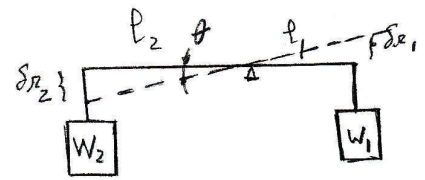


2.1

2.1



$$\sum \vec{F}_i \cdot \delta \vec{R}_i = 0 \quad \delta R_1 = l_1 \tan \theta \quad W_1 l_1 \tan \theta - W_2 l_2 \tan \theta = 0$$

$$\delta R_2 = -l_2 \tan \theta \quad \boxed{W_1 l_1 = W_2 l_2}$$

2.3

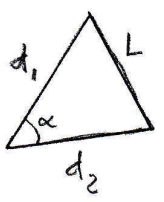
2.3

$$\sum_i \vec{F}_i \cdot \delta \vec{R}_i = 0$$

- a)  $\vec{F}_1 \cdot \delta \vec{R}_1 = 0$ , e como  $\delta \vec{R}_1$  é qualquer, então  $\vec{F}_1 = 0$
- b)  $\vec{F}_1 \cdot \delta \vec{R}_1 + \vec{F}_2 \cdot \delta \vec{R}_2 = 0$  mas  $\delta \vec{R}_1 = \delta \vec{R}_2 = \delta \vec{R}$ , pelo que  $(\vec{F}_1 + \vec{F}_2) \cdot \delta \vec{R} = 0 \Rightarrow \vec{F}_1 = -\vec{F}_2$   
 isto é, as forças são iguais em grandeza, colineares e opostas em sentido
- c)  $(\vec{F}_1 + \vec{F}_2 + \vec{F}_3) \cdot \delta \vec{R} = 0 \Rightarrow \vec{F}_3 = -(\vec{F}_1 + \vec{F}_2)$  e a soma de 2 vectores dá um vector coplanar com eles. Logo  $\vec{F}_3$  é coplanar com  $\vec{F}_1$  e  $\vec{F}_2$  e, além disso, as 3 linhas de acção das 3 forças intersectam-se no mesmo ponto O.
- 
- d)  $\sum_i \vec{F}_i \cdot \delta \vec{R}_i = 0$ ;  $\sum F_i \delta R_i \cos \Delta_i = 0$ ;  $(\sum F_i \cos \Delta_i) \delta R_i = 0$   
 e como  $\delta R_i$  é qualquer, vem:  $\sum_i F_i \cos \Delta_i = 0$

2.4

2.4



a)  $L^2 = d_1^2 + d_2^2 - 2d_1 d_2 \cos \alpha$  e se  $\alpha$  varia de  $\Delta \alpha$ , vem:

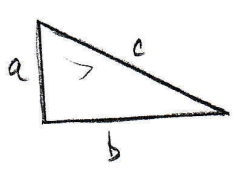
$$(L + \Delta L)^2 = d_1^2 + d_2^2 - 2d_1 d_2 \cos(\alpha + \Delta \alpha)$$

$$L^2 + 2L \Delta L + (\Delta L)^2 = d_1^2 + d_2^2 - 2d_1 d_2 (\cos \alpha \cos \Delta \alpha - \sin \alpha \sin \Delta \alpha)$$

e se  $\Delta \alpha$  pequeno  $\cos \Delta \alpha \approx 1$  e  $\sin \Delta \alpha \approx \Delta \alpha$  e vem:

$$L^2 + 2L \Delta L + (\Delta L)^2 = \underbrace{d_1^2 + d_2^2 - 2d_1 d_2 \cos \alpha}_{L^2} + 2d_1 d_2 \sin \alpha \Delta \alpha$$

$(\Delta L)^2$  vem:  $2L \Delta L = 2d_1 d_2 \sin \alpha \Delta \alpha$  ou  $\boxed{\Delta L = \frac{d_1 d_2 \sin \alpha}{L} \Delta \alpha}$



b)  $c^2 = a^2 + b^2$

$$(c + \Delta c)^2 = (a + \Delta a)^2 + (b + \Delta b)^2$$

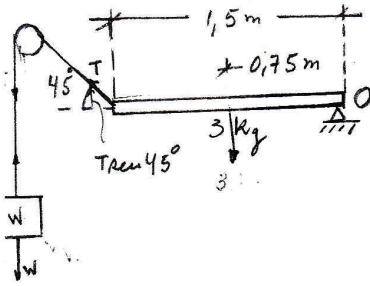
$$c^2 + 2c \Delta c + (\Delta c)^2 = a^2 + 2a \Delta a + (\Delta a)^2 + b^2 + 2b \Delta b + (\Delta b)^2$$

e desprezando  $(\Delta c)^2, (\Delta a)^2, (\Delta b)^2$  e simplificando dá:  $\boxed{c \Delta c = a \Delta a + b \Delta b}$



