exit: $(5/2)T_en_eu_{ze} \gg q_{ze}$
 - □ Near the anode: $(5/2)T_en_eu_{ze} \sim q_{ze}$
 - □ A conductive (Fourier) law $q_{ze} \approx -K_e(dT_e/dz)$, seems appropriate only in the near exit region.
- ➢ Radial energy flux (B∥)
 - Enthalpy flux and heat flux are close in all locations in the channel.
 - □ Heat flux seems to follow a convective-type law. $q_{re} \propto (5/2)T_e n_e u_{re}$



Conclusion and future work

- 2D simulation of a simplified HET discharge.
- The electron VDF is non-Maxwellian and its features are different in the near-anode and near-exit regions. This has important implications on the electron behavior.
 - Wall interaction magnitudes.
 - □ Full pressure tensor.
 - Complex heat flux vector.
- ID model assumptions in the near-exit region.
 - Qualitative matching of plasma profiles.
 - \Box dI_{ze}/dz=0 has been proven to be a good approximation in the near exit region.
 - Neglecting axial fluxes in the 1Dr power balance is questionable.
 - Radial effects are difficult to model in 1Dz models.

Future work

- Realistic/complex magnetic topology.
- Include other collisional processes.
- □ Realistic near plume.

Other research

- Penning discharge benchmark.
- Turbulent transport studies

"Two-dimensional kinetic simulation of electrostatic instabilities in a Hall plasma". IEPC-2022-314



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Backup slides



Effects of an augmented vacuum permittivity

Radial profiles

Axial profiles



Sheath thickness, $\lambda_{D} \propto f_{D}$

- Smoother gradients
- Physical ordering
 - □ Space: $\lambda_D < r_{Le} < L$
 - \Box Time: $1/\omega_{pe} < 1/\omega_{ce}$
- ▶ f_D=20: limit case
- ➢ f_D=10: good enough
- \succ f_D=5: fine details
- Computational cost scales ∝ f_D-3