2.5

2.5



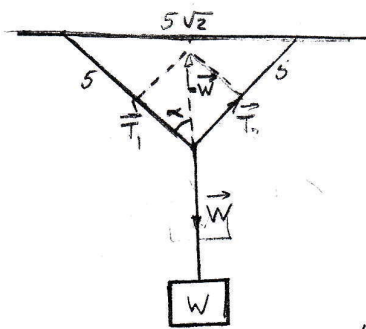
No equilíbrio estático temos:  $T = W$

$$T \cos 45^\circ \cdot 1,5 - 3 \frac{1,5}{2} = 0 \quad \sum_i \text{momentos em relação a } O.$$

$$T = \frac{3 \cdot \frac{1,5}{2}}{\frac{\sqrt{2}}{2} \cdot 1,5} = \frac{3}{\sqrt{2}} = \frac{3}{\sqrt{2}} \text{ kgf} = W$$

2.9

2.9



$$\sin \alpha = \frac{5\sqrt{2}}{2 \cdot 5} = \frac{1}{\sqrt{2}} = \cos \alpha$$

$$T_1 = W \cos \alpha = \frac{1}{\sqrt{2}} 50 = \frac{50}{\sqrt{2}}$$

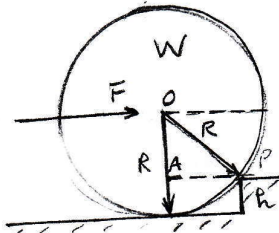
$$\vec{T}_1 + \vec{T}_2 + \vec{W} = 0 \quad |\vec{T}_1| = |\vec{T}_2| = T$$

$$W = T_1 \cos \alpha + T_2 \cos \alpha = 2T \cos \alpha$$

$$T = \frac{1}{2 \cos \alpha} W = \frac{W}{2 \cdot \frac{1}{\sqrt{2}}} = \frac{1}{\sqrt{2}} W$$

2.11

2.11



$$\overline{PA} = \sqrt{R^2 - (R-h)^2}$$

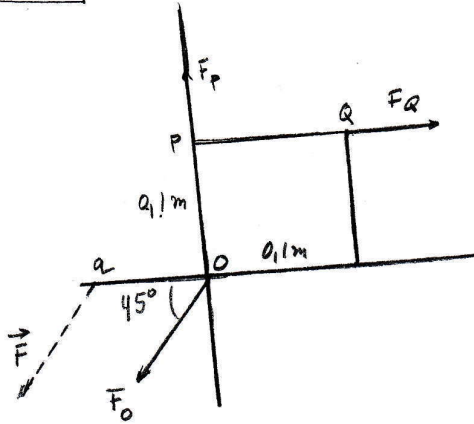
$$\overline{OA} = R-h$$

$\Sigma$  momentos em relação a P =  $W \sqrt{R^2 - (R-h)^2} = F(R-h)$

$$F = \frac{\sqrt{R^2 - R^2 + 2Rh - h^2}}{R-h} W = \frac{\sqrt{h(2R-h)}}{R-h} W$$

2.13

2.13



$$\vec{F}_P = 50 \cdot \hat{j}$$

$$\vec{F}_Q = 50 \cdot \hat{i}$$

$$\vec{F}_0 = -50 \cos 45^\circ \hat{i} - 50 \sin 45^\circ \hat{j} = -\frac{50}{\sqrt{2}} \hat{i} - \frac{50}{\sqrt{2}} \hat{j}$$

$$\vec{F}_P + \vec{F}_Q + \vec{F}_0 = 50 \left(1 - \frac{1}{\sqrt{2}}\right) \hat{i} + 50 \left(1 - \frac{1}{\sqrt{2}}\right) \hat{j} = 50 \left(1 - \frac{1}{\sqrt{2}}\right) (\hat{i} + \hat{j}) = \vec{R} = -\vec{F}$$

$M_{F_P/O}$  = momento da força  $F_P$  em relação a  $O = 0$

$M_{F_Q/O}$  = "  $F_Q$  " =  $50 \cdot 0,1 \cdot (-\hat{k})$

$M_{F_0/O}$  = "  $F_0$  " =  $0$

$$M_{R/O} = \vec{r} \wedge (\vec{F}) = -[a \hat{i} \wedge 50 \left(1 - \frac{1}{\sqrt{2}}\right) (\hat{i} + \hat{j})] = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ a & 0 & 0 \\ 1 & 1 & 0 \end{vmatrix} 50 \left(1 - \frac{1}{\sqrt{2}}\right) =$$

$$= -a \cdot 50 \left(1 - \frac{1}{\sqrt{2}}\right) \hat{k}$$

Mas  $\Sigma$  Momentos = 0 e dá  $[0 - 50 \cdot 0,1 - a 50 \left(1 - \frac{1}{\sqrt{2}}\right)] \hat{k} = 0$  ou  $-a 50 \left(1 - \frac{1}{\sqrt{2}}\right) = 50 \cdot 0,1$

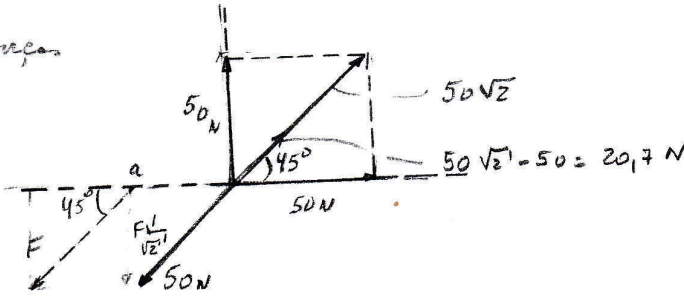
$$a = \frac{-0,1}{1 - \frac{1}{\sqrt{2}}} = -0,34 \text{ m} \quad \text{com } \vec{F} = -50 \left(1 - \frac{1}{\sqrt{2}}\right) (\hat{i} + \hat{j}); |\vec{F}| = 50 \left(1 - \frac{1}{\sqrt{2}}\right) \sqrt{1^2 + 1^2} = 20,7 \text{ N}$$



2.13 Contín.

Contín 2.13

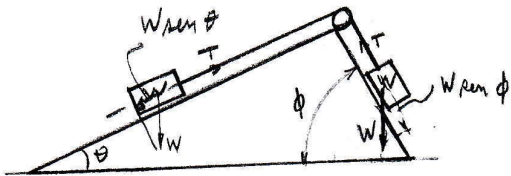
A geometria da figura possibilita uma resolução mais directa. Calculamos a resultante das 3 forças



O ponto de aplicação é tal que:  $F_Q \cdot 0,1 + |\vec{F}| \frac{1}{\sqrt{2}} \cdot a = 0 \quad a = -0,3415 \text{ m}$

2.15

2.15



$$W \sin \theta + \frac{W}{g} \ddot{l}_\theta = T$$

mas  $\ddot{l}_\theta = \ddot{l}_\phi$

$$W \sin \phi - \frac{W}{g} \ddot{l}_\phi = T$$

$$\frac{W}{g} \ddot{l}_\theta + W \sin \theta = W \sin \phi - \frac{W}{g} \ddot{l}_\theta \quad ; \quad 2 \frac{W}{g} \ddot{l}_\theta = W (\sin \phi - \sin \theta) \quad ; \quad \ddot{l}_\theta = \frac{g}{2W} W (\sin \phi - \sin \theta)$$

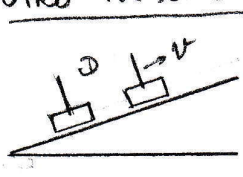
$$\ddot{l}_\theta = \frac{1}{2} g (\sin \phi - \sin \theta) \quad \dot{l}_\theta = \frac{1}{2} g (\sin \phi - \sin \theta) t + C \quad \text{e como } \dot{l}_\theta(t=0) = 0 \Rightarrow C = 0$$

$$l_\theta = \frac{1}{4} g (\sin \phi - \sin \theta) t^2 + C \quad \text{mas } l_\theta(t=0) = 0 \Rightarrow C = 0 \quad \text{donde } t = \sqrt{\frac{4l_0}{g(\sin \phi - \sin \theta)}}$$

que substituindo na equação da velocidade  $\dot{l}_\theta = \frac{1}{2} g (\sin \phi - \sin \theta) \cdot \sqrt{\frac{4l_0}{g(\sin \phi - \sin \theta)}}$

$$= \sqrt{l_0 g (\sin \phi - \sin \theta)} \quad \text{donde } v = \sqrt{Dg(\sin \phi - \sin \theta)}$$

OUTRO MÉTODO: Pela conservação da energia podemos escrever:



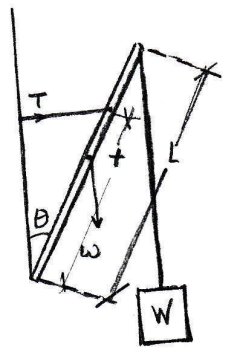
$$\frac{1}{2} \frac{W}{g} v^2 + \frac{WgD \sin \theta}{g} + \frac{1}{2} \frac{W}{g} v^2 - \frac{W}{g} gD \sin \phi = 0$$

$$2 \cdot \frac{1}{2} v^2 = gD (\sin \phi - \sin \theta) \quad \text{donde } v = \sqrt{gD(\sin \phi - \sin \theta)}$$



2.17

2.19



$$\sum \vec{M} = 0$$

$$\frac{L}{2} \sin \theta \cdot w + L \sin \theta W - T \times \cos \theta = 0$$

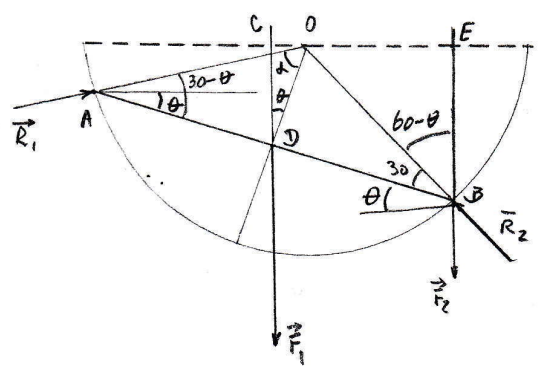
$$T = \frac{L}{x} \left( \frac{w}{2} + W \right) \tan \theta$$

2.19

2.19

$$\overline{AB} = L = \sqrt{3} R$$

$$R \sin \alpha = \frac{R}{2} = \frac{\sqrt{3}}{2} R; \sin \alpha = \frac{\sqrt{3}}{2}; \alpha = 60^\circ$$



$$\overline{OD} = R \cdot \sin 30^\circ = \frac{R}{2}$$

$$\overline{OC} = \frac{R}{2} \sin \theta$$

$$\overline{OE} = R \sin(60^\circ - \theta)$$

O sistema está em equilíbrio estático. Então as reacções em A e B não têm componente tangencial, pois se tivessem e como a barra está em equilíbrio estático e não há atrito entre as extremidades da barra e a superfície em que se apoia, a barra não estaria em equilíbrio estático, como, por hipótese está.

Calculamos a soma dos momentos em relação ao ponto O.

Os momentos das forças  $\vec{R}_1$  e  $\vec{R}_2$  em relação a O são nulos pois a linha de acção dessas forças passam por O, porque não há componente tangencial.

Momento de  $F_1$  em relação a O =  $F_1 \cdot \overline{OC} = W \frac{R}{2} \sin \theta$   
 " "  $F_2$  " " " =  $F_2 \cdot \overline{OE} = \frac{W}{2} R \sin(60^\circ - \theta)$

e a sua soma deve ser nula, e vem:

$$W \frac{R}{2} \sin \theta - \frac{W}{2} R \sin(60^\circ - \theta) = 0$$

$$\sin \theta - \sin(60^\circ - \theta) = 0$$

$$\sin \theta - \sin 60^\circ \cos \theta + \sin \theta \cos 60^\circ = 0; \sin \theta \left( 1 + \frac{1}{2} \right) = \frac{\sqrt{3}}{2} \cos \theta$$

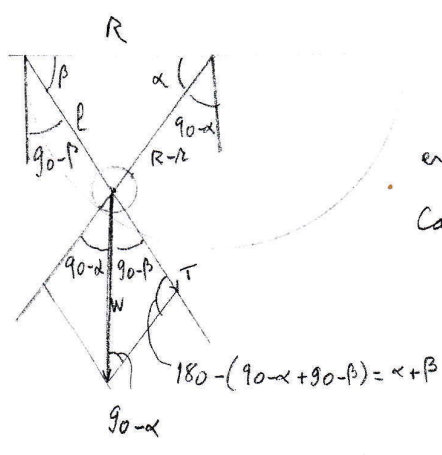
$$\tan \theta = \frac{\frac{\sqrt{3}}{2}}{1 + \frac{1}{2}} = \frac{\sqrt{3}}{3} \text{ pelo que } \theta = 30^\circ$$



2.21

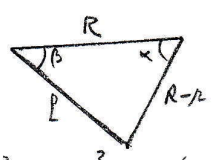
2.21

$R = 49 \text{ cm}$   
 $r = 4,5 \text{ cm}$



$$\frac{W}{\sin(\alpha+\beta)} = \frac{T}{\sin(90-\alpha)} \quad T = \frac{\sin(90-\alpha)}{\sin(\alpha+\beta)} W = \frac{\cos \alpha}{\sin(\alpha+\beta)} W$$

em que T é a tensão no fio para  $l = 40 \text{ cm}$   
 Cálculo de  $\alpha$  e de  $\beta$ :



$$l^2 = R^2 + (R-r)^2 - 2R(R-r)\cos \alpha; \quad \cos \alpha = \frac{R^2 + (R-r)^2 - l^2}{2R(R-r)}$$

$$\cos \alpha = \frac{49^2 + (49-4,5)^2 - 40^2}{2 \cdot 49 \cdot (49-4,5)} = 0,6377 \quad \text{donde } \alpha = 50,37^\circ$$

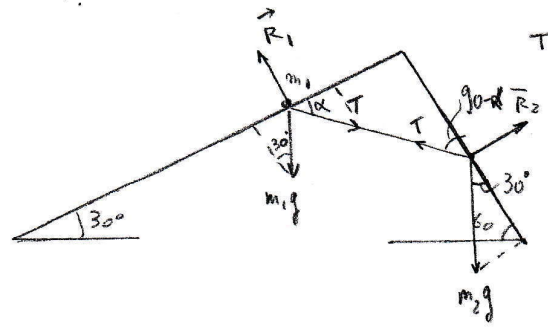
Por outro lado  $(R-r)^2 = l^2 + R^2 - 2lR \cos \beta; \quad \cos \beta = \frac{l^2 + R^2 - (R-r)^2}{2lR} = \frac{40^2 + 49^2 - (49-4,5)^2}{2 \cdot 40 \cdot 49} = 0,515$

donde  $\beta = 58,96^\circ$  e então vem:

$$T = \frac{\cos 50,37}{\sin(50,37+58,96)} W = 0,67 W$$

2.23

2.23



$$T \cos \alpha = m_1 g \sin 30^\circ$$

$$T \cos(90-\alpha) = m_2 g \cos 30^\circ \quad \text{e dividindo vem:}$$

$$\frac{\cos \alpha}{\cos(90-\alpha)} = \frac{m_1 \sin 30}{m_2 \cos 30}; \quad \frac{1}{\tan \alpha} = \frac{m_1}{m_2} \tan 30^\circ$$

$$\tan \alpha = \frac{m_2}{m_1} \frac{1}{\tan 30} = 3 \cdot 1,73 = 5,196 \quad \alpha = 79,1^\circ$$

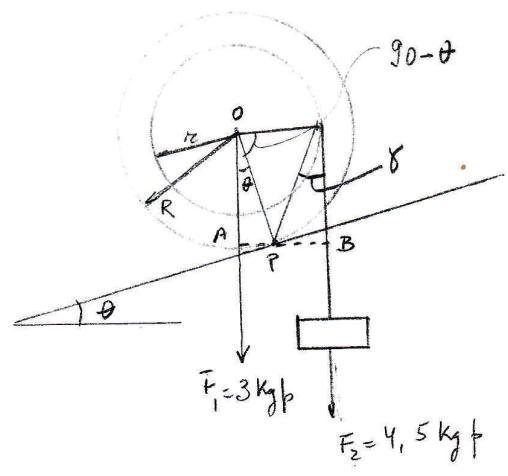
e ainda  $T = m_1 g \frac{\sin 30}{\cos 79,1} = 264,6 \text{ gramas-peso}$



2.25

2.25

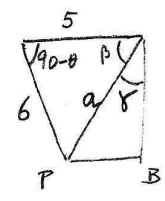
$R=6$   
 $r=5$



No equilíbrio  $\Sigma$  Momentos em relação a P = 0

$\overline{AP} = R \text{ sen } \theta$

Cálculo de  $\overline{PB}$



$a^2 = 5^2 + 6^2 - 2 \cdot 5 \cdot 6 \cos(90-\theta) = 61 - 60 \text{ sen } \theta$

$a = \sqrt{61 - 60 \text{ sen } \theta}$

$\frac{6}{\text{sen } \beta} = \frac{\sqrt{61 - 60 \text{ sen } \theta}}{\text{sen}(90-\theta)}$

$\text{sen } \beta = \frac{6 \text{ sen}(90-\theta)}{\sqrt{61 - 60 \text{ sen } \theta}} = \frac{6 \text{ cos } \theta}{\sqrt{61 - 60 \text{ sen } \theta}} = \frac{6 \text{ cos } \theta}{a}$

$\gamma = 90 - \beta$

$\Sigma \vec{M} = 0$

$3 \cdot R \cdot \text{sen } \theta - 4,5 \cdot a \cdot \text{sen } \gamma = 0$

$3 \cdot R \cdot \text{sen } \theta = 4,5 \cdot \sqrt{61 - 60 \text{ sen } \theta} \cdot \text{sen}(90-\beta)$

$= 4,5 \sqrt{61 - 60 \text{ sen } \theta} \cdot \text{cos } \beta = 4,5 \cdot a \cdot \sqrt{1 - \left(\frac{6 \text{ cos } \theta}{a}\right)^2} = 4,5 \cdot a \cdot \frac{\sqrt{a^2 - (6 \text{ cos } \theta)^2}}{\sqrt{a^2}} = L$

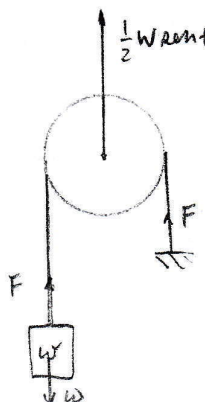
$3R \text{ sen } \theta = 4,5 \cdot \sqrt{a^2 - (6 \text{ cos } \theta)^2} = 4,5 \sqrt{61 - 60 \text{ sen } \theta - 36 \text{ cos }^2 \theta} = 4,5 \sqrt{61 - 60 \text{ sen } \theta - 36 + 36 \text{ sen }^2 \theta}$

$\frac{9 R^2}{4,5^2} \text{ sen }^2 \theta = 25 - 60 \text{ sen } \theta + 36 \text{ sen }^2 \theta ; \underbrace{\left(36 - \frac{9 \cdot 36}{4,5^2}\right)}_{=20} \text{ sen }^2 \theta - 60 \text{ sen } \theta + 25 = 0$

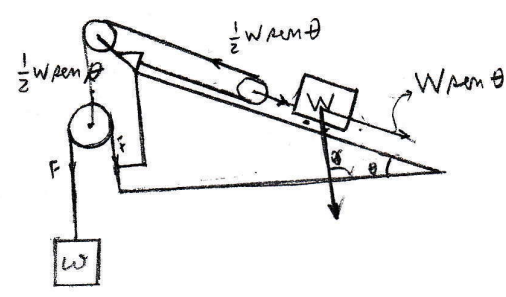
$\text{sen }^2 \theta - 3 \text{ sen } \theta + 1,25 = 0$  duas soluções, mas  $\text{sen } \theta = 2,5$  impossível!  
 $\text{sen } \theta = \frac{1}{2}$  donde  $\theta = 30^\circ$

2.27

2.27



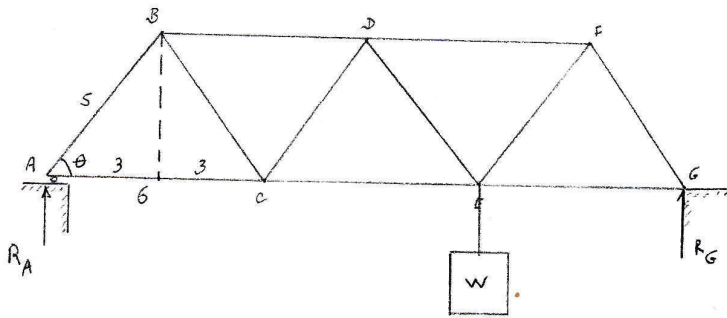
$\frac{1}{2} W \text{ sen } \theta = 2F$



$\frac{1}{2} W \text{ sen } \theta = 2 \cdot F = 2 \cdot W$

$W = \frac{4W}{\text{sen } \theta}$





$$\cos \theta = \frac{3}{5}$$

$$\sin \theta = \sqrt{1 - \left(\frac{3}{5}\right)^2} = \sqrt{1 - \frac{9}{25}} = \frac{4}{5}$$

Nota: cada nó é entendido como um ponto material livre e actualizado por forças, e as barras estão em compressão e força no nó aponta para o nó; em tração será o contrário.

Calculo das forças  $R_A$  e  $R_G$ :  $R_A + R_G = W$  e  $R_A \cdot 18 - 6W = 0$  donde  $R_A = \frac{1}{3}W$  e  $R_G = \frac{2}{3}W$

Equilíbrio de forças nos nós:

nó A:

$$F_{AB} \sin \theta - R_A = 0; F_{AB} = \frac{1}{\sin \theta} R_A = \frac{5}{4} \frac{1}{3} W \quad F_{AB} = \frac{5}{12} W \text{ compressão}$$

$$-F_{AB} \cos \theta + F_{AC} = 0; F_{AC} = F_{AB} \cos \theta = \frac{5}{12} \frac{3}{5} W = \frac{1}{4} W \quad F_{AC} = \frac{1}{4} W \text{ tração}$$

nó B:

$$\frac{5}{12} W \sin \theta - F_{BC} \sin \theta = 0 \quad F_{BC} = \frac{5}{12} W \text{ tração}$$

$$\frac{5}{12} W \cos \theta + F_{BC} \cos \theta + F_{BD} = 0; \frac{5}{12} \frac{3}{5} W + \frac{5}{12} \frac{3}{5} W = -F_{BD} \quad F_{BD} = -\frac{1}{2} W \text{ compressão}$$

nó C:

$$\frac{5}{12} W \sin \theta + F_{CD} \sin \theta = 0 \quad F_{CD} = -\frac{5}{12} W \text{ compressão}$$

$$-\frac{5}{12} W \cos \theta - \frac{1}{4} W + F_{CD} \cos \theta + F_{CE} = 0; -\frac{5}{12} \frac{3}{5} W - \frac{1}{4} W - \frac{5}{12} \frac{3}{5} W = -F_{CE}; F_{CE} = \frac{3}{4} W \text{ tração}$$

nó D:

$$\frac{5}{12} W \sin \theta - F_{DE} \sin \theta = 0; F_{DE} = \frac{5}{12} W \text{ tração}$$

$$\frac{1}{2} W + \frac{5}{12} W \cos \theta + F_{DE} \cos \theta + F_{DF} = 0; \left(\frac{1}{2} + \frac{5}{12} \frac{3}{5} + \frac{5}{12} \frac{3}{5}\right) W = -F_{DF} \quad F_{DF} = -W \text{ compressão}$$

nó E:

$$\frac{5}{12} W \sin \theta + F_{EF} \sin \theta - W = 0; F_{EF} = \frac{1}{\sin \theta} \left(W - \frac{5}{12} W \sin \theta\right) = \frac{5}{4} \left(1 - \frac{5}{12} \frac{4}{5}\right) W; F_{EF} = \frac{5}{6} W \text{ tração}$$

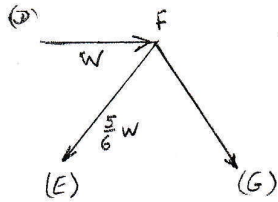
$$-\frac{3}{4} W - \frac{5}{12} W \cos \theta + F_{EF} \cos \theta + F_{EG} = 0; \left(-\frac{3}{4} - \frac{5}{12} \frac{3}{5} + \frac{5}{6} \frac{3}{5}\right) W = -F_{EG}; F_{EG} = \frac{1}{2} W \text{ tração}$$




2.29 Contin.

Contin. 2.29

nó F:

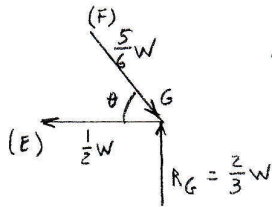


$$\frac{5}{6}W \sin \theta + F_{FG} \sin \theta = 0 ;$$

$$F_{FG} = -\frac{5}{6}W \text{ compressão}$$

Conhecemos agora o valor de todas as forças que atuam nos barras e se estas estão em compressão ou em tração. Para verificação da correção dos cálculos vamos calcular o equilíbrio das forças no nó G, que se deverá verificar se os valores calculados para as barras FG e EG estiverem corretos.

nó G:



$$\left. \begin{aligned} -\frac{5}{6}W \sin \theta + R_G &= -\frac{5}{6} \frac{4}{5}W + \frac{2}{3}W = \left(-\frac{2}{3} + \frac{2}{3}\right)W = 0 \\ -\frac{1}{2}W + \frac{5}{6}W \cos \theta &= \left(-\frac{1}{2} + \frac{5}{6} \frac{3}{5}\right)W = \left(-\frac{1}{2} + \frac{1}{2}\right)W = 0 \end{aligned} \right\} \text{ verifica-se o equilíbrio em G.}$$

b) Todas as barras em tração podem ser substituídas por cabos flexíveis.

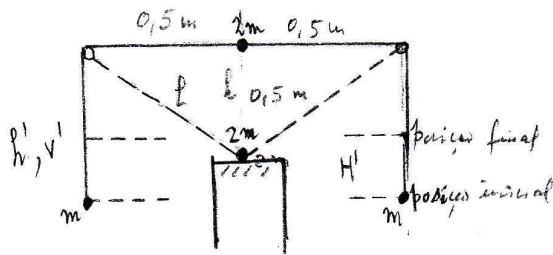
São elas: AC, BC, CE, DE, EF, EG,

$$F_{BD} = \frac{1}{2}W \text{ compressão} \quad \text{e} \quad F_{DE} = \frac{5}{12}W \text{ tração}$$



2.31

2.31



A perda de energia potencial da massa central 2m é transformada em energia cinética da massa central, energia cinética das duas massas laterais e em energia potencial das molas.

ou seja  $2mgH = \frac{1}{2} 2m v^2 + 2 \cdot \frac{1}{2} m v'^2 + 2mgH'$

ou  $l = \sqrt{(\frac{1}{2})^2 + h'^2} = \frac{1}{2} \sqrt{1 + 4h'^2}$

$v' = \frac{dh'}{dt} = \frac{dl}{dt} = \frac{1}{2} \cdot \frac{1}{2} \frac{8h}{\sqrt{1+4h'^2}} \frac{dh'}{dt} = \frac{2h'}{\sqrt{1+4h'^2}} v$

Se  $h = 0,5m$  vem  $v' = \frac{1}{\sqrt{2}} v$

Cálculo de  $H'$ :  $l_{max} = \frac{1}{2} \sqrt{1 + 4(\frac{1}{2})^2} = 0,5\sqrt{2}$  e  $h_{min} = 0,5$  e então

$H' = l_{max} - l_{min} = 0,5(\sqrt{2} - 1) = 0,207m$

E substituindo na equação das energias, vem:

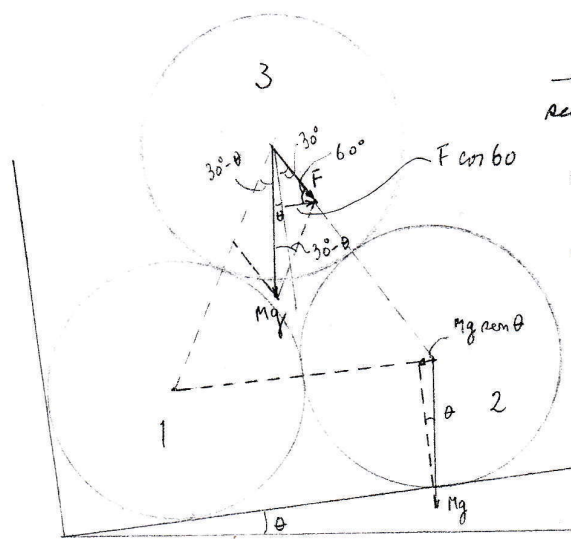
$2mgH = \frac{1}{2} 2m v^2 + 2 \cdot \frac{1}{2} m \frac{1}{2} v^2 + 2mgH'$

$v^2 + \frac{1}{2} v^2 = 2g(H - H')$ ;  $\frac{3}{2} v^2 = 2g(0,5 - 0,207)$ ;  $v^2 = \frac{4}{3} g(0,5 - 0,207)$

e vem  $v = 1,96 m/s^{-1}$

2.33

2.33



$\frac{F}{\cos(30-\theta)} = \frac{Mg}{\cos 120}$

$F \cos 60 = Mg \sin \theta$  para que o cilindro 3 esteja em equilíbrio com o cilindro 2

Eliminando F vem:  $\tan \theta = \frac{1}{3\sqrt{3}}$  ou  $\theta = 10,9^\circ$

$\frac{\sin(30-\theta)}{\sin 60} \cos 60 = \sin \theta$ ;  $\sin 30 \cos \theta - \sin \theta \cos 30 = \tan 60 \sin \theta$

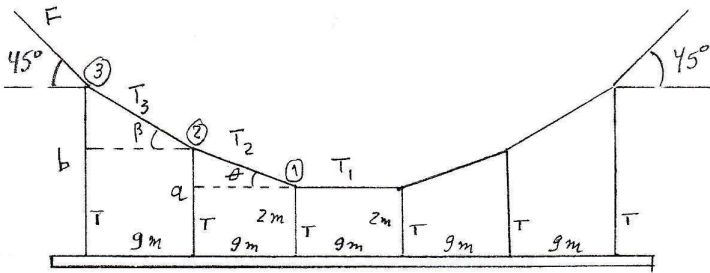
$\sin 30 - \cos 30 \tan \theta = \tan 60 \tan \theta$ ;  $\sin 30 = \tan \theta (\cos 30 + \tan 60)$

$\tan \theta = \frac{\sin 30}{\cos 30 + \tan 60} = \frac{1}{2} \frac{1}{\frac{\sqrt{3}}{2} + \sqrt{3}} = \frac{1}{3\sqrt{3}}$



2.35

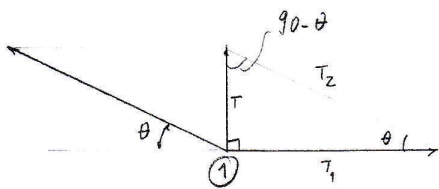
2.35



$$\operatorname{tg} \theta = \frac{a-z}{g}$$

$$\operatorname{tg} \beta = \frac{b-a}{g}$$

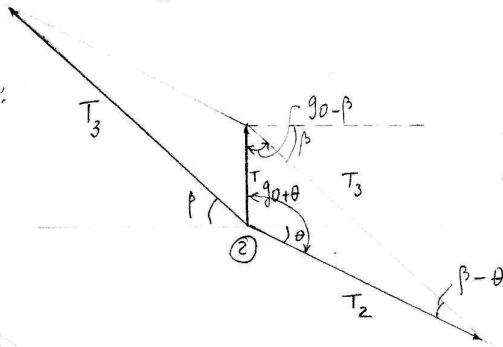
Equilíbrio de forças no nó 1:



$$\frac{T}{\operatorname{sen} \theta} = \frac{T_1}{\operatorname{sen}(90-\theta)} = \frac{T_2}{\operatorname{sen} 90^\circ} \quad \text{donde}$$

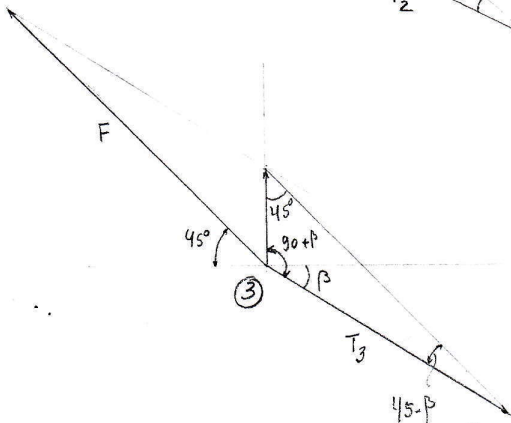
$$T_2 = \frac{T}{\operatorname{sen} \theta} \quad \text{e} \quad T_1 = \frac{T}{\operatorname{tg} \theta}$$

nó 2:



$$\frac{T}{\operatorname{sen}(\beta-\theta)} = \frac{T_2}{\operatorname{sen}(90-\beta)} = \frac{T_3}{\operatorname{sen}(90+\theta)} \quad \text{donde:}$$

$$T_3 = \frac{\operatorname{sen}(90+\theta)}{\operatorname{sen}(90-\beta)} T_2 = \frac{\operatorname{csc} \theta}{\operatorname{csc} \beta} \frac{T}{\operatorname{sen} \theta} = \frac{T}{\operatorname{tg} \theta \operatorname{csc} \beta}$$



$$\frac{F}{\operatorname{sen}(90+\beta)} = \frac{T}{\operatorname{sen}(45-\beta)} = \frac{T_3}{\operatorname{sen} 45^\circ}$$

$$\text{Mas } F \cdot \operatorname{sen} 45^\circ = 3 \cdot T \quad \text{ou} \quad F = 3\sqrt{2} T$$

$$\text{e vem: } \frac{3\sqrt{2} T}{\operatorname{sen}(90+\beta)} = \frac{T}{\operatorname{sen}(45-\beta)} \quad \text{e simplificando:}$$

$$3\sqrt{2} \operatorname{sen}(45-\beta) = \operatorname{sen}(90+\beta) ; \quad 3\sqrt{2} [\operatorname{sen} 45 \operatorname{csc} \beta - \operatorname{sen} \beta \operatorname{csc} 45] = \operatorname{csc} \beta ;$$

$$\operatorname{sen} 45 - \operatorname{tg} \beta \operatorname{csc} 45 = \frac{1}{3\sqrt{2}} ; \quad \operatorname{csc} 45 \cdot [\operatorname{tg} 45 - \operatorname{tg} \beta] = \frac{1}{3\sqrt{2}} ; \quad 1 - \operatorname{tg} \beta = \frac{1}{3\sqrt{2}} \frac{1}{\operatorname{csc} 45} = \frac{1}{3}$$

$$\operatorname{tg} \beta = 1 - \frac{1}{3} = \frac{2}{3} \quad \text{ou seja} \quad \frac{b-a}{g} = \frac{2}{3}$$

$$\text{Por outro lado: } T_3 = \frac{T}{\operatorname{tg} \theta \operatorname{csc} \beta} = \frac{\operatorname{sen} 45^\circ}{\operatorname{sen}(90+\beta)} \cdot 3\sqrt{2} T ; \quad \frac{T}{\operatorname{tg} \theta \operatorname{csc} \beta} = \frac{\sqrt{2}}{2} \frac{1}{\operatorname{csc} \beta} \cdot 3\sqrt{2} T ; \quad \frac{1}{\operatorname{tg} \theta} = 3$$

$$\operatorname{tg} \theta = \frac{1}{3} \quad \text{ou seja} \quad \frac{a-z}{g} = \frac{1}{3} \quad \text{ou} \quad a = 5 \text{ m e de } \frac{b-a}{g} = \frac{2}{3} \text{ dá } b-a = 6 \quad b = 5+6 = 11 \text{ m}$$

Assim:  $a = 5 \text{ m}$  e  $b = 11 \text{ m}$  e  $\beta = 33,7^\circ$  e  $\theta = 18,4^\circ$  e  $F = 3\sqrt{2} T$  que dá:

$$F = 3\sqrt{2} \cdot \frac{4,8 \cdot 10^4}{6} = 34 \cdot 10^3 \text{ kgf} = 34 \text{ tonf}$$

